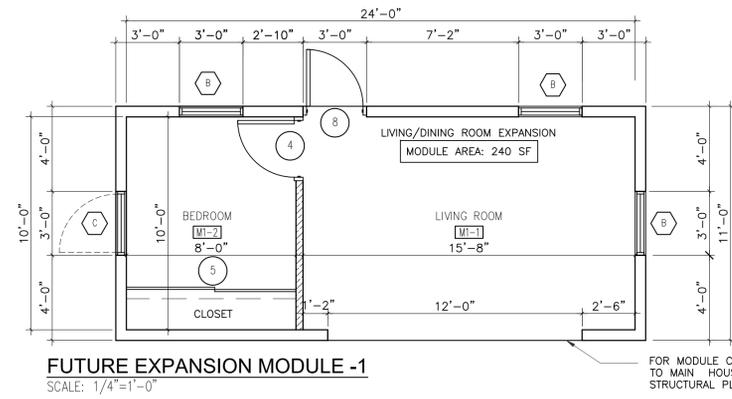


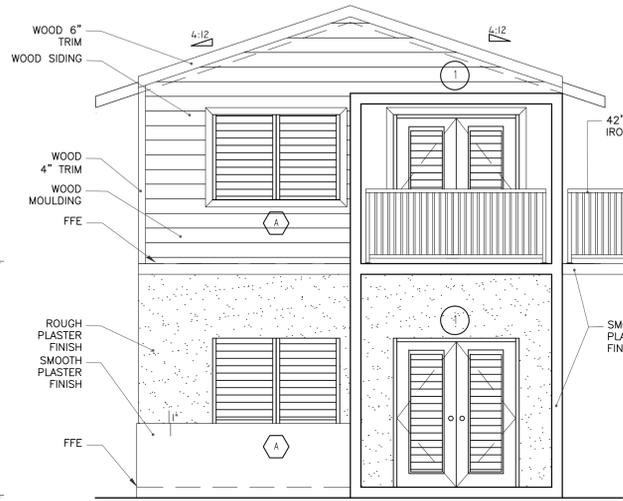
ADDITION OPTION



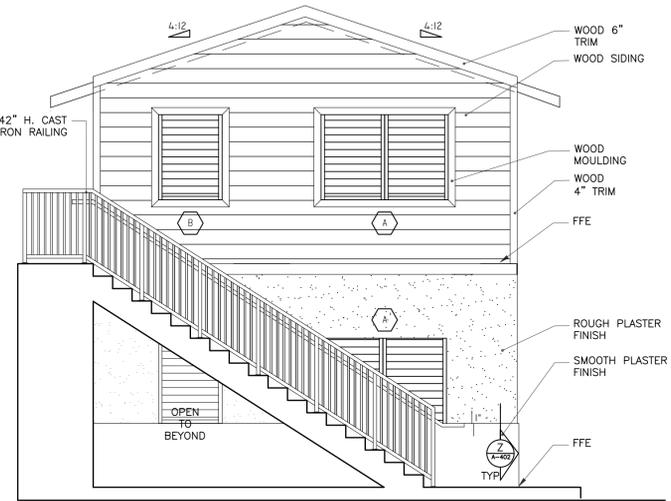
FUTURE EXPANSION MODULE - 1
SCALE: 1/4"=1'-0"

FOR MODULE CONNECTION TO MAIN HOUSE REFER TO STRUCTURAL PLANS

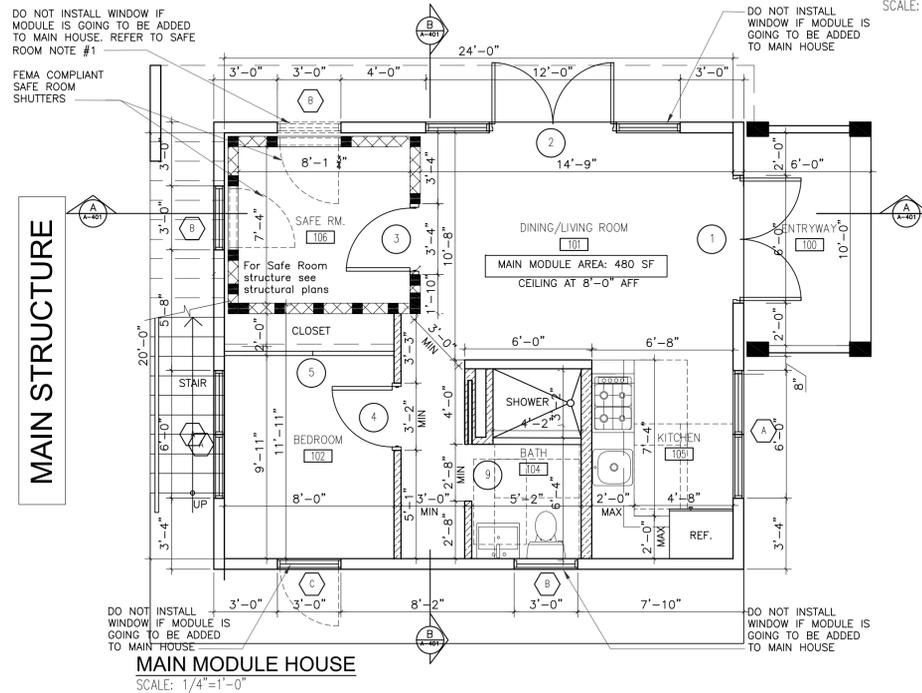
FRONT ELEVATION
SCALE: 1/4"=1'-0"



REAR ELEVATION
SCALE: 1/4"=1'-0"



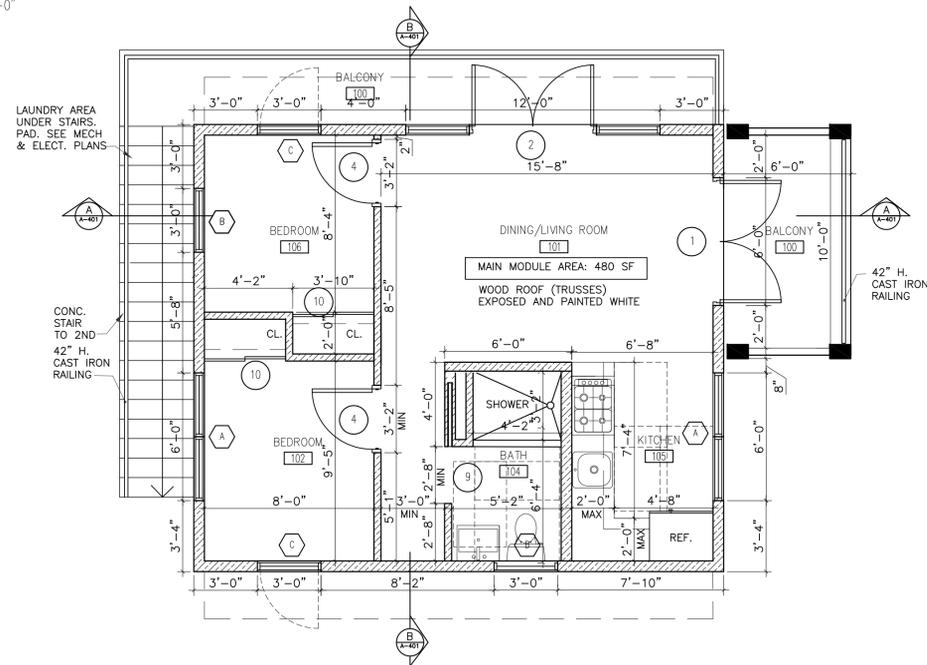
MAIN STRUCTURE



MAIN MODULE HOUSE
SCALE: 1/4"=1'-0"

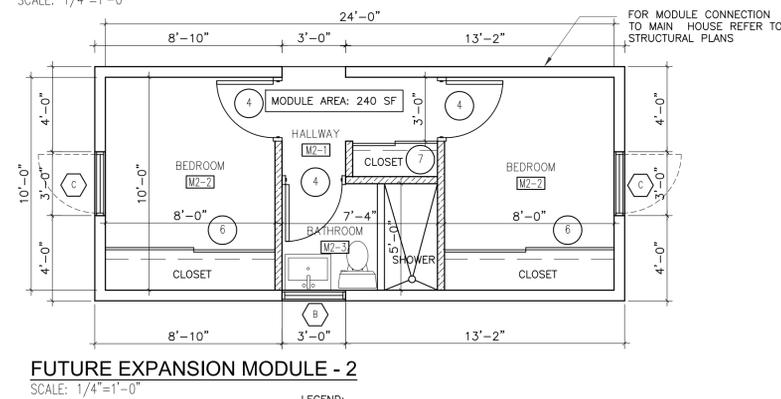
FOR MODULE CONNECTION TO MAIN HOUSE REFER TO STRUCTURAL PLANS

MAIN MODULE HOUSE-SECOND FLOOR
SCALE: 1/4"=1'-0"



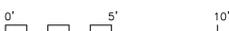
WOOD HOUSE ROOFING OPTIONS:
1. LIQUID APPLIED MEMBRANE
2. STANDING SEAM
3. GALVANIZED CORRUGATED PANELS
OWNER SHALL DECIDE WHAT SYSTEM TO BE USED IN THE WOOD CEILING. INSTALLATION TO BE AS PER MANUFACTURERS' INSTRUCTIONS.

ADDITION OPTION



FUTURE EXPANSION MODULE - 2
SCALE: 1/4"=1'-0"

- LEGEND:
- CONCRETE
 - REINFORCED MASONRY WALLS
 - STRUCTURAL WOOD WALL
 - SOLID GROUTED MASONRY WALLS



NOTE: FOR STRUCTURE DESIGN, FOOTINGS AND WALLS DESCRIPTION SEE STRUCTURAL PLANS

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (OPM-DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

ISSUE LOG

No.	Date	Description

PROFESSIONAL SEALS:

SHEET TITLE:

PROTOTYPE 4 - FLOOR PLANS & ELEVATIONS

SHEET INFORMATION:

JOB No.	Date Issued: 05/08/20
Drawn By:	Sheet Number:
Checked By:	A-400
QC Review:	
Phase:	

GENERAL NOTES

- ALL WORK SHALL BE DONE IN STRICT ACCORDANCE WITH ALL APPLICABLE LOCAL, STATE, AND FEDERAL BUILDING CODES AND/OR REGULATIONS.
- ALL WORK SHALL BE DONE IN A MANNER CONSISTENT WITH THE HIGHEST STANDARDS OF THE RESPECTIVE TRADES.
- THE CONTRACTOR SHALL VISIT THE SITE AND BECOME FAMILIAR WITH THE EXISTING CONDITIONS BEFORE BIDDING.
- THE CONTRACTOR SHALL VERIFY ALL FIELD DIMENSIONS BEFORE PROCEEDING WITH THE WORK AND COMPLIANCE WITH ZONING REGULATIONS.
- THE CONTRACTOR SHALL ABIDE BY ALL REQUIREMENTS OF THE OWNER WITH RESPECT TO CONSTRUCTION SCHEDULING, COORDINATION, TEMPORARY CONSTRUCTION, UTILITIES, ETC.
- THE CONTRACTOR SHALL NOT SCALE THESE CONSTRUCTION DOCUMENTS. IN THE EVENT THAT THE CONTRACTOR DOES SCALE THESE DOCUMENTS, IT SHALL BE AT THEIR OWN RISK.
- ALL MATERIALS, PRODUCTS, AND UNITS, SHALL BE INSTALLED PER MANUFACTURER'S RECOMMENDATIONS AND INSTRUCTIONS.
- INSTALLATION OF ALL MATERIALS AND/OR UNITS TO BE SELECTED BY, SUPPLIED BY, AND/OR INSTALLED BY THE OWNER SHALL BE SCHEDULED AND COORDINATED BY THE CONTRACTOR TO MAINTAIN THE CONSTRUCTION SCHEDULE. PRIOR TO THE COMMENCEMENT OF THE WORK, THE CONTRACTOR SHALL NOTIFY THE OWNER OF ALL QUANTITIES OF OWNER SUPPLIED MATERIALS AND/OR UNITS NOT SPECIFICALLY CALLED OUT IN THESE CONSTRUCTION DOCUMENTS. THE CONTRACTOR SHALL NOTIFY THE OWNER OF REQUIRED DELIVERY DATES OF OWNER SUPPLIED MATERIALS AND UNITS.
- ALL FINISH PAINT SHALL BE APPLIED OVER A COMPATIBLE FACTORY OR FIELD APPLIED PRIMER.
- THE CONTRACTOR SHALL PROTECT ALL EXISTING AND ADJACENT AREAS AT ALL TIMES DURING CONSTRUCTION. ANY AREA DAMAGED OR AFFECTED BY CONSTRUCTION SHALL BE PATCHED, REPAIRED, OR REPLACED AS REQUIRED TO MATCH EXISTING OR ADJACENT AREAS AT THE CONTRACTOR'S EXPENSE.
- THE CONTRACTOR SHALL YIELD TO THE OWNER AND THEIR VISITORS AT ALL TIMES.
- THE CONTRACTOR SHALL NOT DISRUPT THE BUILDING OR OPERATIONS WITHOUT PRIOR SCHEDULING AND APPROVAL FROM THE OWNER.
- NOT USED
- IF A CONFLICT OCCURS ON THESE CONSTRUCTION DOCUMENTS AND/OR THE SPECIFICATIONS, THE CONTRACTOR SHALL BID THE HIGHER QUALITY AND/OR QUANTITY.
- AIR CONDITIONING NOT INCLUDED. HOUSE OWNER SHALL DECIDE IF REQUIRED AND INSTALLATION WILL BE DONE BY OTHERS AFTER HOUSE IS BUILT.
- ALL WORK THAT IS EITHER IMPLIED OR REASONABLY INFERRED BY THE CONTRACT DOCUMENTS, DRAWINGS, AND SPECIFICATIONS SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.
- ALL DRAWINGS ARE DIRECTED TO THE ATTENTION OF THE CONTRACTOR, AND THE INCLUSION OF ANY WORK BY MENTION, NOTE, DETAIL, OR IMPLICATION, HOWEVER BRIEF, MEANS THAT THE CONTRACTOR SHALL PROVIDE AND INSTALL THE SAME.
- ALL WORK PERFORMED SHALL INCLUDE ALL APPURTENANCES AND APPARATUS NORMALLY DEEMED TO BE PART OF A COMPLETE PACKAGE WITHIN THE DEFINITIONS OF NORMAL INDUSTRY STANDARDS.
- ALL DIMENSIONS ARE CLEAR (FINISH TO FINISH). ALL FINAL DIMENSIONS AND LAYOUT SHALL BE VERIFIED WITH AND APPROVED BY THE OWNER AS REQUIRED BEFORE PROCEEDING WITH THE WORK.
- ROOF WATERPROOFING TO BE LIQUID APPLIED MEMBRANE SYSTEM ON CONCRETE ROOFS, OR STANDING SEAM OR GALVANIZED CORRUGATED PANELS. ALL ROOFING DESIGNS BY OTHERS.
- ONE BEDROOM WINDOW SHOULD BE CASEMENT TYPE JALOUSIE TO SWING IN THE DIRECTION OF EGRESS PER CODE
- NOT USED
- THE CONTRACTOR ASSUMES RESPONSIBILITY FOR CONSTRUCTION MEANS, METHODS, MATERIALS, TECHNIQUES, PROCEDURES, SEQUENCES, OR SCHEDULING IN CONNECTION WITH THIS WORK.
- NOT USED
- THE CONTRACTOR SHALL REMOVE ALL RUBBISH AND WASTE MATERIAL PERIODICALLY AND KEEP THE JOB SITE BROOM CLEAN AT ALL TIMES. ALL WASTE MATERIAL SHALL BE DISPOSED OF PROPERLY.
- ALL MECHANICAL, ELECTRICAL, PLUMBING FIXTURES AND EQUIPMENT SHOWN IN THE ARCHITECTURAL CONSTRUCTION DOCUMENTS, ARE SHOWN FOR LOCATION PURPOSES ONLY. ALL SPECIFICATIONS, ETC. SHALL BE PROVIDED UNDER SEPARATE COVER.

SAFE ROOM NOTES

SAFE ROOM SIZE SHOWN IN THIS PLAN SET IS BASED UPON A 7 PERSON OCCUPANCY. PER FEMA P-320 REQUIREMENTS 7 S.F. OF SPACE IS REQUIRED PER OCCUPANT. FOR VARYING OCCUPANCY REQUIREMENTS CONFIRM SAFE ROOM SIZE REQUIREMENTS WITH FEMA P-320, FEMA 361, AND ICC 500.

SEE FEMA P-361 AND ICC-500 FOR ADDITIONAL SAFE ROOM REQUIREMENTS SUCH AS FIRST AID KITS, OPERATION, AND MAINTENANCE REQUIREMENTS. ONCE THE SAFE ROOM IS CONSTRUCTED IT SHOULD BE REGISTERED WITH LOCAL FIRST RESPONDERS (E.G., POLICE, FIRE, RESCUE ORGANIZATIONS).

NOT ALL SAFE ROOM OPENINGS ARE SHOWN IN THESE DRAWINGS. ESTABLISH AND VERIFY ALL OPENINGS AND INSERTS FOR MECHANICAL, PLUMBING, AND ELECTRICAL WITH APPROPRIATE TRADES, DRAWINGS, AND SUBCONTRACTORS PRIOR TO CONSTRUCTION. OPENINGS MAY REQUIRE ADDITIONAL REINFORCING OR SUPPORTS AS SHOWN ON TYPICAL DETAILS. OPENINGS NEED TO BE PROTECTED PER ICC 500.

COMPLETE SAFE ROOM INSPECTION REQUIREMENTS SHALL BE AS DIRECTED BY THE LOCAL BUILDING DEPARTMENT.

SAFE ROOM VENTILATION IS TO BE PROVIDED. VERIFY SIZE REQUIREMENTS BASED ON SAFE ROOM SIZE, OCCUPANCY, AND ICC 500 SPECIFICATIONS. CONSULT LOCAL BUILDING OFFICIAL AND REFER TO ICC 500-14 FOR VENTILATION OPENING PROTECTION.

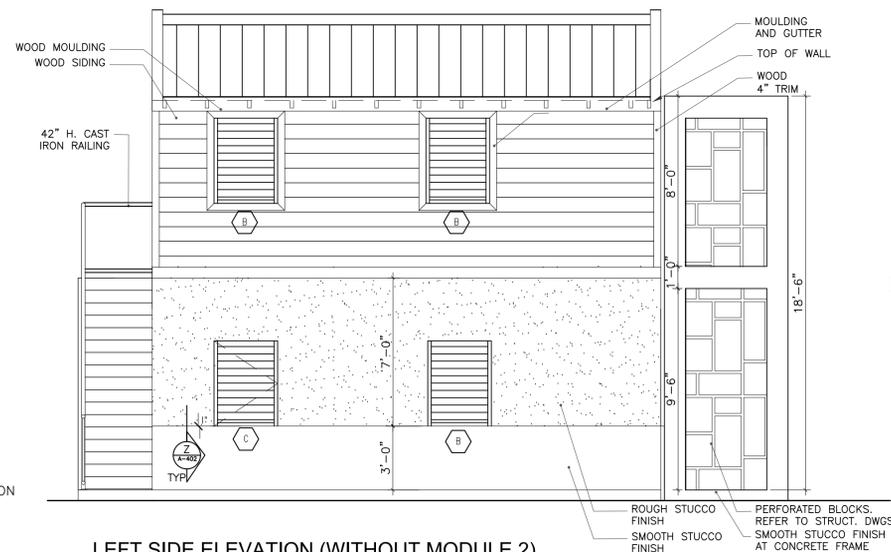
THE SELECTED DOOR AND WINDOW PROTECTION SHALL MEET THE DESIGN CRITERIA OF 2015 FEMA P-361 AND 2014 ICC-500. ALL DOORS AND WINDOW PROTECTIONS SHALL BE A TESTED ASSEMBLY AND INSTALLED PER MANUFACTURER'S RECOMMENDATIONS.

① OWNER HAS THE OPTION TO ELIMINATE SAFE ROOM WINDOW IF THIS ROOM WILL NEVER BE USED AS A BEDROOM.



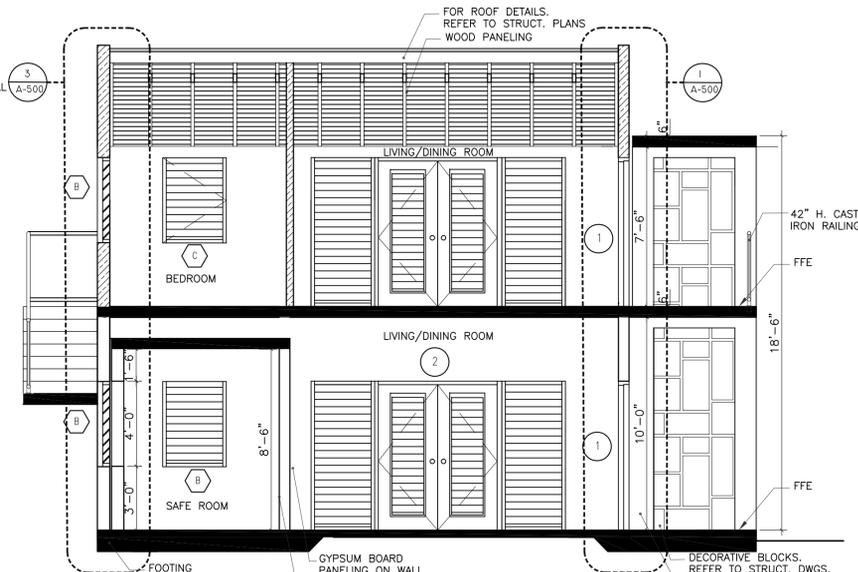
RIGHT SIDE ELEVATION (WITHOUT MODULE 1)

SCALE: 1/4"=1'-0"



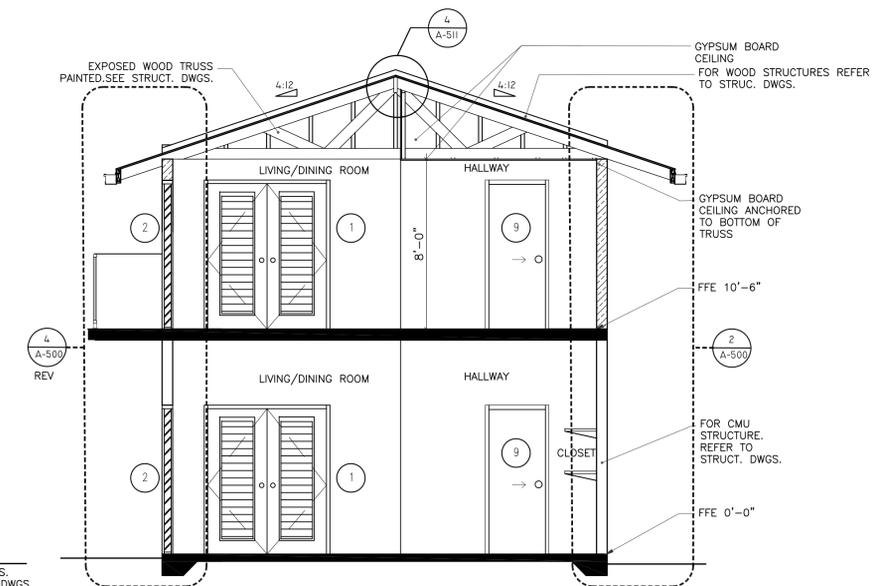
LEFT SIDE ELEVATION (WITHOUT MODULE 2)

SCALE: 1/4"=1'-0"



SECTION A-A

SCALE: 1/4"=1'-0"



SECTION B-B

SCALE: 1/4"=1'-0"

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

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ISSUE LOG

No.	Date	Description

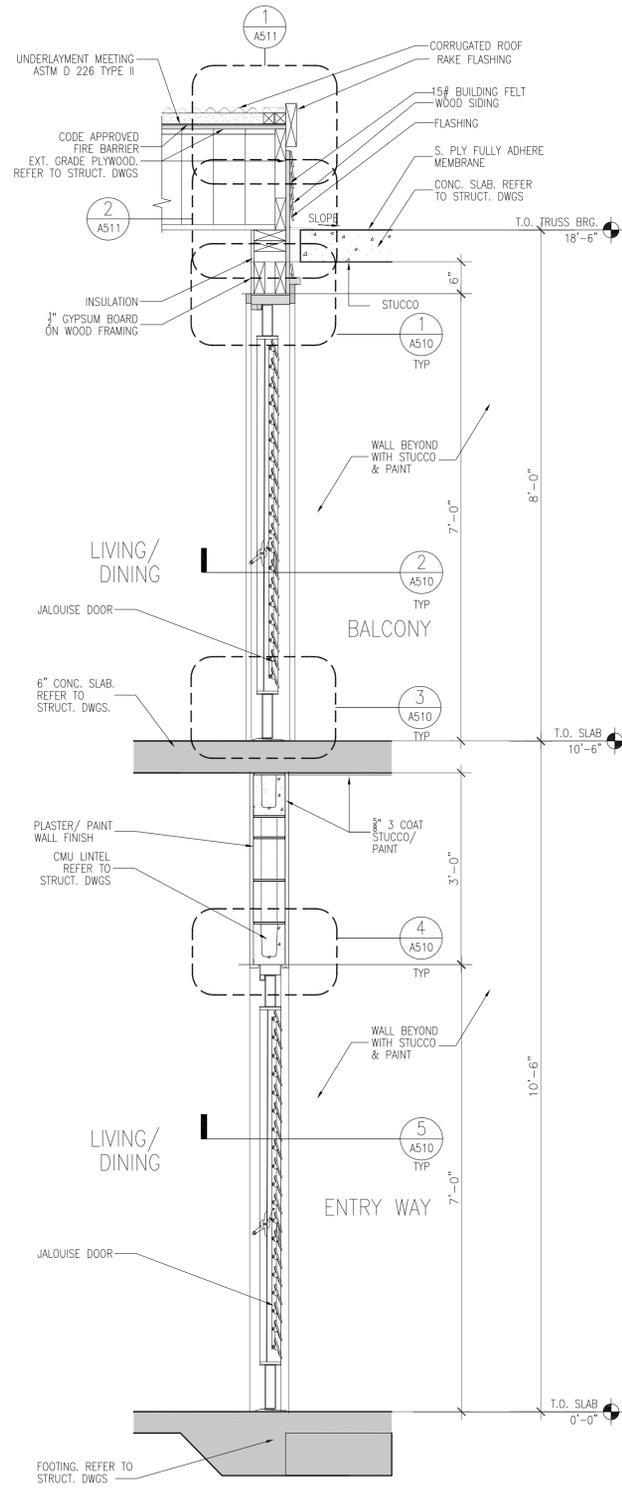
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SHEET TITLE:

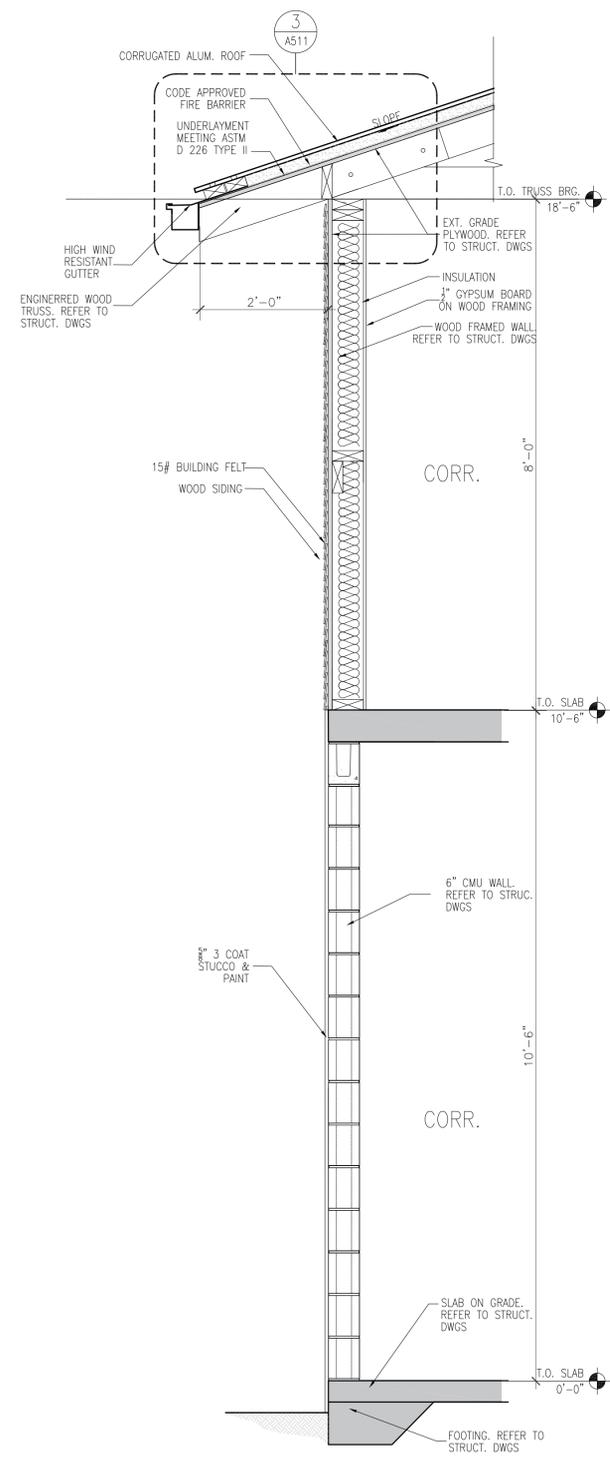
PROTOTYPE 4 - SECTIONS & ELEVATIONS

SHEET INFORMATION:

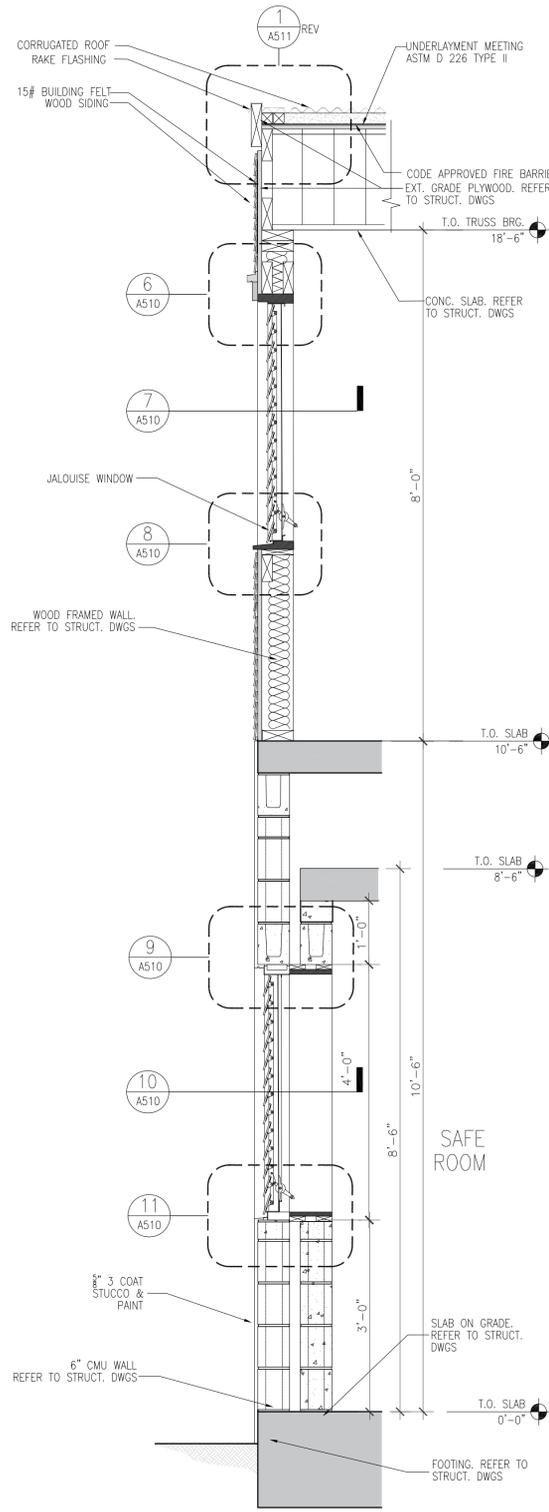
JOB No.	Date Issued: 05/08/20
Drawn By:	Sheet Number:
Checked By:	A-401
QC Review:	
Phase:	



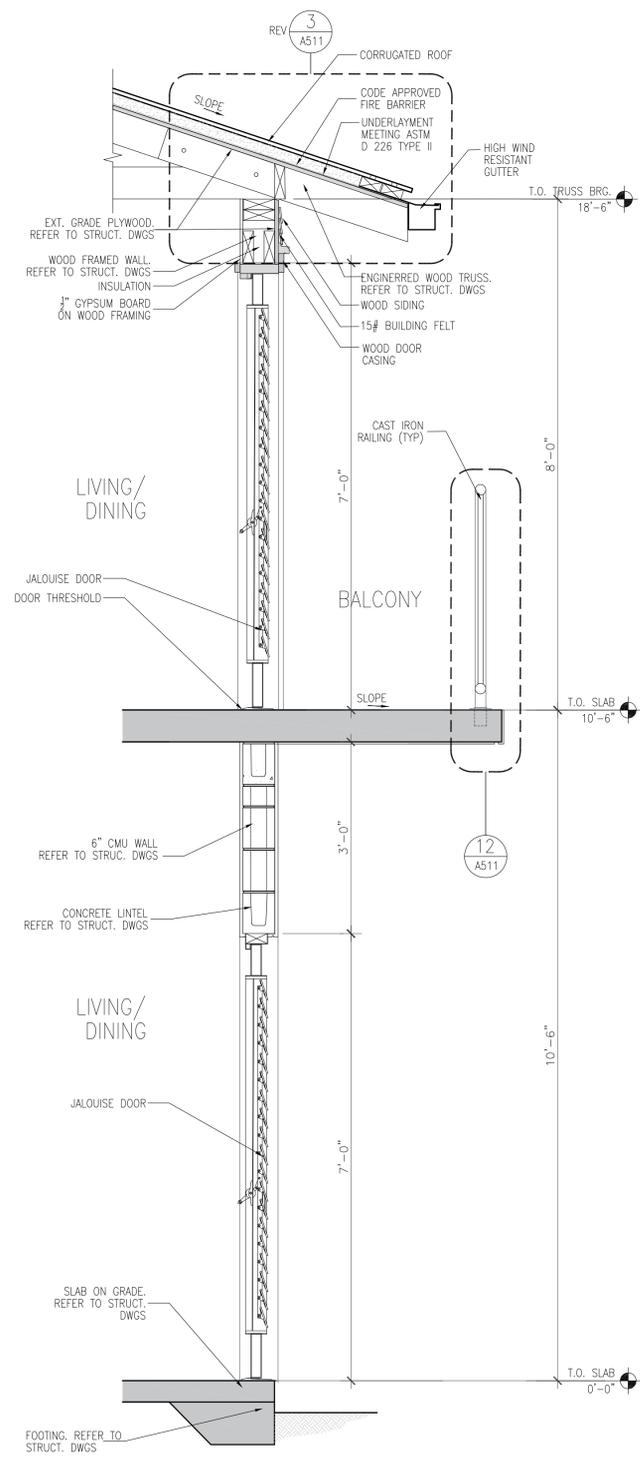
1 WALL SECTION
SCALE: 3/4" = 1'-0"



2 WALL SECTION
SCALE: 3/4" = 1'-0"



3 WALL SECTION
SCALE: 3/4" = 1'-0"



4 WALL SECTION
SCALE: 3/4" = 1'-0"

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

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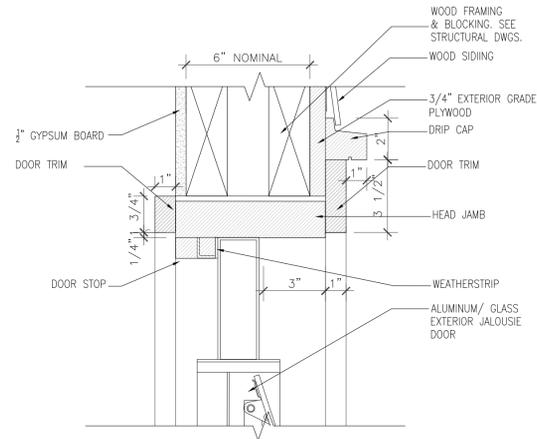
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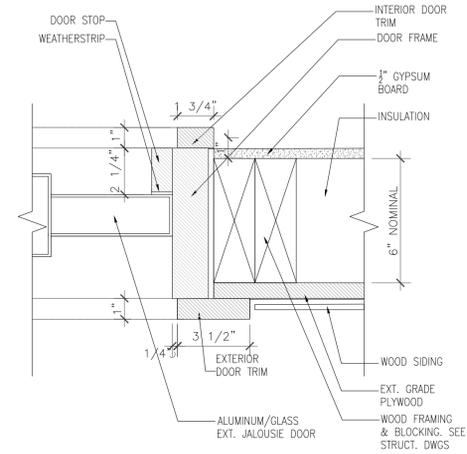
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**PROTOTYPE #4
WALL SECTIONS**

SHEET INFORMATION:

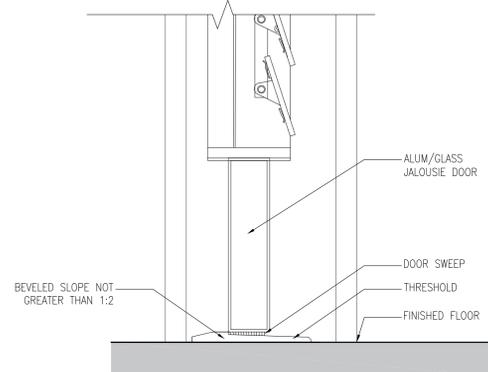
JOB No.	Date Issued: 05/08/20
Drawn By:	Sheet Number:
Checked By:	A-500
QC Review:	
Phase:	



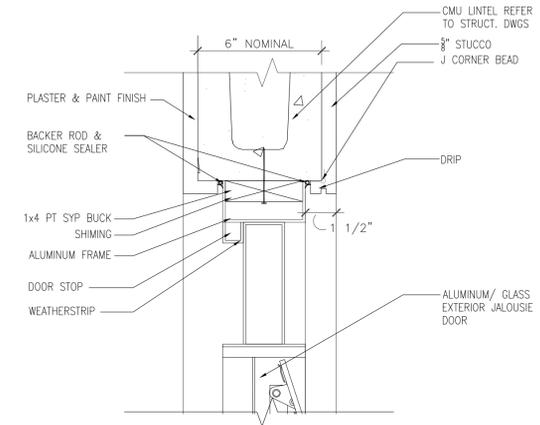
1 SECTION DETAIL-DOOR HEADER-WOOD WALL FRAME
SCALE: 3" = 1'-0"



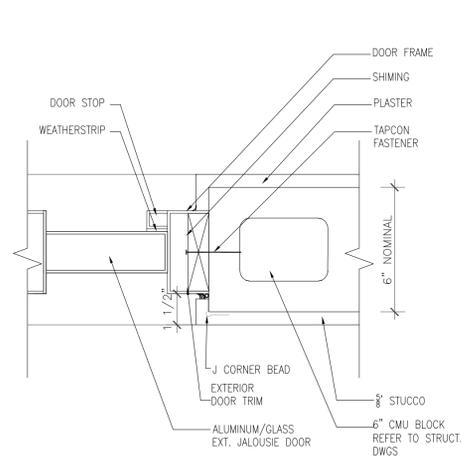
2 SECTION DETAIL-DOOR JAMB-WOOD WALL FRAME
SCALE: 3" = 1'-0"



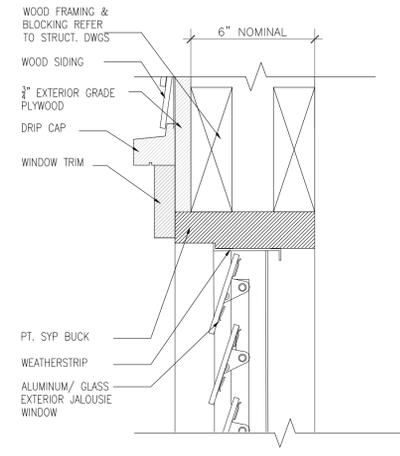
3 SECTION DETAIL-DOOR THRESHOLD-CONC. FLOOR
SCALE: 3" = 1'-0"



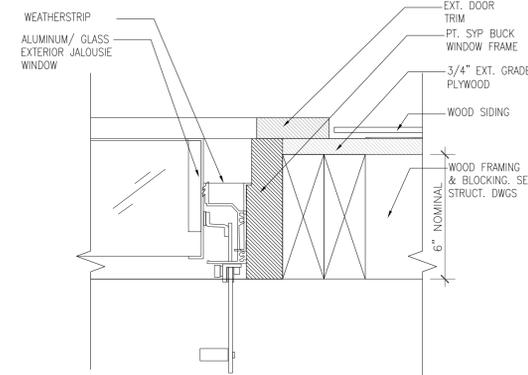
4 SECTION DETAIL-DOOR HEADER-CMU WALL
SCALE: 3" = 1'-0"



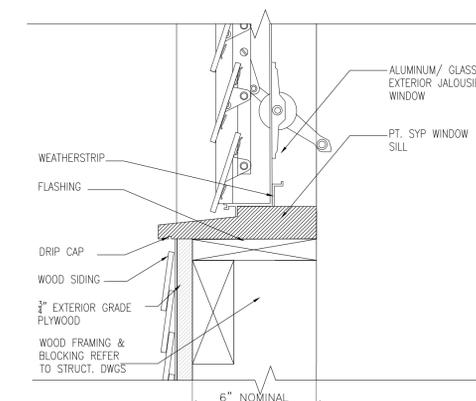
5 SECTION DETAIL-DOOR JAMB-CONC WALL
SCALE: 3" = 1'-0"



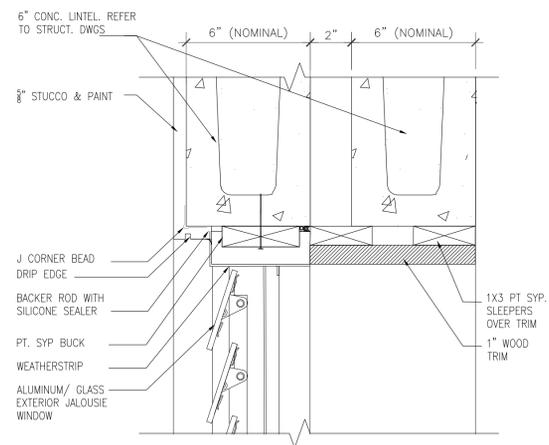
6 SECTION DETAIL-WINDOW HEADER-WOOD WALL FRAME
SCALE: 3" = 1'-0"



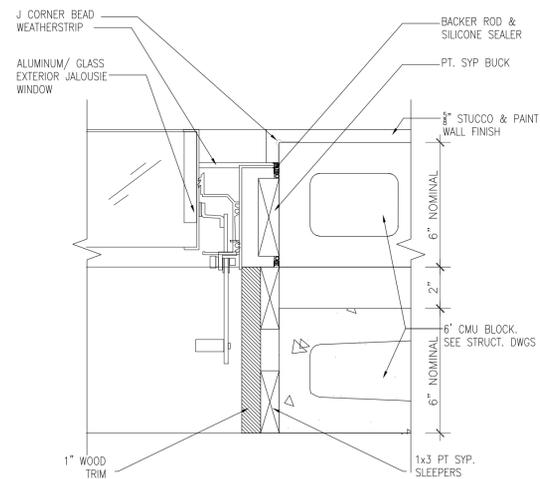
7 SECTION DETAIL-WINDOW JAMB-WOOD WALL FRAME
SCALE: 3" = 1'-0"



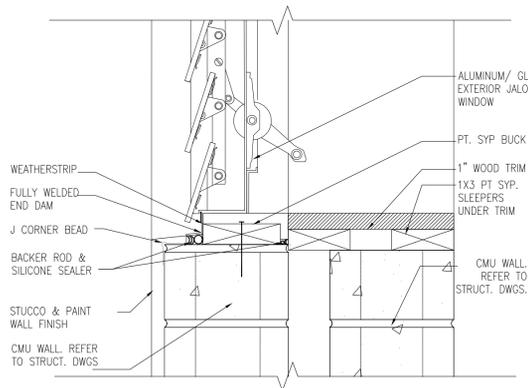
8 SECTION DETAIL-WINDOW SILL-WOOD WALL FRAME
SCALE: 3" = 1'-0"



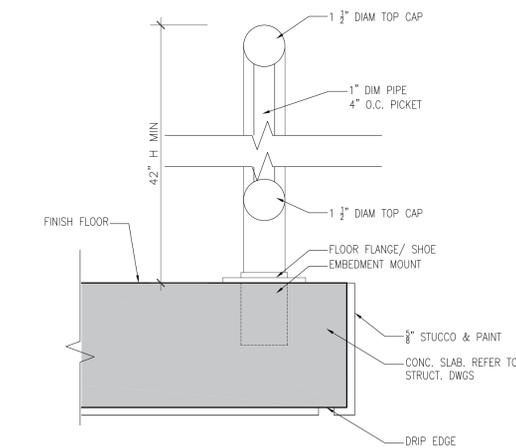
9 SECTION DETAIL-WINDOW HEADER-CONC. WALL
SCALE: 3" = 1'-0"



10 SECTION DETAIL-WINDOW JAMB-CONC. WALL
SCALE: 3" = 1'-0"



11 SECTION DETAIL-WINDOW SILL-CONC. WALL
SCALE: 3" = 1'-0"



12 SECTION DETAIL-CAST IRON RAILING
SCALE: 3" = 1'-0"

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

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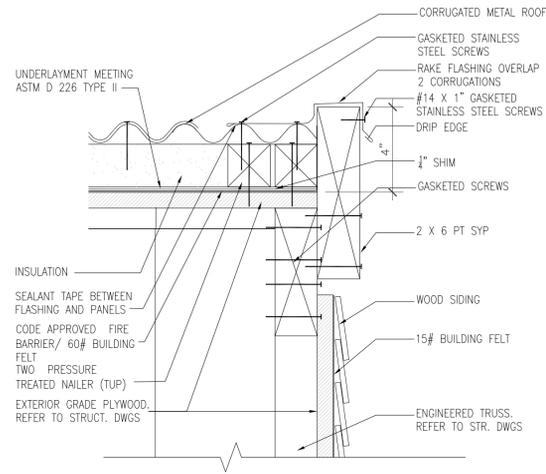
ISSUE LOG

No.	Date	Description

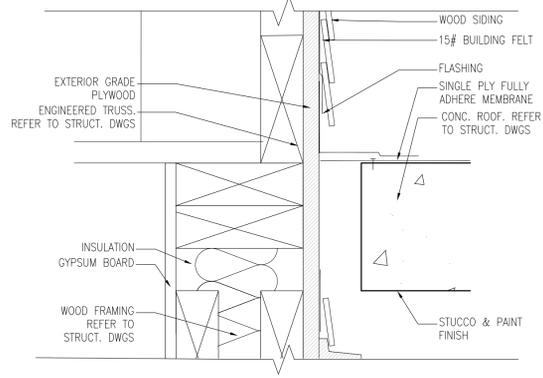
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SHEET TITLE: PROTOTYPE #4-DETAILS DOORS AND WINDOWS

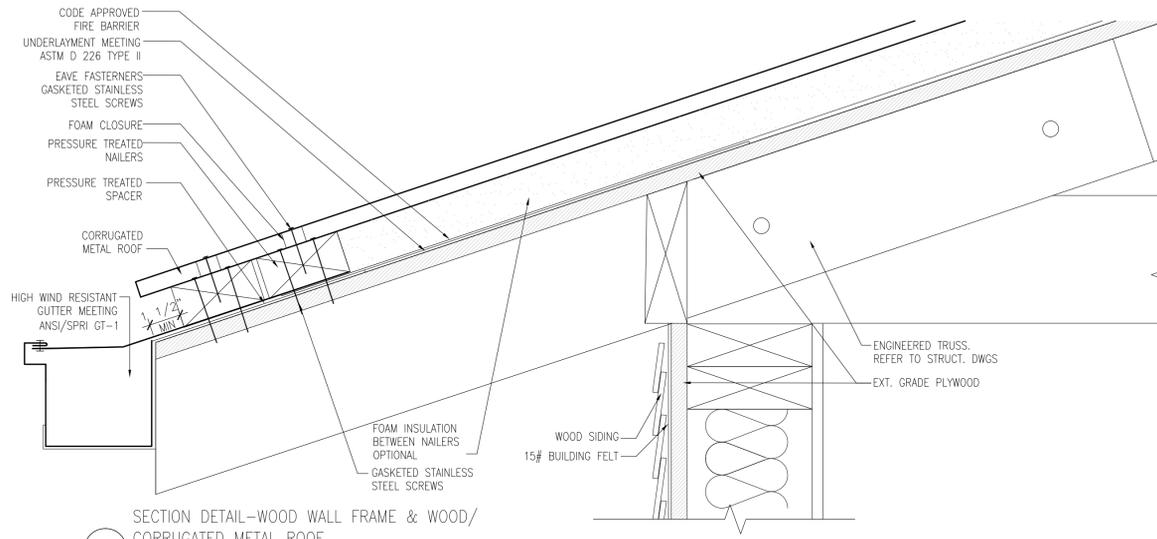
SHEET INFORMATION:	
JOB No.	Date Issued: 05/08/20
Drawn By:	Sheet Number:
Checked By:	A-510
QC Review:	
Phase:	



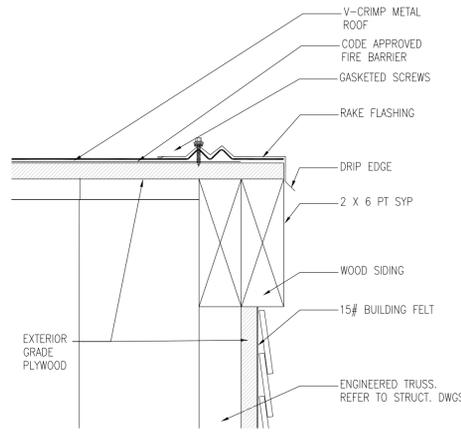
1 SECTION DETAIL—RAKE—WOOD/ CORRUGATED METAL ROOF
SCALE: 3" = 1'-0"



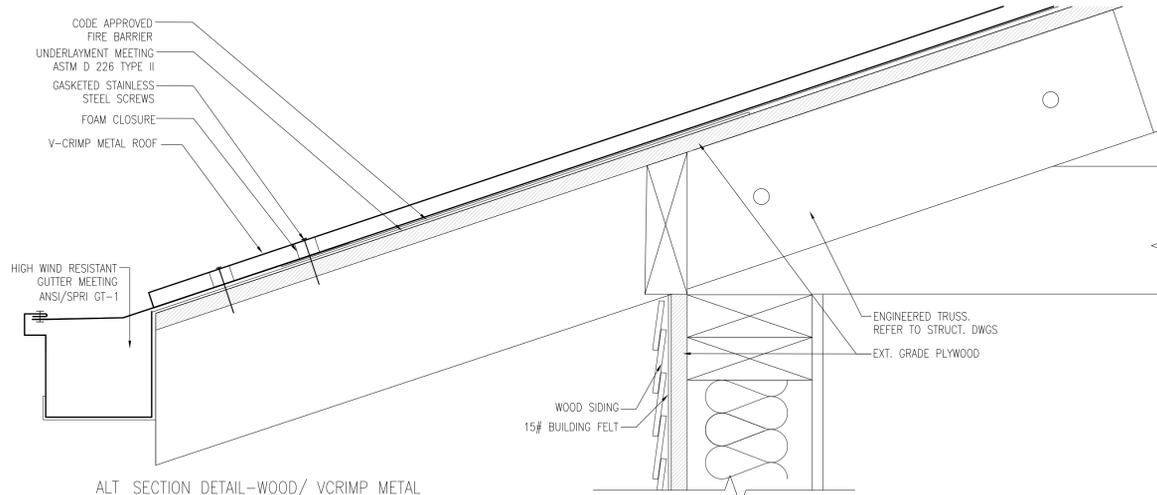
2 SECTION DETAIL—WOOD WALL / CONC. ROOF JOINT
SCALE: 3" = 1'-0"



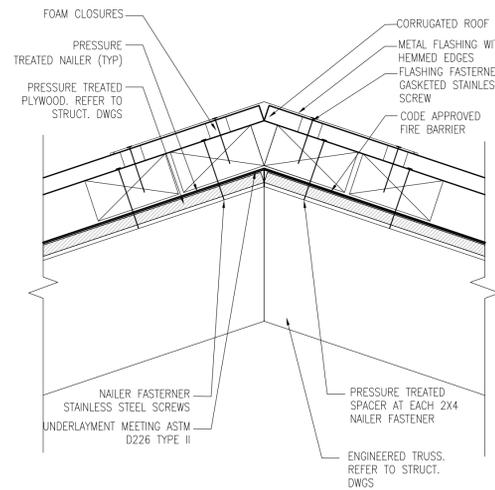
3 SECTION DETAIL—WOOD WALL FRAME & WOOD/ CORRUGATED METAL ROOF
SCALE: 3" = 1'-0"



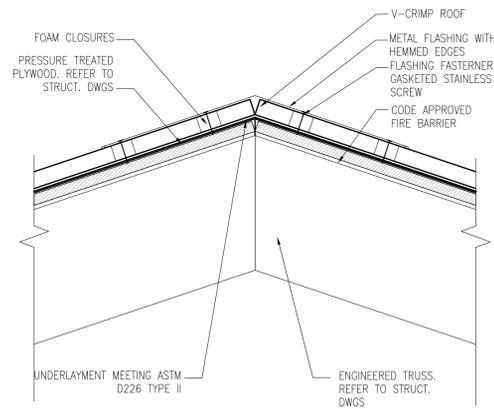
ALT 1 SECTION DETAIL—RAKE—WOOD/ V-CRIMP METAL ROOF
SCALE: 3" = 1'-0"



ALT 3 SECTION DETAIL—WOOD/ VCRIMP METAL ROOF—SCUPPER
SCALE: 3" = 1'-0"



4 SECTION DETAIL AT ROOF RIDGE—CORRUGATED METAL ROOF
SCALE: 3" = 1'-0"



ALT 4 SECTION DETAIL AT ROOF RIDGE—V-CRIMP METAL ROOF
SCALE: 3" = 1'-0"

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

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No.	Date	Description

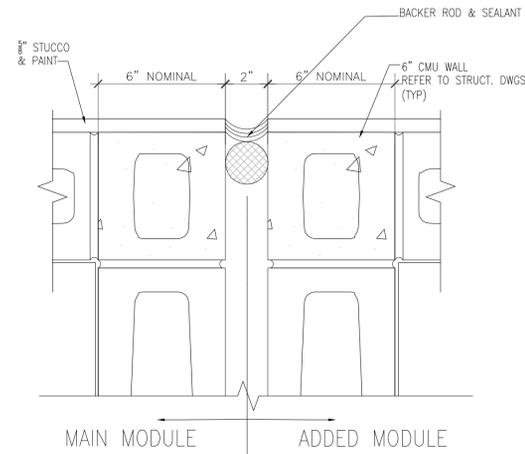
PROFESSIONAL SEALS:

SHEET TITLE:

PROTOTYPE #4 ROOF DETAILS

SHEET INFORMATION:

JOB No.	Date Issued: 05/08/20
Drawn By:	Sheet Number:
Checked By:	A-511
QC Review:	
Phase:	



1 SECTION DETAIL—MAIN AND NEW MODULE JOINT
 CMU WALLS
 SCALE: 3" = 1'-0"

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
 CMU AND 2ND FL.
 WOOD HOME**

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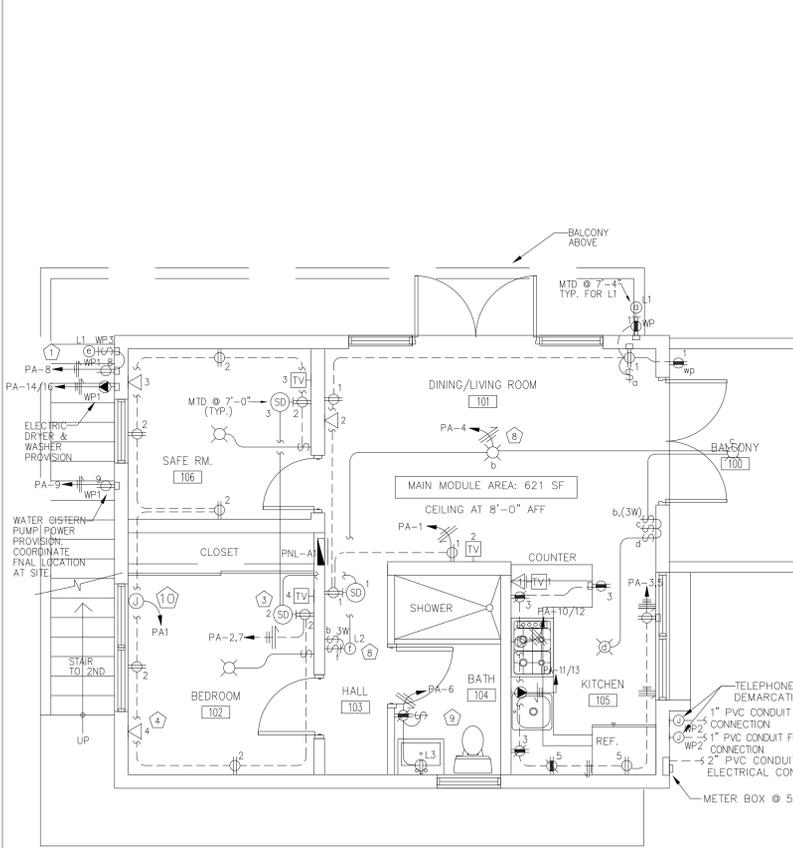
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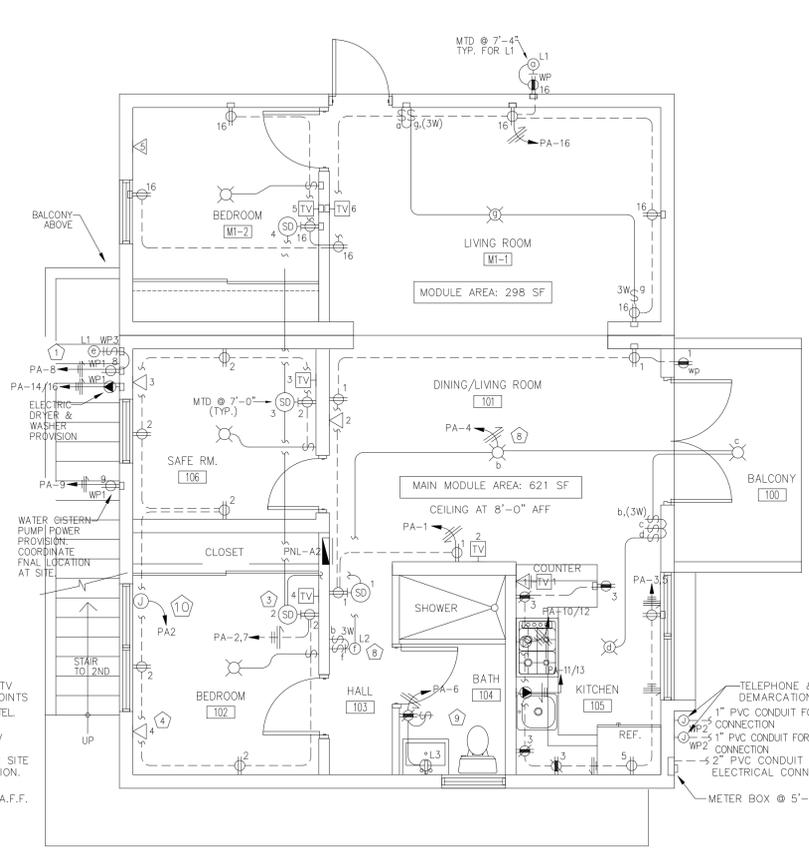
SHEET TITLE:
**PROTOTYPE #4
 MODULES JOINT DETAILS**

SHEET INFORMATION:

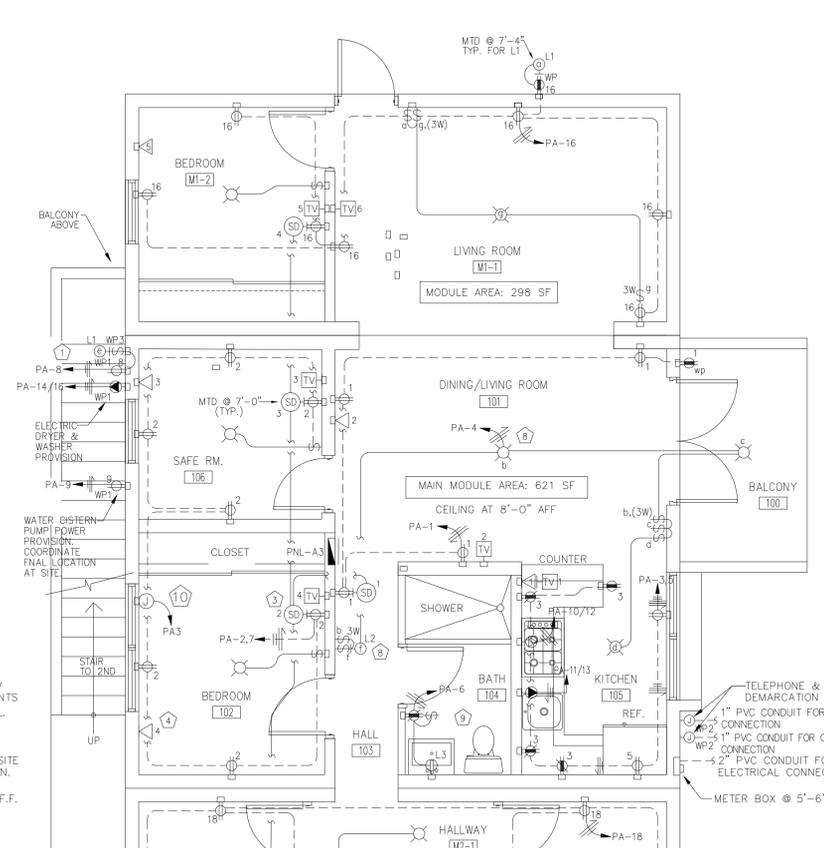
JOB No.	Date Issued: 05/08/20
Drawn By:	Sheet Number:
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QC Review:	
Phase:	



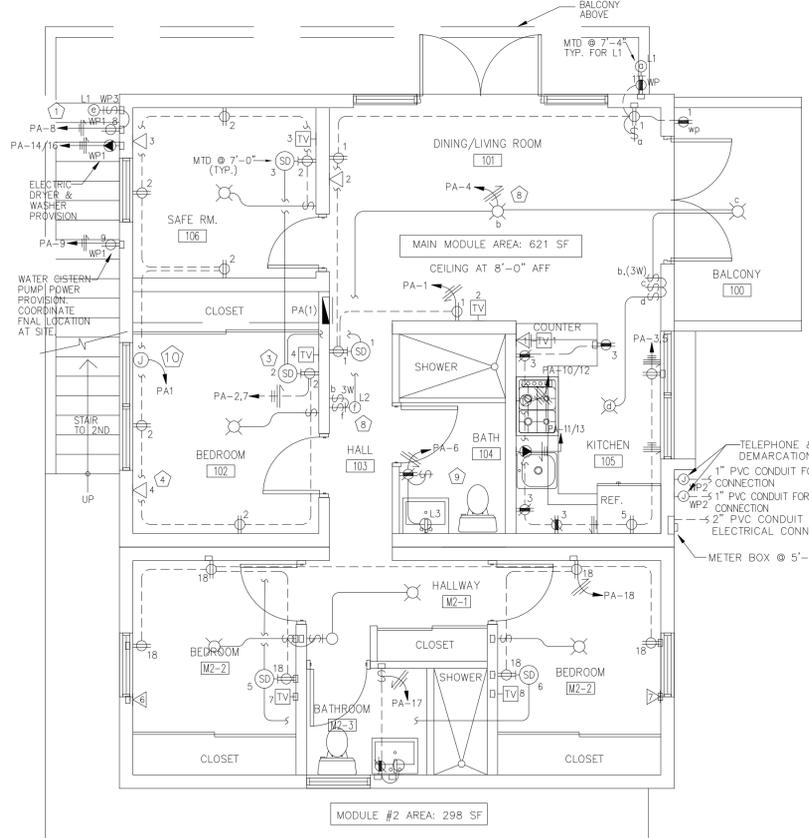
MAIN MODULE HOUSE
SCALE: 1/4"=1'-0"



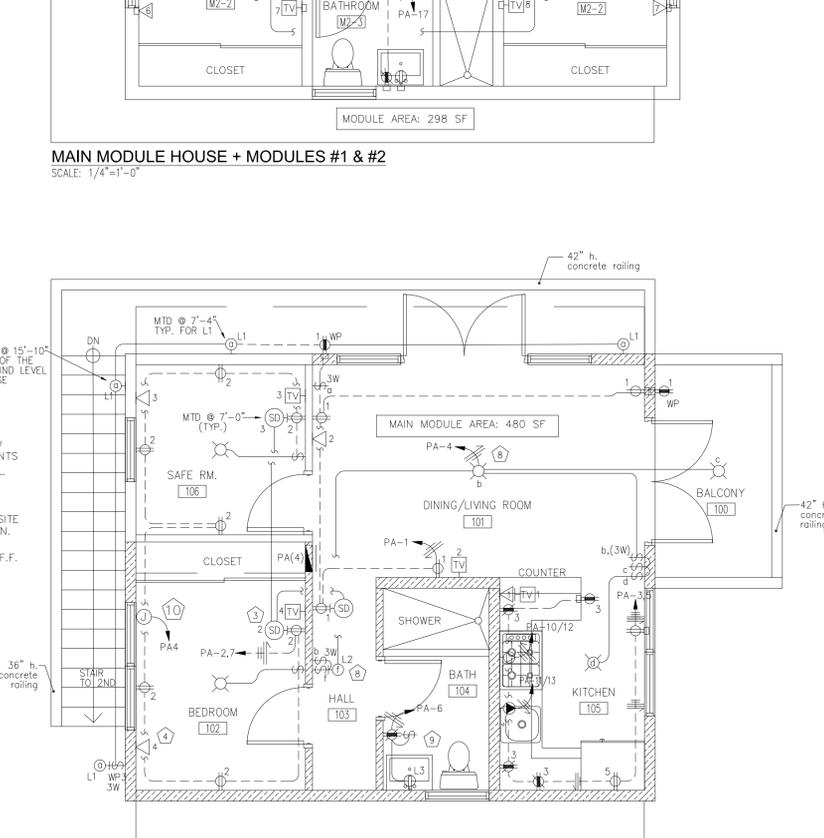
MAIN MODULE HOUSE + MODULE #1
SCALE: 1/4"=1'-0"



MAIN MODULE HOUSE + MODULES #1 & #2
SCALE: 1/4"=1'-0"



MAIN MODULE HOUSE + MODULE #2
SCALE: 1/4"=1'-0"



MAIN MODULE HOUSE-SECOND FLOOR
SCALE: 1/4"=1'-0"

- LEGEND:**
- CONCRETE
 - ▭ STRUCTURAL WALLS (CMU)
 - ▨ STRUCTURAL WOOD WALL
- NOTE: FOR STRUCTURE DESIGN SEE STRUCTURAL PLANS

- NOTES:**
- 1 WASHER AND DRYER AREA RECEPTACLES LOCATED @ 48" A.F.F. (COORDINATE FINAL LOCATION WITH FIELD ENGINEER.)
 - 2 NOT USED
 - 3 ALL DETECTORS MUST BE CONNECTED BETWEEN EACH OTHER FOR PARALLEL ACTIVATION.
 - 4 COORDINATE WITH ARCHITECT OR FIELD ENGINEER THE FINAL LOCATION FOR ALL TELEPHONE AND CTV OUTLETS (TYPICAL).
 - 5 VANITY LIGHTS OUTLETS. COORDINATE FINAL HEIGHT WITH ARCHITECT.
 - 6 COORDINATE WITH ARCHITECT OR FIELD ENGINEER THE FINAL HEIGHT FOR LIGHTING FIXTURE.
 - 7 NOT USED
 - 8 ALL INDOOR & OUTDOOR LIGHTING FIXTURES ARE TO BE PORCELAIN LAMP HOLDERS WITH 26 WATTS FLUORESCENT BULBS OR LED EQUIVALENTS.
 - 9 INTERLOCK FAN WITH BATHROOM LIGHTING SWITCH. COORDINATED WITH MECHANICAL DWGS.
 - 10 4"x4" JUNCTION BOX FOR A/C UNIT DEDICATED RECEPTACLE. INSTALL EMPTY CONDUIT UP TO PANEL BOARD PA. RECEPTACLE, WIRING AND BREAKER (N.I.C.).

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DEEC), PERMITS MANAGEMENT OFFICE (DOP-DEEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DEEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

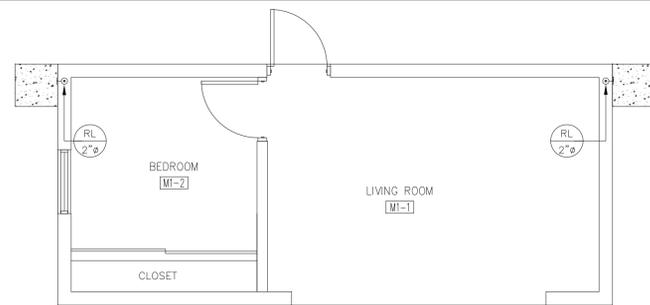
No.	Date	Description

ISSUE LOG
PROFESSIONAL SEALS:

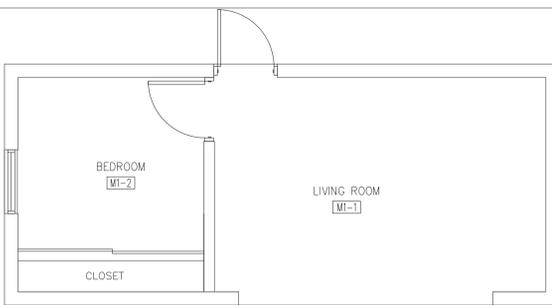
SHEET TITLE:
**PROTOTYPE #4 SCHEMATIC - TWO
STORY, CONC. & WOOD STRUCTURE &
WOOD GABLE ROOF**

SHEET INFORMATION:	
JOB No.	Date Issued: 05/08/2020
Drawn By:	Sheet Number:
Checked By:	E-400
QC Review:	
Phase:	

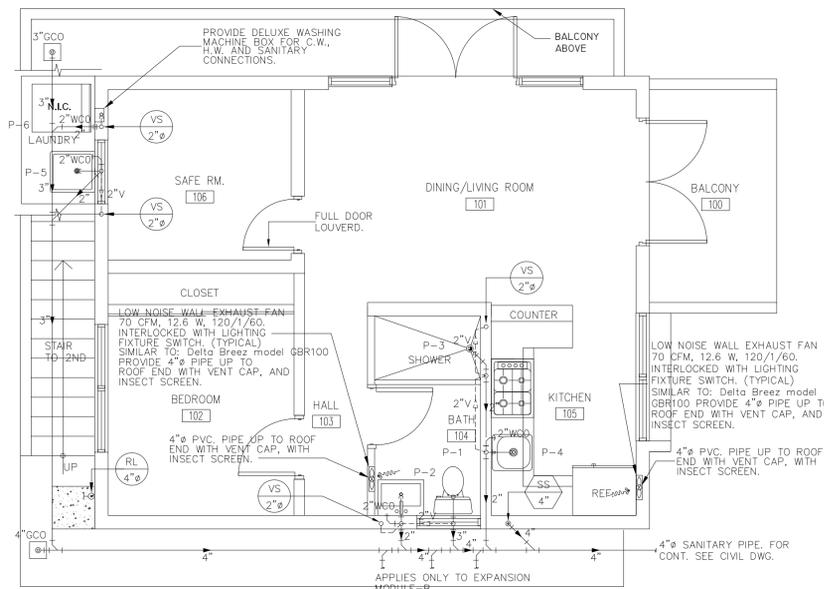
NOT FOR CONSTRUCTION



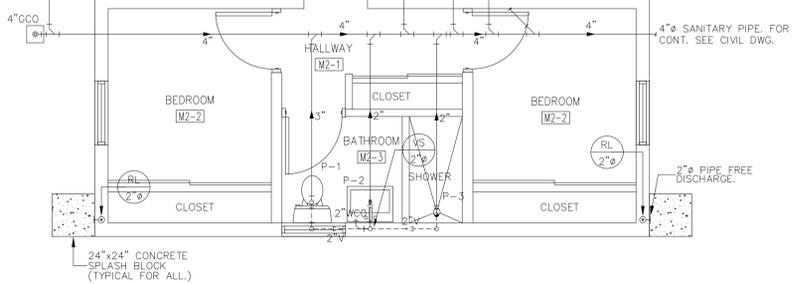
EXPANSION MODULE - A
FLOOR PLAN- SANITARY LAYOUT
SCALE: 1/4"=1'-0"



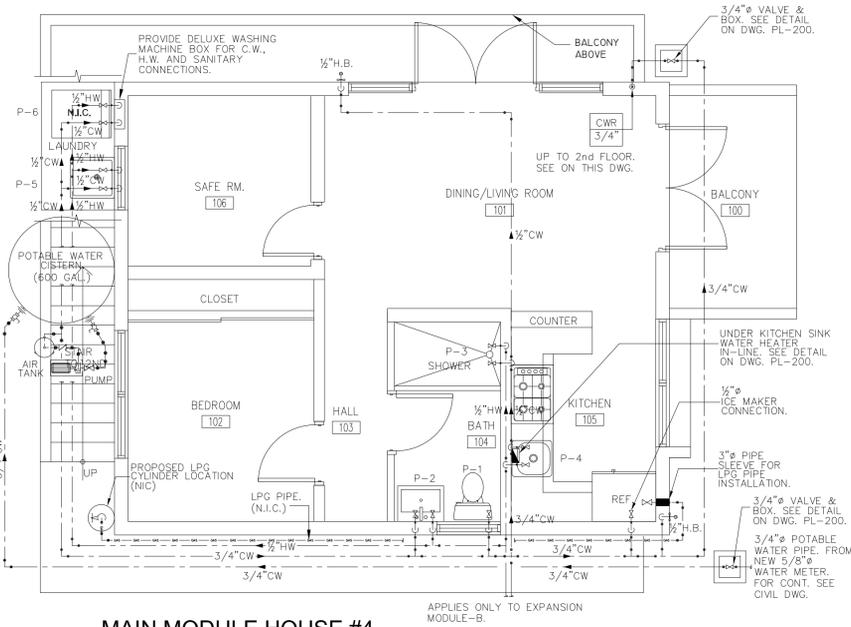
EXPANSION MODULE - A
FLOOR PLAN- POTABLE WATER LAYOUT
SCALE: 1/4"=1'-0"



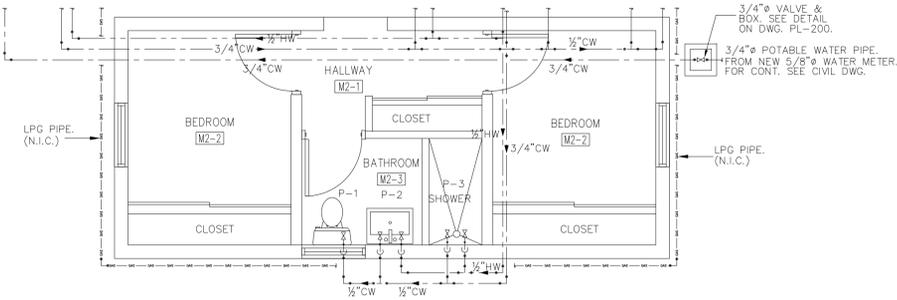
MAIN MODULE HOUSE #4
FLOOR PLAN- SANITARY LAYOUT
SCALE: 1/4"=1'-0"



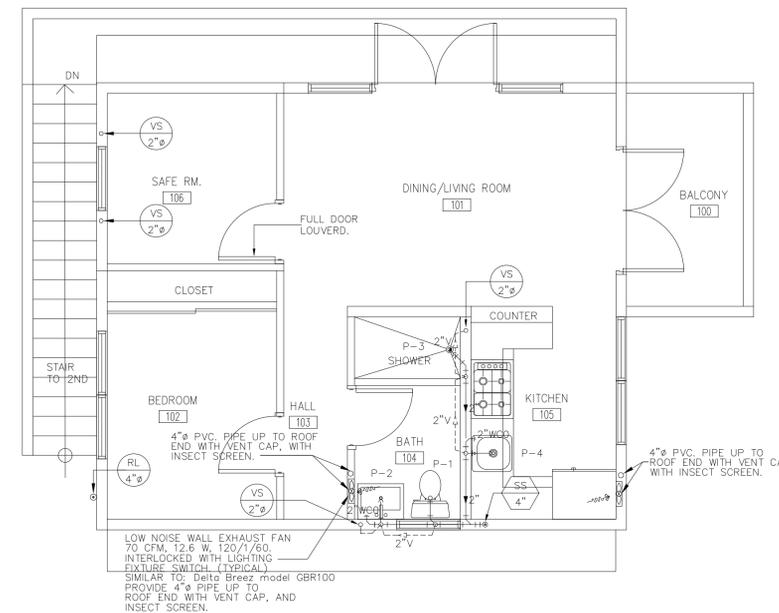
EXPANSION MODULE - B
FLOOR PLAN- SANITARY LAYOUT
SCALE: 1/4"=1'-0"



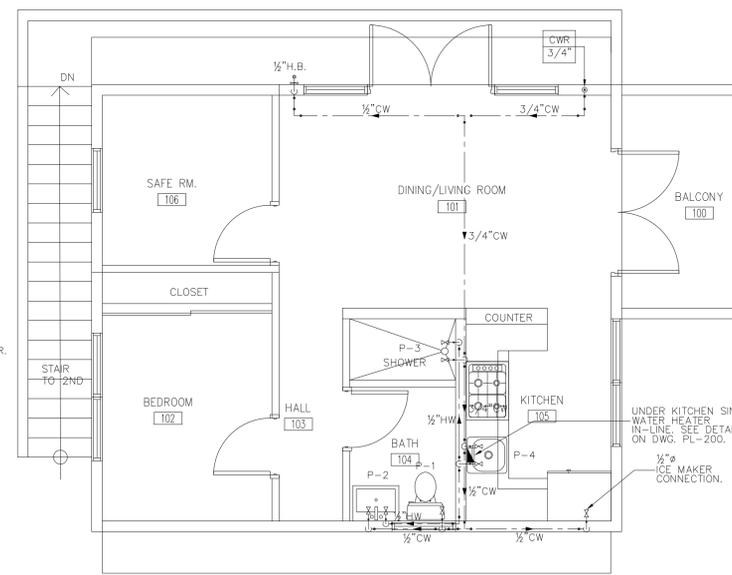
MAIN MODULE HOUSE #4
FLOOR PLAN- POTABLE WATER LAYOUT
SCALE: 1/4"=1'-0"



EXPANSION MODULE - B
FLOOR PLAN- POTABLE WATER LAYOUT
SCALE: 1/4"=1'-0"



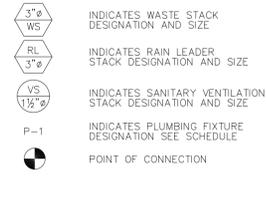
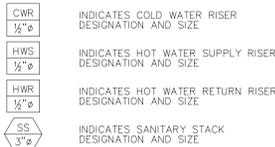
MAIN MODULE HOUSE #4
2nd FLOOR PLAN- SANITARY LAYOUT
SCALE: 1/4"=1'-0"



MAIN MODULE HOUSE #4
2nd FLOOR PLAN- POTABLE WATER LAYOUT
SCALE: 1/4"=1'-0"

PLUMBING LEGEND:

- COLD POTABLE WATER LINE
- HOT POTABLE WATER LINE
- SANITARY SEWER LINE
- SANITARY VENTILATION LINE



PLUMBING ABBREVIATIONS:

- C.W. COLD WATER
- HWS HOT WATER SUPPLY
- HWR HOT WATER RETURN
- (TYP.) TYPICAL
- VS VENT STACK
- WCO WALL CLEAN OUT
- FCO FLOOR CLEAN OUT
- GCO GROUND CLEAN OUT
- W.H. WATER HEATER
- FD FLOOR DRAIN
- V VENTILATION
- H.B. HOSE BIBB
- (E) EXISTING
- CC CEILING CASSETTE
- FCU FAN COIL UNIT

NOTE:

- 1) NON-POTABLE WATER SYSTEM IS NOT IN CONTRACT. CISTERN LOCATION SHOULD BE EVALUATED ACCORDING TO ACTUAL SITE CONDITIONS.
- 2) LPG SYSTEM IS NOT IN CONTRACT. INSTALLATION SHALL COMPLY WITH APPLICABLE CODES, REGULATIONS, STANDARDS AND "COMISION DE SERVICIO PUBLICO"

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DEEC), PERMITS MANAGEMENT OFFICE (DGR&DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DEEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

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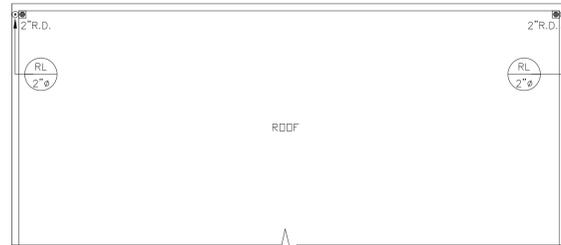
PROFESSIONAL SEALS:

SHEET TITLE:

PROTOTYPE #4 FLOOR PLAN- PLUMBING LAYOUT

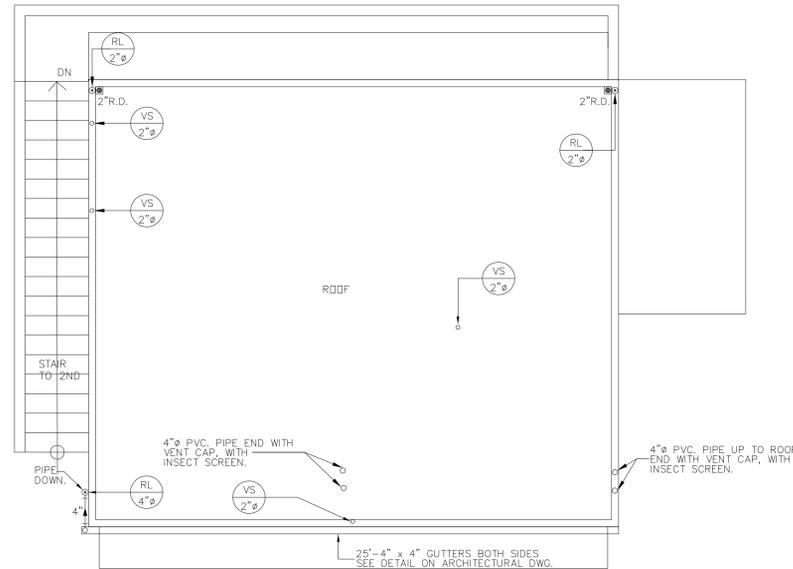
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JOB No.	Date Issued: 05/08/2020
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QC Review:	
Phase:	



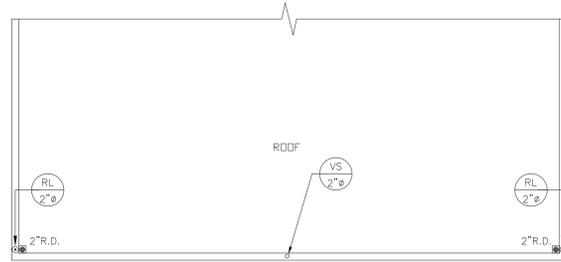
**EXPANSION MODULE - A
ROOF PLAN- PLUMBING LAYOUT**

SCALE: 1/4"=1'-0"



**MAIN MODULE HOUSE #4
ROOF PLAN- PLUMBING LAYOUT**

SCALE: 1/4"=1'-0"



**EXPANSION MODULE - B
ROOF PLAN- PLUMBING LAYOUT**

SCALE: 1/4"=1'-0"

PLUMBING LEGEND:

- COLD POTABLE WATER LINE
- HOT POTABLE WATER LINE
- SANITARY SEWER LINE
- SANITARY VENTILATION LINE
- CWR
1/2" 0 INDICATES COLD WATER RISER DESIGNATION AND SIZE
- HWS
1/2" 0 INDICATES HOT WATER SUPPLY RISER DESIGNATION AND SIZE
- HWR
1/2" 0 INDICATES HOT WATER RETURN RISER DESIGNATION AND SIZE
- SS
3" 0 INDICATES SANITARY STACK DESIGNATION AND SIZE
- 3" 0
WS INDICATES WASTE STACK DESIGNATION AND SIZE
- RL
3" 0 INDICATES RAIN LEADER STACK DESIGNATION AND SIZE
- VS
1 1/2" 0 INDICATES SANITARY VENTILATION STACK DESIGNATION AND SIZE
- P-1 INDICATES PLUMBING FIXTURE DESIGNATION SEE SCHEDULE
- POINT OF CONNECTION

PLUMBING ABBREVIATIONS:

- C.W. COLD WATER
- HWS HOT WATER SUPPLY
- HWR HOT WATER RETURN
- (TYP.) TYPICAL
- VS VENT STACK
- WCO WALL CLEAN OUT
- FCO FLOOR CLEAN OUT
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- W.H. WATER HEATER
- FD FLOOR DRAIN
- V VENTILATION
- H.B. HOSE BIBB
- (E) EXISTING
- CC CEILING CASSETTE
- FCU FAN COIL UNIT

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND FL.
WOOD HOME**

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (DPR-DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPERATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

No.	Date	Description

ISSUE LOG

PROFESSIONAL SEALS:

SHEET TITLE:

**PROTOTYPE #4
ROOF PLAN-
PLUMBING LAYOUT**

SHEET INFORMATION:

JOB No. _____ Date Issued: 05/08/2020

Drawn By: _____ Sheet Number: _____

Checked By: _____

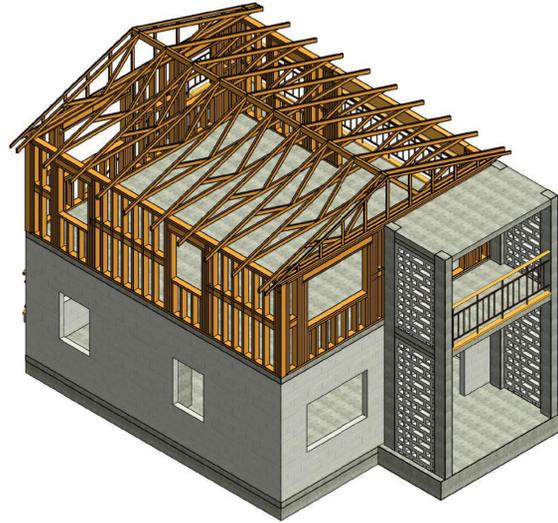
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Phase: _____

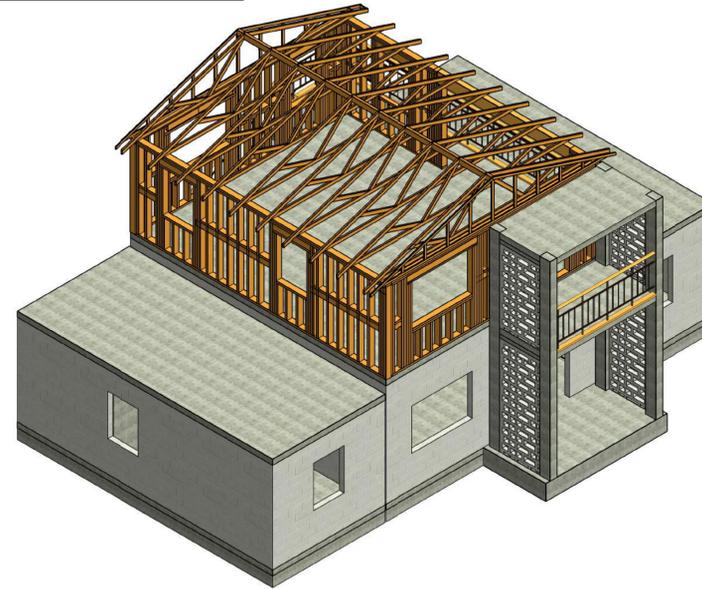
PL-104

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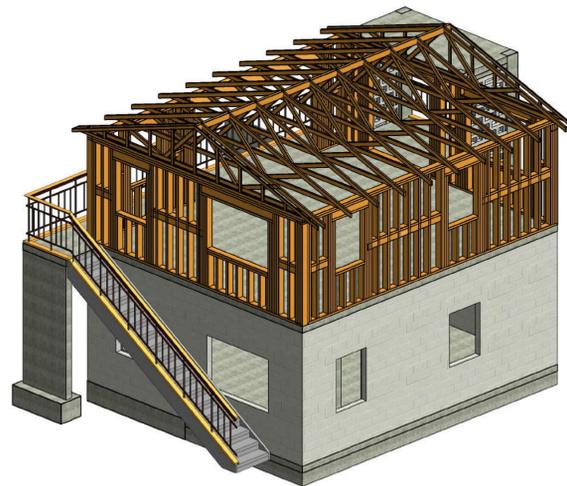
**PRESCRIPTIVE DESIGN FOR TWO STORY CMU/WOOD RESIDENTIAL HOME IN
PUERTO RICO**



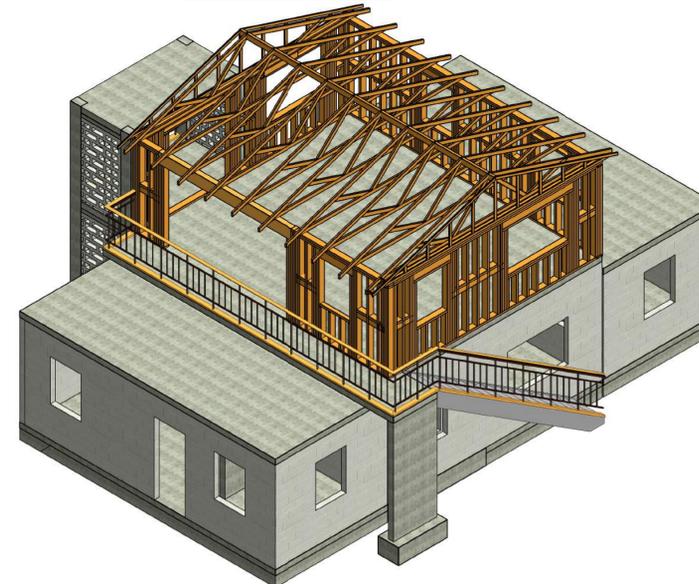
**ISOMETRIC VIEW OF
PRIMARY STRUCTURE**



**ISOMETRIC VIEW OF
PRIMARY STRUCTURE WITH
MODULES ATTACHED**



**ISOMETRIC VIEW OF PRIMARY
STRUCTURE**



**ISOMETRIC VIEW OF PRIMARY STRUCTURE
WITH MODULES ATTACHED**

PREFACE:

THIS PRESCRIPTIVE HOME DRAWING SET PRESENTS RECOMMENDATIONS FOR THE CONSTRUCTION OF A TWO STORY HOME (PRIMARY STRUCTURE) WITH FUTURE ADDITIONS (MODULES).

THIS GUIDANCE DISPLAYS INFORMATION FOR A PARTICULAR SIZED HOME. THE DESIGN INFORMATION PROVIDED HEREIN INCORPORATES SEISMIC AND WIND CRITERIA BASED UPON THE LATEST PUERTO RICO BUILDING CODE WHICH REFERENCES THE 2018 INTERNATIONAL RESIDENTIAL CODE (2018 IRC), 2018 INTERNATIONAL BUILDING CODE (2018 IBC), AND THE AMERICAN SOCIETY OF CIVIL ENGINEERS ASCE/SEI 7-16: MINIMUM DESIGN LOADS AND ASSOCIATED CRITERIA FOR BUILDINGS AND OTHER STRUCTURES.

ALL RECOMMENDED DESIGN WORK, INCLUDING THOSE PARTS COVERED BY THIS DOCUMENT, SHALL BE DESIGNED BY A REGISTERED DESIGN PROFESSIONAL SUCH AS A REGISTERED PROFESSIONAL ENGINEER OR A LICENSED ARCHITECT IN PUERTO RICO. WHEN THESE GUIDANCE DRAWINGS ARE USED FOR A PROJECT, THEY SHOULD BE MODIFIED AS NEEDED IN ORDER TO COMPLY WITH ALL OF THE APPLICABLE CODE REQUIREMENTS FOR A GIVEN PROJECT SITE, THEN SIGNED AND SEALED IN ACCORDANCE WITH PUERTO RICO LAWS, BUILDING CODE, AND DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC).

THE FOLLOWING BOUNDARY CONDITIONS SHALL BE MET IN ORDER TO USE THIS DRAWING SET. THIS DRAWING SET IS NOT VALID IF THE PROJECT PARAMETERS ARE OUTSIDE OF THESE BOUNDARY CONDITIONS:

1. TWO STORY BUILDING WITH THE MAXIMUM MEAN ROOF HEIGHT AS SHOWN IN THE DRAWING SET.
2. ROOF AS SHOWN IN THE DRAWING SET.
3. BUILDING WIDTH AND LENGTH AS SHOWN IN THE DRAWING SET.

DETERMINE SITE SPECIFIC EXPOSURE CATEGORY FIRST AND THEN DETERMINE THE SITE SPECIFIC WIND SPEED AS SHOWN IN THE ATC ONLINE HAZARDS TOOL. FOR THE PUERTO RICO BUILDING CODE 2018, CONFIRM THAT THE EXPOSURE AND DESIGN WIND SPEED DO NOT EXCEED THAT SHOWN IN THE DESIGN DATA WITHIN THE DRAWING SET.

SITE SPECIFIC WIND AND SEISMIC INFORMATION FOR PUERTO RICO CAN BE FOUND BY USING THE ONLINE HAZARDS TOOL DEVELOPED BY ATC AND FOUND AT THE WEBSITE: [HTTPS://HAZARDS.ATCOUNCIL.ORG/](https://hazards.atcouncil.org/)

ALL CONSTRUCTION MUST COMPLY WITH THE PUERTO RICO BUILDING CODE. YOU ARE REQUIRED TO OBTAIN THE NECESSARY BUILDING PERMITS FROM THE DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC). SIGNED AND SEALED DRAWINGS FOR PERMIT MUST BE SUBMITTED TO THE DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (OPPe-DDEC).

STRUCTURES LOCATED IN SPECIAL FLOOD HAZARD AREAS SHALL BE DESIGNED BY A REGISTERED DESIGN PROFESSIONAL AND CERTIFIED TO COMPLY WITH ASCE 24-14 FLOOD RESISTANT DESIGN AND CONSTRUCTION.

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND
FL. WOOD
HOME**

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (OPPe-DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

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No.	Date	Description

PROFESSIONAL SEALS:

SHEET TITLE:

Title Sheet

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-001
QC Review:	
Phase:	

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COMPONENTS AND CLADDING ULTIMATE DESIGN PRESSURE SCHEDULE				
GABLE ROOF, $\phi \leq 7^\circ$ WALLS $h \leq 60'$			EXPOSURE CATEGORY, TOPOGRAPHIC FACTOR EXP. D, $Kzt = 1.0$	
COMPONENT	ZONE	EFFECTIVE WIND AREA (SF)	SURFACE PRESSURE (PSF)	
			POSITIVE	NEGATIVE
ROOF ELEMENTS	1	10	38.8	-152.1
		50	33.2	-127.8
		100	30.8	-119.7
	1'	10	38.8	-87.4
		50	33.2	-87.4
		100	30.8	-87.4
	2	10	38.8	-200.7
		50	33.2	-168.3
		100	30.8	-168.3
3	10	38.8	-273.5	
	50	33.2	-247.6	
	100	30.8	-213.6	
EXTERIOR WALL ELEMENTS	4	10	95.5	-103.6
		50	87.4	-95.5
		100	79.3	-87.4
	5	10	95.5	-127.8
		50	87.4	-110.0
		100	79.3	-103.6

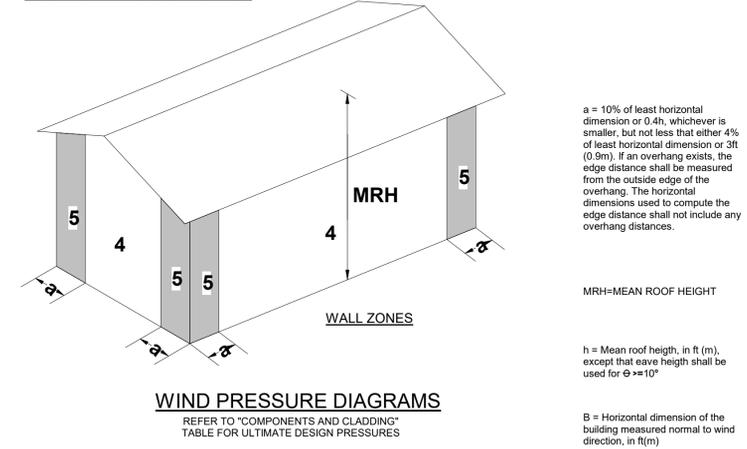
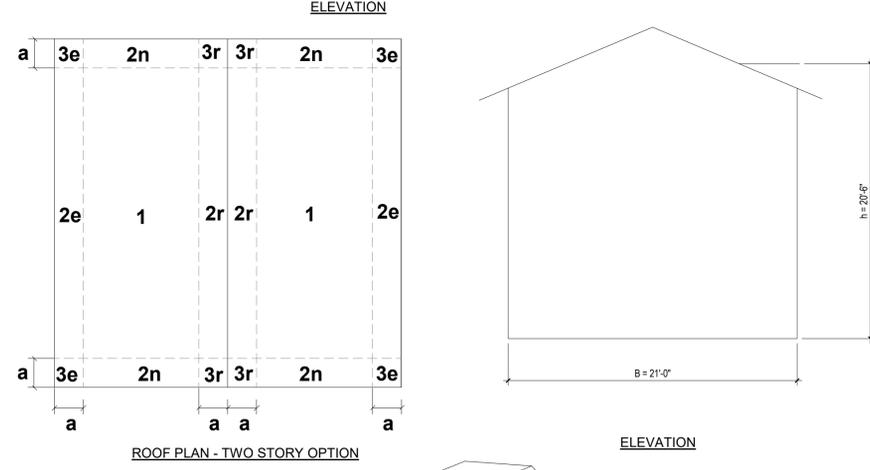
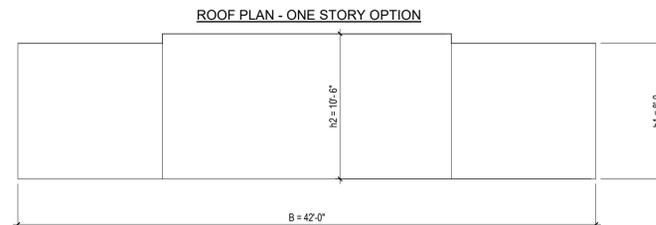
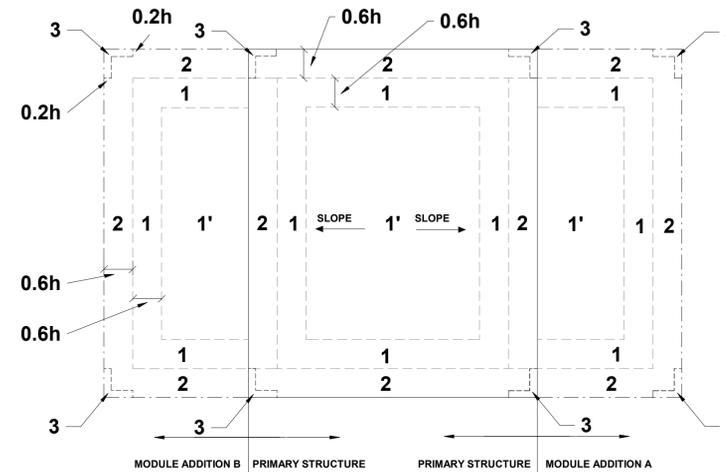
NOTES:
1. DESIGN WIND PRESSURES SHALL BE USED IN THE DESIGN OF ALL COMPONENTS AND CLADDING ELEMENTS COMPRISING THE BUILDING ENVELOPE.
2. REFER TO THE WIND PRESSURE DIAGRAM FOR ZONE LOCATIONS AND EXTENTS.
3. POSITIVE PRESSURES ACT TOWARD COMPONENT SURFACES AND NEGATIVE PRESSURES ACT AWAY FROM COMPONENT SURFACES.
4. LINEAR INTERPOLATION BETWEEN EFFECTIVE WIND AREAS MAY BE USED TO OBTAIN THE REQUIRED COMPONENT AND CLADDING DESIGN PRESSURE.
5. OVERHANG SOFFIT PRESSURE EQUALS ADJACENT WALL PRESSURE.

1
S-003 1/16" = 1'-0"
ROOF & WALL DIAGRAM-C & C PRESSURES - ONE STORY OPTION

COMPONENTS AND CLADDING ULTIMATE DESIGN PRESSURE SCHEDULE				
GABLE ROOF $7^\circ < \phi \leq 20^\circ$ WALLS $h \leq 60'$			EXPOSURE CATEGORY, TOPOGRAPHIC FACTOR EXP. D, $Kzt = 1.0$	
COMPONENT	ZONE	EFFECTIVE WIND AREA (SF)	SURFACE PRESSURE (PSF)	
			POSITIVE	NEGATIVE
ROOF ELEMENTS	1 & 2e	10	58.2	-186.7
		50	48.8	-109.6
		100	41.1	-58.2
	2n, 2r, & 3e	10	58.2	-272.3
		50	48.8	-186.7
		100	41.1	-152.4
	3r	10	58.2	-323.7
		50	48.8	-220.9
		100	41.1	-169.5
	Ovh, 1 & 2e	10	N/A	-229.5
		50	N/A	-202.9
		100	N/A	-178.1
	Ovh, 2n	10	N/A	-315.1
		50	N/A	-229.5
		100	N/A	-186.7
	Ovh, 3e	10	N/A	-366.5
		50	N/A	-255.2
		100	N/A	-212.3
Ovh, 3r	10	N/A	-417.8	
	50	N/A	-272.3	
	100	N/A	-212.3	
EXTERIOR WALL ELEMENTS	4	10	101.0	-109.6
		50	92.5	-101.0
		100	83.9	-92.5
	5	10	101.0	-135.3
		50	92.5	-116.5
		100	83.9	-109.6

NOTES:
1. DESIGN WIND PRESSURES SHALL BE USED IN THE DESIGN OF ALL COMPONENTS AND CLADDING ELEMENTS COMPRISING THE BUILDING ENVELOPE.
2. REFER TO THE WIND PRESSURE DIAGRAM FOR ZONE LOCATIONS AND EXTENTS.
3. POSITIVE PRESSURES ACT TOWARD COMPONENT SURFACES AND NEGATIVE PRESSURES ACT AWAY FROM COMPONENT SURFACES.
4. LINEAR INTERPOLATION BETWEEN EFFECTIVE WIND AREAS MAY BE USED TO OBTAIN THE REQUIRED COMPONENT AND CLADDING DESIGN PRESSURE.
5. OVERHANG SOFFIT PRESSURE EQUALS ADJACENT WALL PRESSURE.

2
S-003 1/16" = 1'-0"
ROOF & WALL DIAGRAM-C & C PRESSURES - TWO STORY OPTION



CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND
FL. WOOD
HOME**

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (OGP+DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

ISSUE LOG

No.	Date	Description

PROFESSIONAL SEALS:

SHEET TITLE:

Design Data

SHEET INFORMATION:

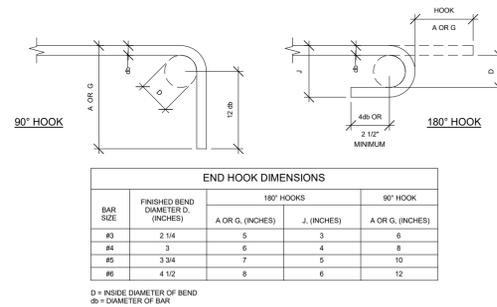
JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-003
QC Review:	Phase:

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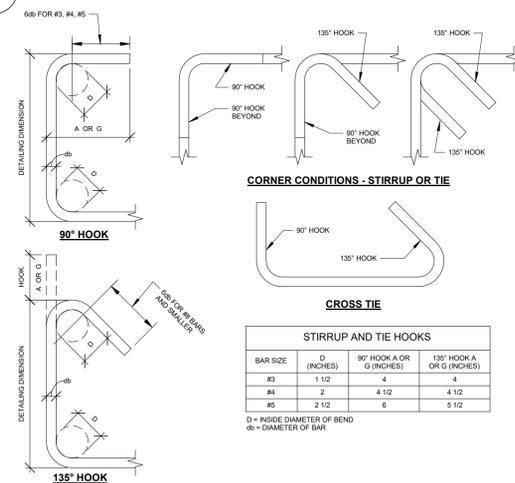
WOOD FASTENING SCHEDULE			
ITEM	DESCRIPTION OF BUILDING ELEMENTS	NUMBER AND TYPE OF FASTENER	SPACING AND LOCATION
Roof			
1	Rafter or roof truss to top plate	Use Connector See Plans	See Plans
2	Blocking to top plate	A34 Connector with 8 #9 x 1 1/2" SD Screws	6" o.c.
Wall			
3	Built-up header ((3) 2x header with (2) 1/2" spacers)	16d common (3 1/2" x 0.162") 16d box (3 1/2" x 0.135")	16" o.c each edge, face nail, both sides 12" o.c each edge, face nail, both sides
4	Top plate to top plate	10d box (3" x 0.128")	6" o.c face nail
5	Double top plate splice	See Plans	See Plans
6	Top plate or bottom plate to stud	Use Connector See Plans	See Plans
7	Top plate, laps at corners	3-10d box (3" x 0.128") or 2-16d common (3 1/2" x 0.162")	Face nail
8	King Stud to King Stud at Openings	See Plans	See Plans
9	Blocking to Stud	6-10d box (3" x 0.128")	Toe Nail (3) Ea. End
10	Sill Plate to Sill Plate	10d box (3" x 0.128")	6" o.c. face nail

NOTE: THIS FASTENING SCHEDULE SHALL APPLY TO ALL MEMBERS UNLESS SPECIFIED IN PLANS. WHERE PLANS CALL OUT MORE STRINGENT REQUIREMENTS FOLLOW PLANS.

1 WOOD FASTENING SCHEDULE



2 TYPICAL END HOOK TYPES



3 TYPICAL STIRRUP AND TIE HOOK TYPES

HEADERED WALL OPENING SCHEDULE					
OPENING WIDTH	BEAM SIZE	KING & JACK STUD (EA. SIDE)	SILL PLATE	LOCATION	HEADER STRAPS (EA. SIDE)
3'-0"	(3) 2"x8"	2 & 2	(1) 2"x6"	2ND. FLOOR	MSTA 30
6'-0"	(3) 2"x8"	3 & 3	(2) 2"x6"	2ND. FLOOR	MSTA 30

NOTES:
1. PROVIDE TSP STUD PLATE TIES AT EACH KING/JACK, REF. TYP. WALL OPENING DETAILS.
2. PROVIDE MSTA 30 STRAPS EACH SIDE OF BEARING HEADERED OPENINGS, REF. TYPICAL WALL OPENING DETAILS.

4 HEADERED WALL OPENING SCHEDULE

LAP SPLICE SCHEDULE CONCRETE		
BAR SIZE	f'c = 3000 psi	
	TENSION	COMPRESSION
3	21	8
4	28	11
5	36	14
6	43	16
7	62	19
8	71	22
9	80	25

NOTES:
1. LAP LENGTHS ARE IN INCHES AND ARE BASED ON GRADE 60 REINFORCING STEEL AND NORMAL WEIGHT CONCRETE.

5 LAP SPLICE SCHEDULE CONCRETE

LAP SPLICE SCHEDULE MASONRY		
BAR SIZE	f'm = 1900 psi	
	TENSION	COMPRESSION
3	27	27
4	36	36
5	45	45
6	54	54
7	63	63
8	72	72
9	82	82

NOTES:
1. LAP LENGTHS ARE IN INCHES AND ARE BASED ON GRADE 60 REINFORCING STEEL AND NORMAL WEIGHT MASONRY UNITS.

6 LAP SPLICE SCHEDULE MASONRY

STRUCTURAL SHEATHING SCHEDULE					
ELEMENT	SHEATHING	FASTENER	SPAN RATING	PANEL FASTENING EDGE	
				INTERIOR	EXTERIOR
EXTERIOR WALL	23/32" STRUCT. 1 PANELS	#12 SCREW W/ 3" LENGTH	48/24	3" C/C	6" C/C
ROOF	23/32" STRUCT. 1 PANELS	#12 SCREW W/ 3" LENGTH	48/24	3" C/C	6" C/C

NOTES:
1. FOR ALL WALL SHEATHING PROVIDE CONTINUOUS BLOCKING AT ALL PANEL EDGES PERPENDICULAR TO THE FRAMING MEMBERS. APPLY SHEATHING PERPENDICULAR TO FRAMING MEMBERS. PROVIDE DOUBLE WALL STUDS TO SUPPORT EXTERIOR SHEATHING AT SHEATHING JOINTS.
2. WHERE FASTENER ATTACHES TO BLOCKING PROVIDE 3/4" EDGE DISTANCE FROM PANEL EDGE TO CENTER LINE OF FASTENER.

7 STRUCTURAL SHEATHING SCHEDULE

WALL STUD SCHEDULE				
EXTERIOR LOAD BEARING				
STUD SIZE	SPECIES/GRADE	UNBRACED HGT.	LOCATION	SPACING
2"x6"	S-Y-P No.2	8'-0"	2nd FLOOR	12" C/C
INTERIOR NON-LOAD BEARING				
2"x4"	S-Y-P No.2	8'-0"	2nd FLOOR	16" C/C

NOTES:
1. SEE TYPICAL DETAILS FOR REQUIRED CONNECTORS
2. PROVIDE ATTACHMENT OF INTERIOR NON LOAD BEARING WALLS TO CONC. SLAB AND WOODEN ROOF TRUSSES UTILIZING VERTICALLY SLOTTED CONNECTION.

8 WALL STUD SCHEDULE

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (OGP-DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

ISSUE LOG

No.	Date	Description

PROFESSIONAL SEALS:

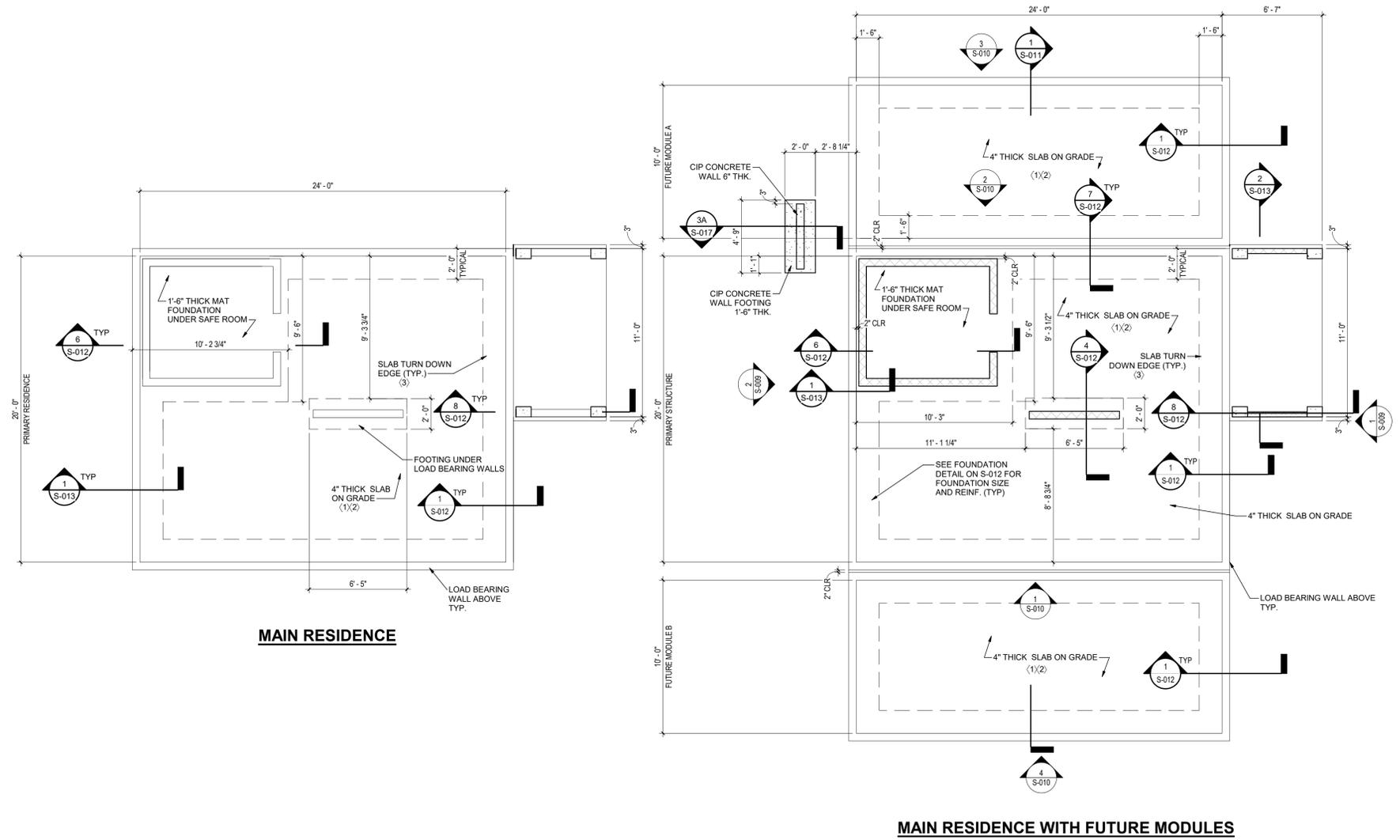
SHEET TITLE:

Schedules and Hook Types

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-004
QC Review:	Phase:

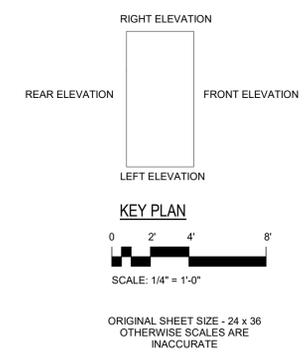
NOT FOR CONSTRUCTION



- STRUCTURAL NOTES:**
1. MAIN RESIDENCE (PRIMARY STRUCTURE) TO BE BUILT PRIOR OR SIMULTANEOUSLY WITH BUILDING MODULES. MODULES SHALL NOT BE CONSTRUCTED WITHOUT CONSTRUCTING THE PRIMARY STRUCTURE.
 2. SEE SECTIONS FOR CONCRETE STEEL REINFORCING.
 3. COORDINATE DOOR/WINDOW OPENINGS WITH ARCH. DWGS.
 4. COORDINATE WITH OTHER DISCIPLINES AND TRADES FOR LOCATIONS AND DIMENSIONS OF OPENINGS, RECESSES, SLEEVES, AND PIPING.
 5. DIMENSIONS INDICATED ARE FROM FACE OF UNFINISHED WALL, UNLESS NOTED OTHERWISE.

- DRAWING KEY NOTES:**
- ① SLAB ON GRADE SHALL BE A MINIMUM 4" THICK CONCRETE WITH 4" x 4" W8 x W8 WWF
 - ② TOP OF SLAB ELEVATION IS AT 0'-0" (DATUM ELEVATION). ALL OTHER ELEVATIONS ARE REFERENCED AS + OR - FROM DATUM.
 - ③ BOTTOM OF FDN = 1'-6" BELOW FINISHED FLOOR ASSUMING A FLAT SITE WITH LEVEL GROUND ON ALL SIDES OF STRUCTURE.

1 FOUNDATION PLANS
S-005 1/4" = 1'-0"



NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (OGP&DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

ISSUE LOG

No.	Date	Description

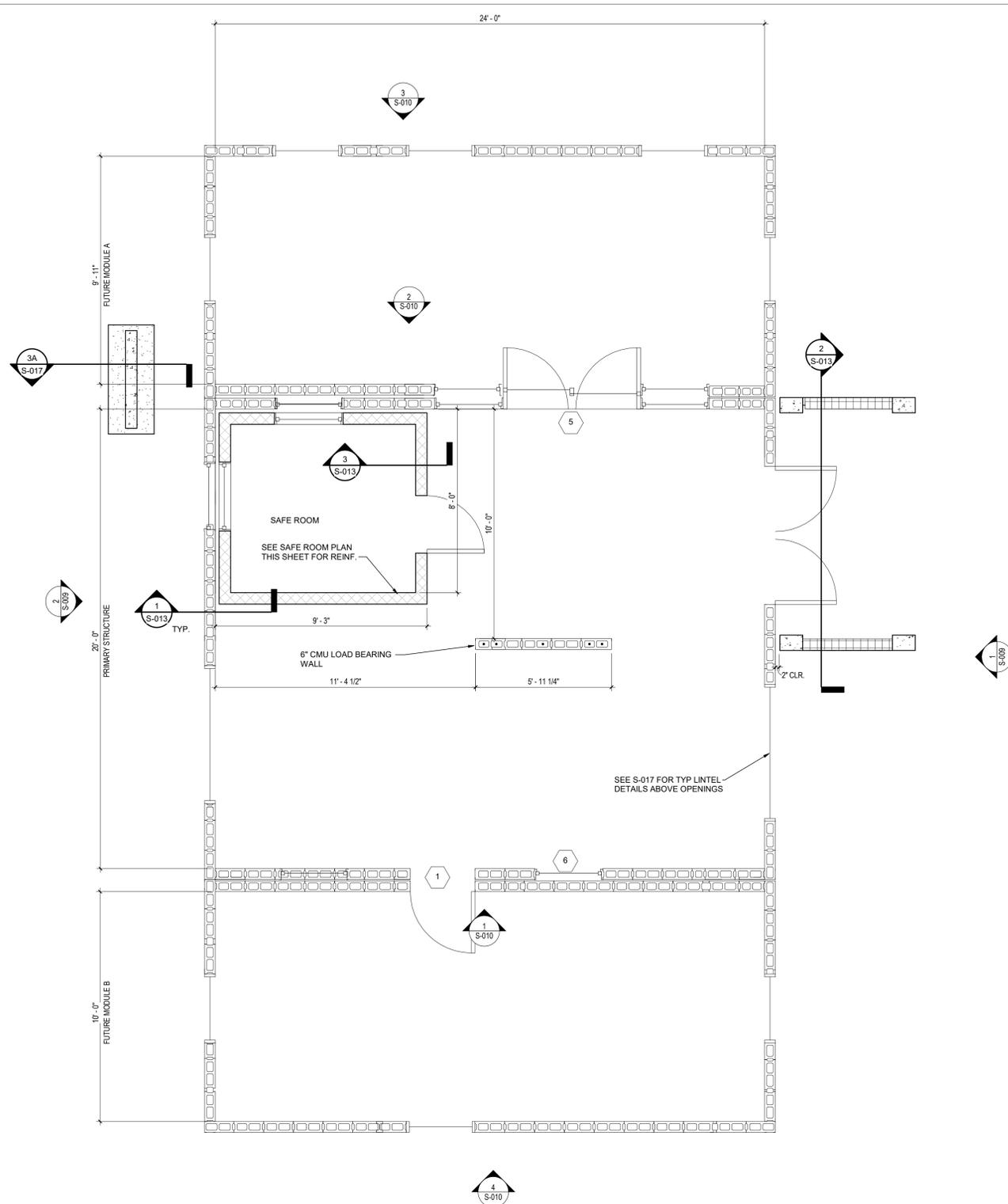
PROFESSIONAL SEALS:

SHEET TITLE:

Foundation Plans

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-005
QC Review:	Phase:



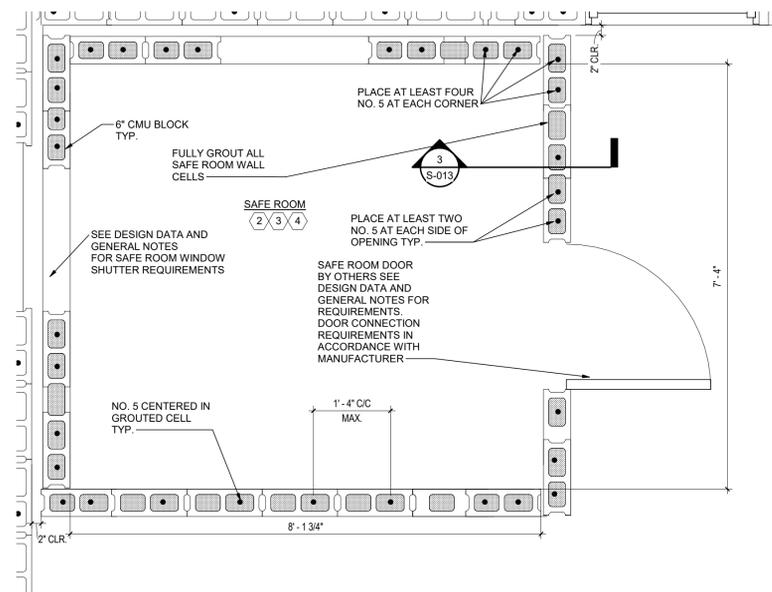
1
S-006
FIRST FLOOR PLAN
3/8" = 1'-0"

STRUCTURAL NOTES

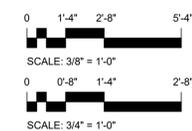
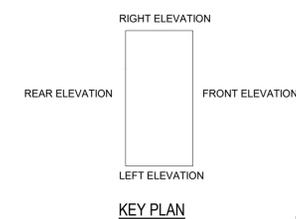
1. MAIN RESIDENCE FOUNDATION AND STRUCTURE TO BE BUILT PRIOR OR SIMULTANEOUSLY TO BUILDING MODULES.
2. SEE SECTIONS FOR MASONRY AND CONCRETE STEEL REINFORCING.
3. MODULES ARE NOT ATTACHED TO PRIMARY STRUCTURE. SEE S-009 FOR FLOOR JOINT DETAIL.
4. COORDINATE DOOR AND WINDOW OPENING LOCATIONS WITH ARCH. DWGS.
5. ALL MASONRY CELLS WITH REBAR SHALL BE FULLY GROUTED. SEE S-013 FOR TYPICAL PRIMARY STRUCTURE AND MODULE WALL REINFORCING. SEE ELEVATIONS FOR ADDITIONAL SHEAR WALL REINFORCING.

DRAWING KEY NOTES

- ① PROVIDE DOOR AT THIS LOCATION ONLY WHEN BUILDING MODULE. SEE TYPICAL FLOOR JOINT DETAIL ON S-012.
- ② PROVIDE 2" CLR BETWEEN SAFE ROOM WALLS AND ANY ADJACENT WALLS.
- ③ PROVIDE DOOR AND WINDOW SHUTTERS MEETING SAFE ROOM REQUIREMENTS. SEE STRUCTURAL GENERAL NOTES.
- ④ SEE "TYPICAL LINTEL DETAIL" ON S-017 FOR LINTEL ABOVE DOORS AND WINDOWS.
- ⑤ SEE TYPICAL FLOOR JOINT DETAIL ON S-012.
- ⑥ WINDOW NOT REQUIRED IF MODULE IS CONSTRUCTED AT THE SAME TIME AS PRIMARY RESIDENCE.



3
S-006
SAFE ROOM PLAN
3/4" = 1'-0"



ORIGINAL SHEET SIZE - 24 x 36
OTHERWISE SCALES ARE
INACCURATE

NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND
FL. WOOD
HOME**

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (DGP+DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

ISSUE LOG

No.	Date	Description

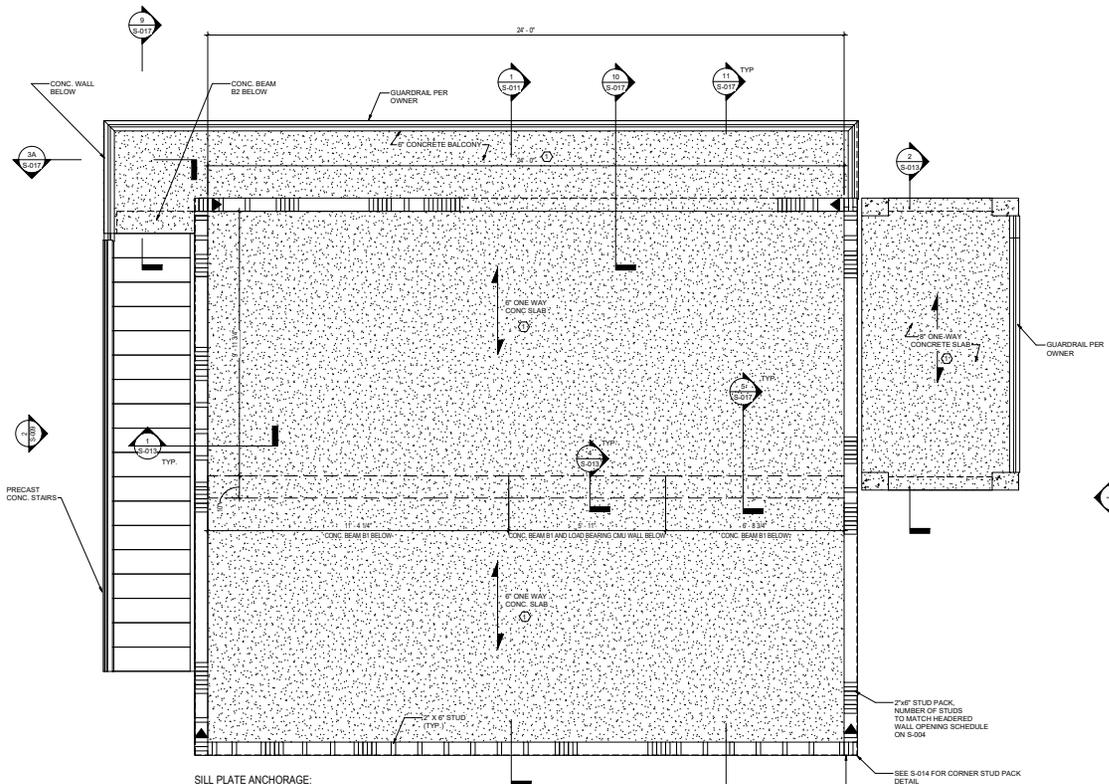
PROFESSIONAL SEALS:

SHEET TITLE:

First Floor Plan

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-006
QC Review:	Phase:



STRUCTURAL NOTES:

1. SEE SECTIONS FOR CONCRETE STEEL REINFORCING.
2. SECOND STORY CAN BE BUILT IMMEDIATELY FOLLOWING CONSTRUCTION OF THE 1ST STORY (CAST IN PLACE) OR AT A LATER TIME (POST INSTALLED).
3. FUTURE MODULES NOT SHOWN FOR CLARITY.
4. ALL SILL PLATES SHALL BE PRESSURE TREATED.
5. DO NOT PLACE A CISTERN ON THE ROOF/2ND FLOOR SLAB WITHOUT ADDITIONAL REINFORCEMENT. CONCRETE SLAB IS NOT INTENDED TO SUPPORT A ROOF CISTERN WHEN 2ND STORY IS NOT CONSTRUCTED.

DRAWING KEY NOTES:

- Ⓢ TOP OF CONCRETE ELEVATION = 10'-0"

SILL PLATE ANCHORAGE:

AT ALL SILL PLATES PROVIDE MASA SILL PLATE ANCHORS AT 12" O.C. (CAST IN PLACE) OR 3/8" X 6 3/8" HLT HT Z ANCHOR WITH HLT HT Y ADHESIVE OR EQUIVALENT AT 36" O.C. AND WITHIN 16" EA SIDE OF ALL WALL OPENINGS AND CORNERS WITH 9" X 3" X 3/16" WASHER AND NUT. SEE S-012, AND S-014 FOR DETAILS.

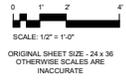
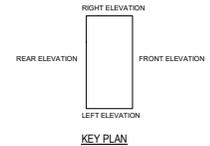
▲ = SIMPSON HOUS-HOLD-DOWN OR EQUIVALENT WITH CAST IN PLACE 5/8" X 9" THREADED ROD. SEE S-012 FOR DETAILS.

THE REFERENCED CONNECTORS ARE MANUFACTURED BY THE SIMPSON STRONG-TIE COMPANY WITH MITEK/USP ALLOWED AS ACCEPTABLE SUBSTITUTIONS. FMS/ADDC DOES NOT SPECIFICALLY ENDORSE THE CONNECTORS OF ANY MANUFACTURER. CONNECTORS THAT EQUAL THE SPECIFICATIONS OF THE NOTED CONNECTORS MAY BE SUBSTITUTED.

2"x4" STUD PACK, NUMBER OF STUDS TO MATCH HEADERED WALL OPENING SCHEDULE ON S-004

SEE S-014 FOR CORNER STUD PACK DETAIL

PROVIDE A MINIMUM OF (2) 2" X 6" STUDS AT EACH HOLD-DOWN SEE S-014 FOR STUD NAILING



1 SECOND FLOOR FRAMING PLAN
1/2" = 1'-0"

NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND
FL. WOOD
HOME**

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DECE), PERMITS MANAGEMENT OFFICE (OPM-DOCE) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DECE, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

ISSUE LOG

No.	Date	Description

PROFESSIONAL SEALS

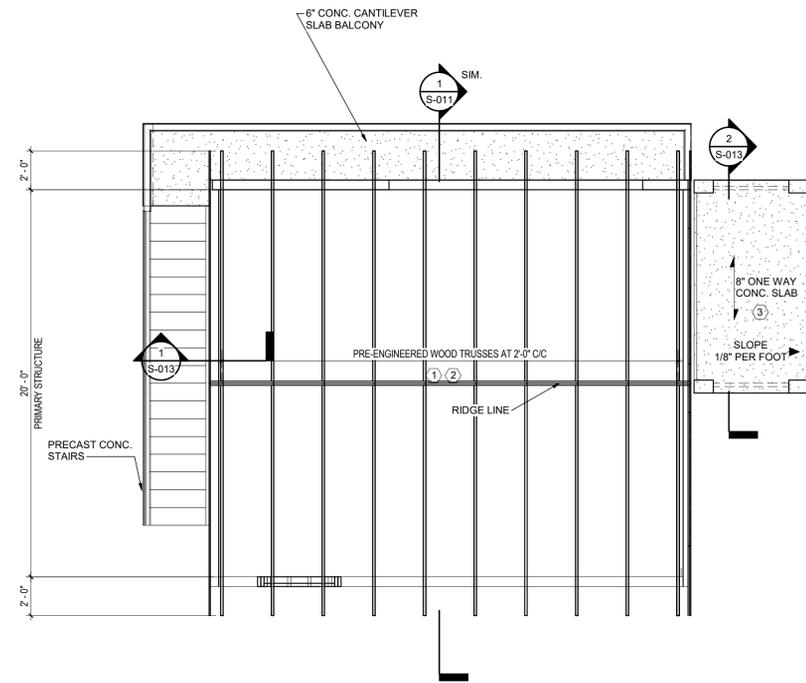
SHEET TITLE:

Second Floor Framing Plan

SHEET INFORMATION:

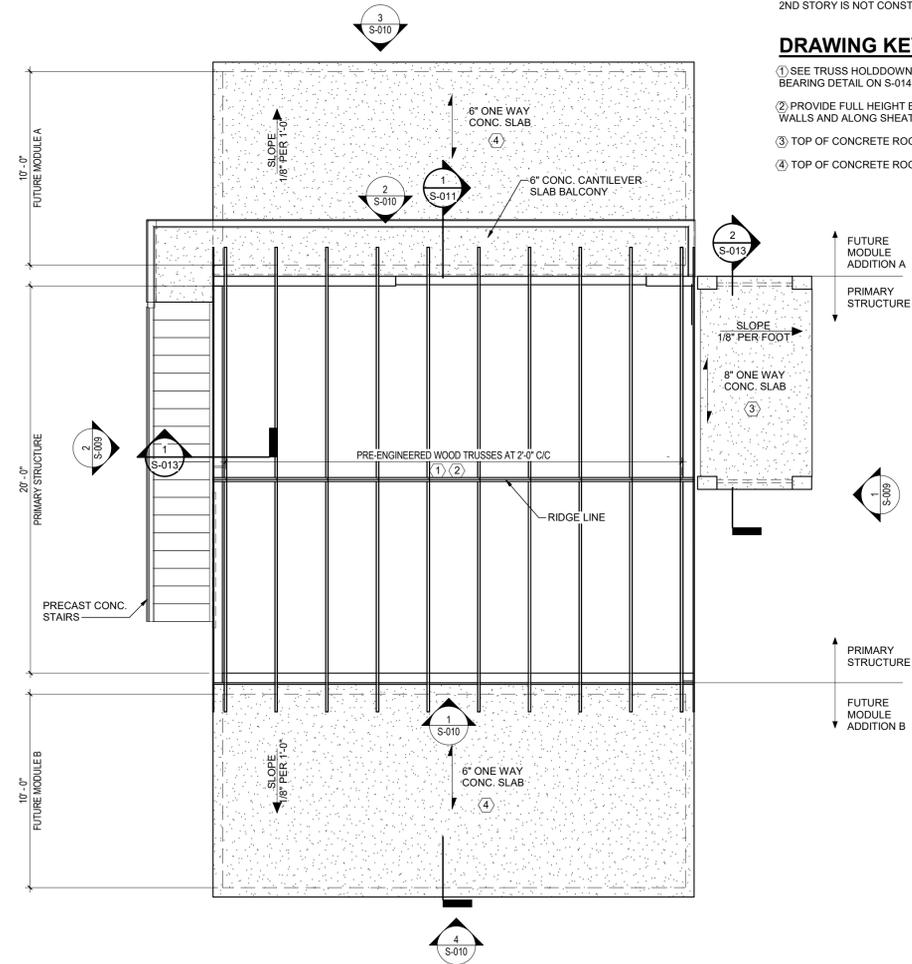
JOB No.	Date Issued	5/15/2020
Drawn By:	Sheet Number:	
Checked By:		
OC Review:		
Phase:		

S-007



MAIN RESIDENCE

1 ROOF FRAMING PLANS
S-008 1/4" = 1'-0"



MAIN RESIDENCE WITH FUTURE MODULES

STRUCTURAL NOTES:

1. SECOND STORY CAN BE BUILT IMMEDIATELY FOLLOWING CONSTRUCTION OF THE 1ST STORY (CAST IN PLACE) OR AT A LATER TIME (POST INSTALLED).
2. SEE S-015 FOR TYPICAL GABLE END BRACING DETAIL AND FOR CONTINUOUS LATERAL RESTRAINT FOR TRUSSES.
3. DO NOT PLACE A CISTERN ON THE ROOF/2ND FLOOR SLAB WITHOUT ADDITIONAL REINFORCEMENT. CONCRETE SLAB IS NOT INTENDED TO SUPPORT A ROOF CISTERN WHEN 2ND STORY IS NOT CONSTRUCTED.

DRAWING KEY NOTES:

- ① SEE TRUSS HOLDDOWN DETAIL AND TRUSS BEARING DETAIL ON S-014.
- ② PROVIDE FULL HEIGHT BLOCKING ABOVE BEARING WALLS AND ALONG SHEATHING EDGES.
- ③ TOP OF CONCRETE ROOF ELEVATION = 18' - 6"
- ④ TOP OF CONCRETE ROOF ELEVATION = 9' - 2"

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND
FL. WOOD
HOME**

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ISSUE LOG

No.	Date	Description

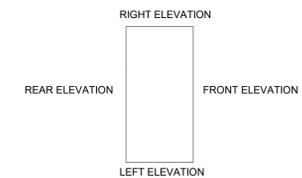
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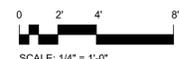
Roof Framing Plans

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-008
QC Review:	Phase:

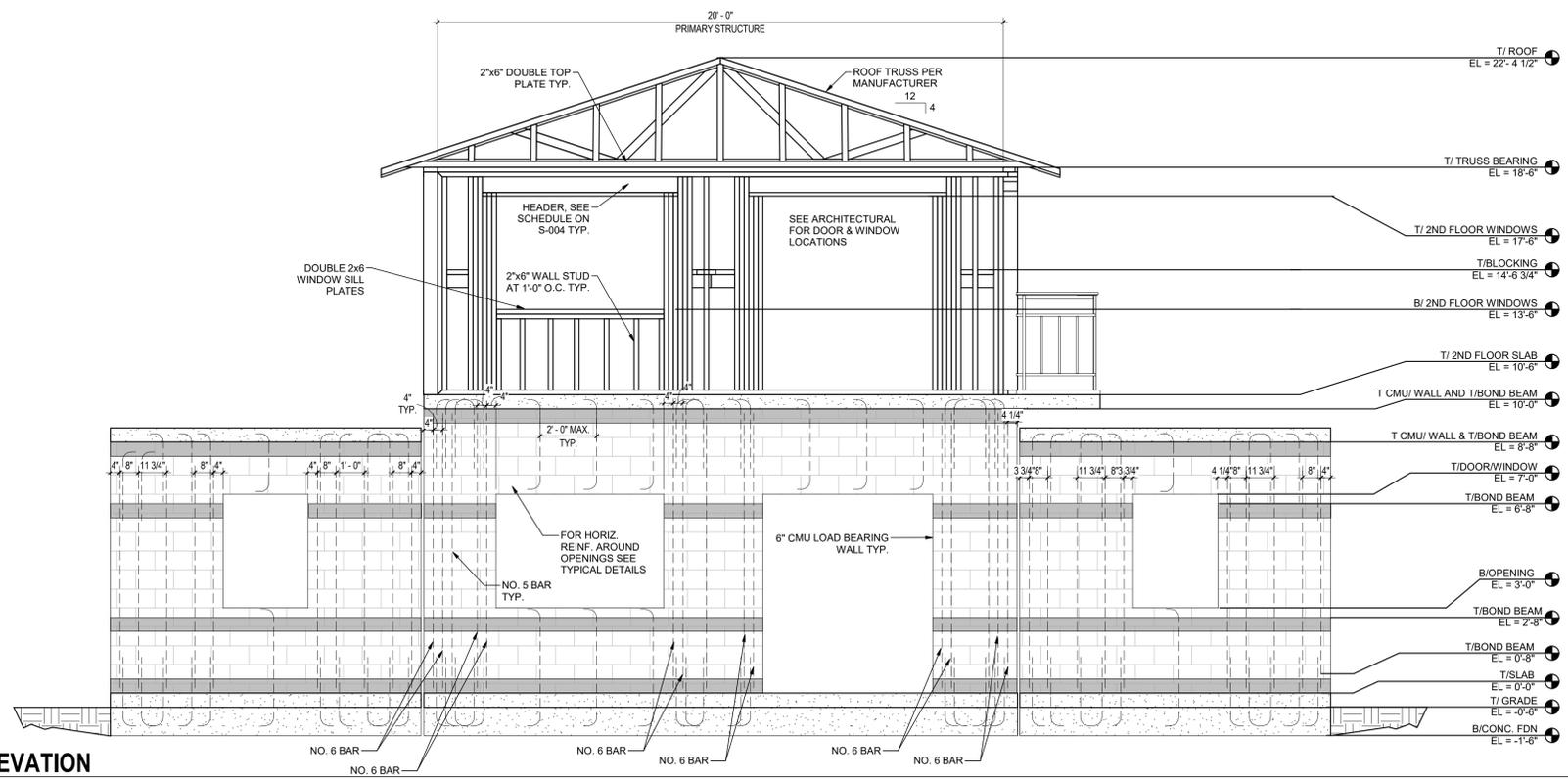


KEY PLAN

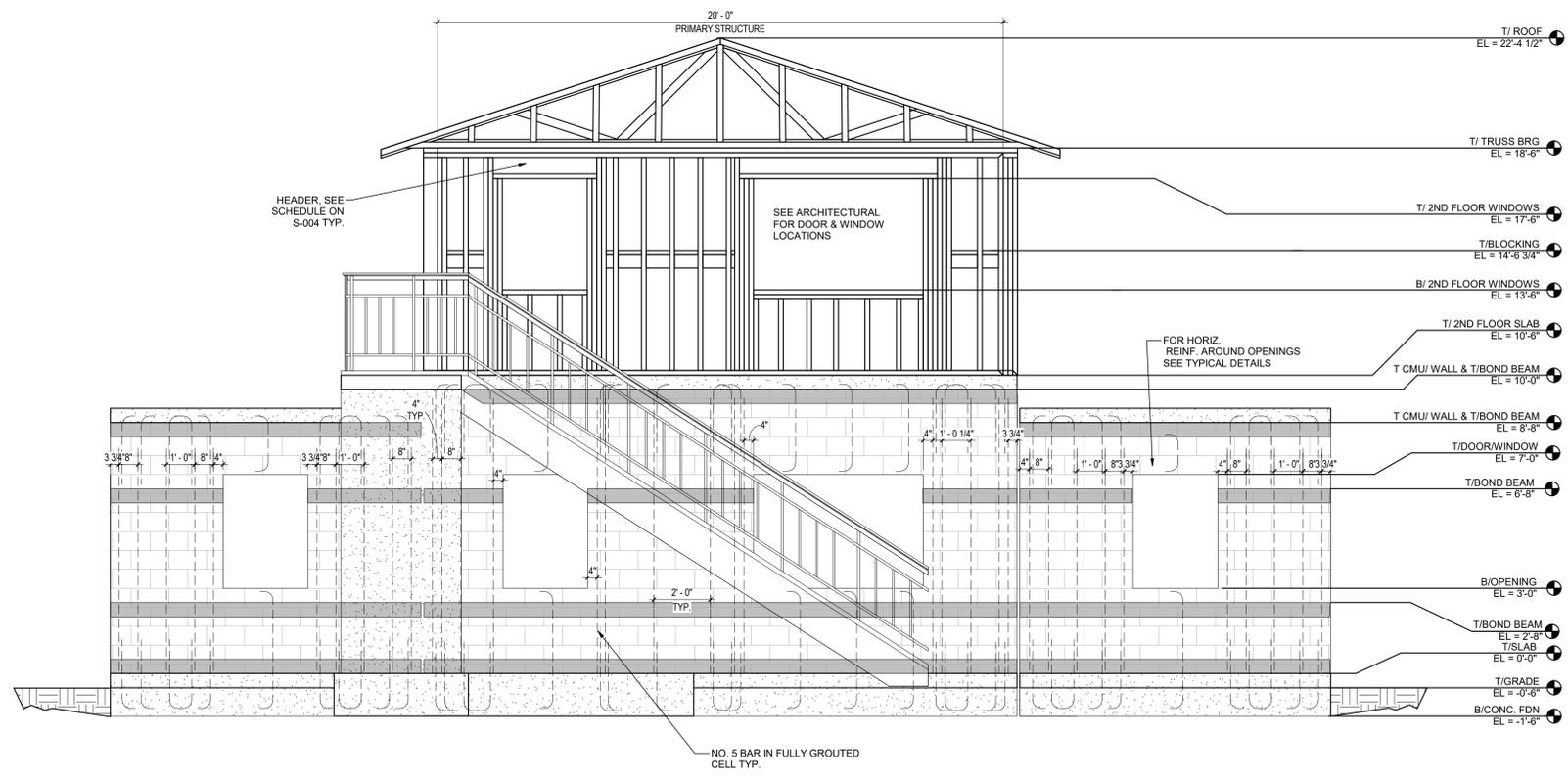


SCALE: 1/4" = 1'-0"
ORIGINAL SHEET SIZE - 24 x 36
OTHERWISE SCALES ARE INACCURATE

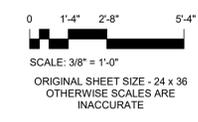
NOT FOR CONSTRUCTION



1 FRONT ELEVATION
S-009 3/8" = 1'-0"



2 REAR ELEVATION
S-009 3/8" = 1'-0"



NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

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ISSUE LOG

No.	Date	Description

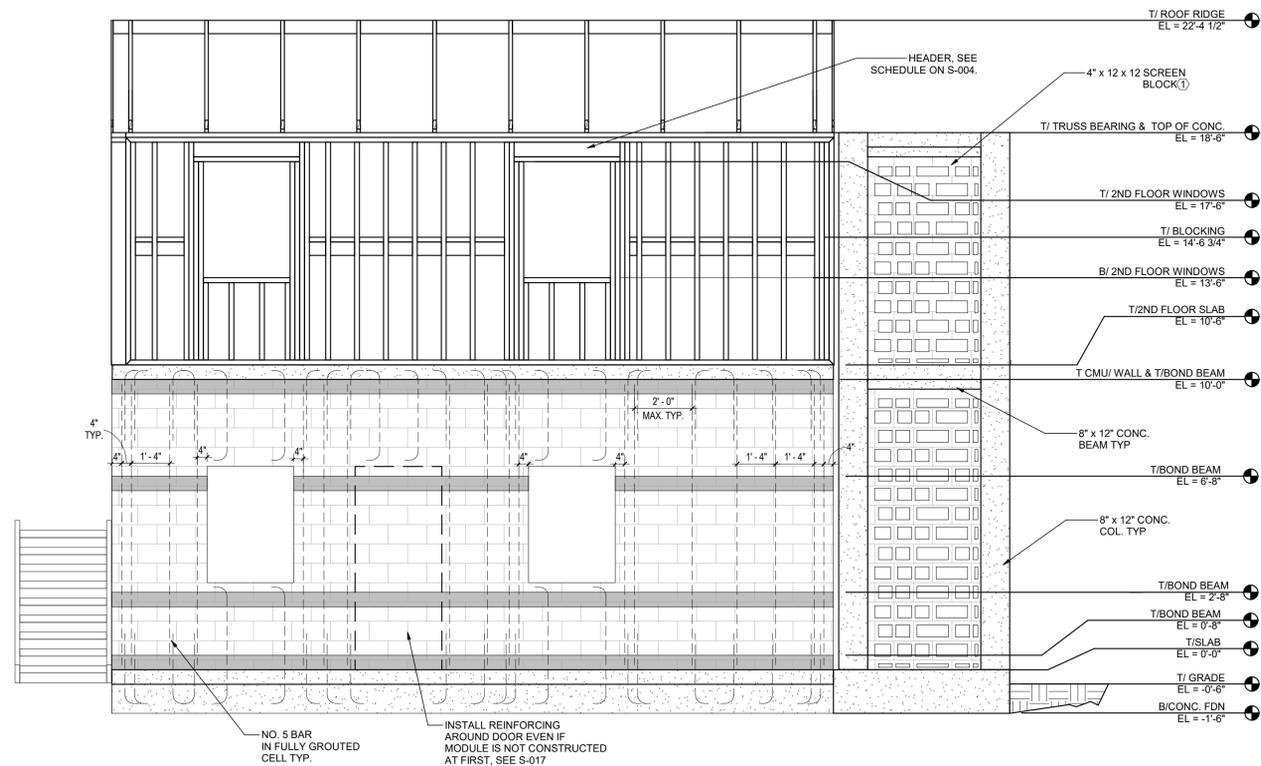
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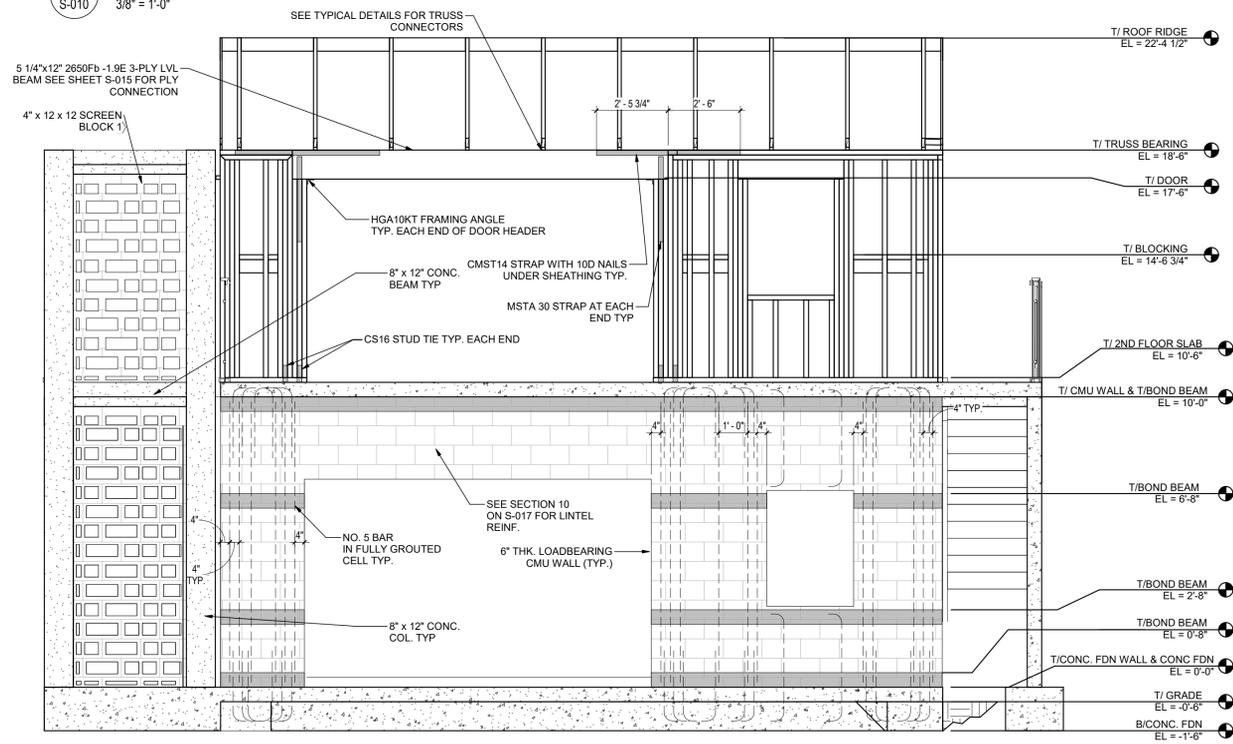
Primary Structure Elevations

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-009
QC Review:	Phase:



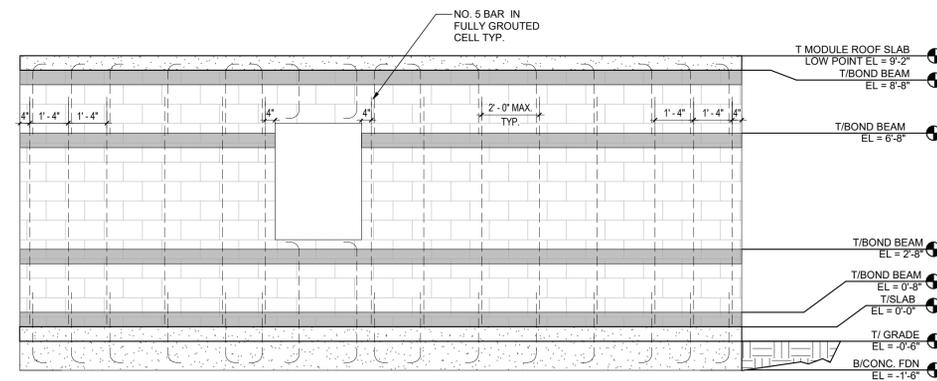
1 LEFT ELEVATION PRIMARY RESIDENCE
S-010 3/8" = 1'-0"



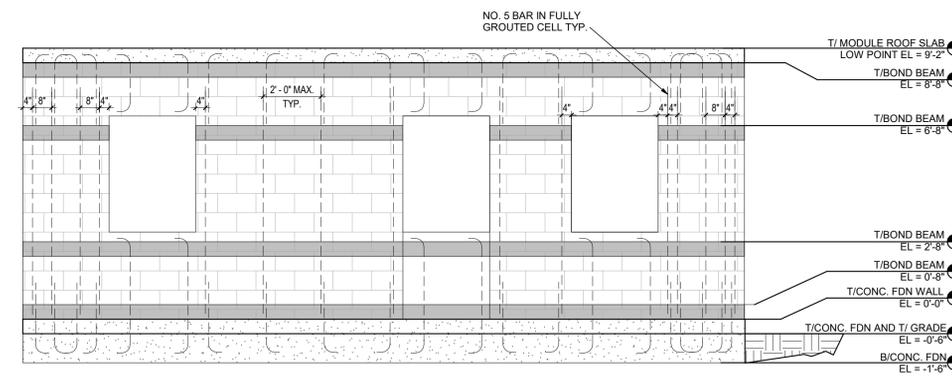
2 RIGHT ELEVATION PRIMARY RESIDENCE
S-010 3/8" = 1'-0"

DRAWING KEY NOTES

(1) SCREEN BLOCK TO HAVE MINIMUM 30% OPEN AREA AND MINIMUM 2000 PSI NET AREA COMPRESSIVE STRENGTH. PROVIDE 9 GA. TRUSS TYPE JOINT REINFORCEMENT AT EVERY COURSE AND EXTEND 4" INTO COLUMN.



4 EXPANSION MODULE B LEFT ELEVATION
S-010 3/8" = 1'-0"



3 EXPANSION MODULE A RIGHT ELEVATION
S-010 3/8" = 1'-0"

SCALE: 3/8" = 1'-0"
ORIGINAL SHEET SIZE - 24 x 36
OTHERWISE SCALES ARE INACCURATE

NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND
FL. WOOD
HOME**

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ISSUE LOG

No.	Date	Description

PROFESSIONAL SEALS:

SHEET TITLE:

Primary Structure Elevations

SHEET INFORMATION:

JOB No. _____ Date Issued: 5/15/2020

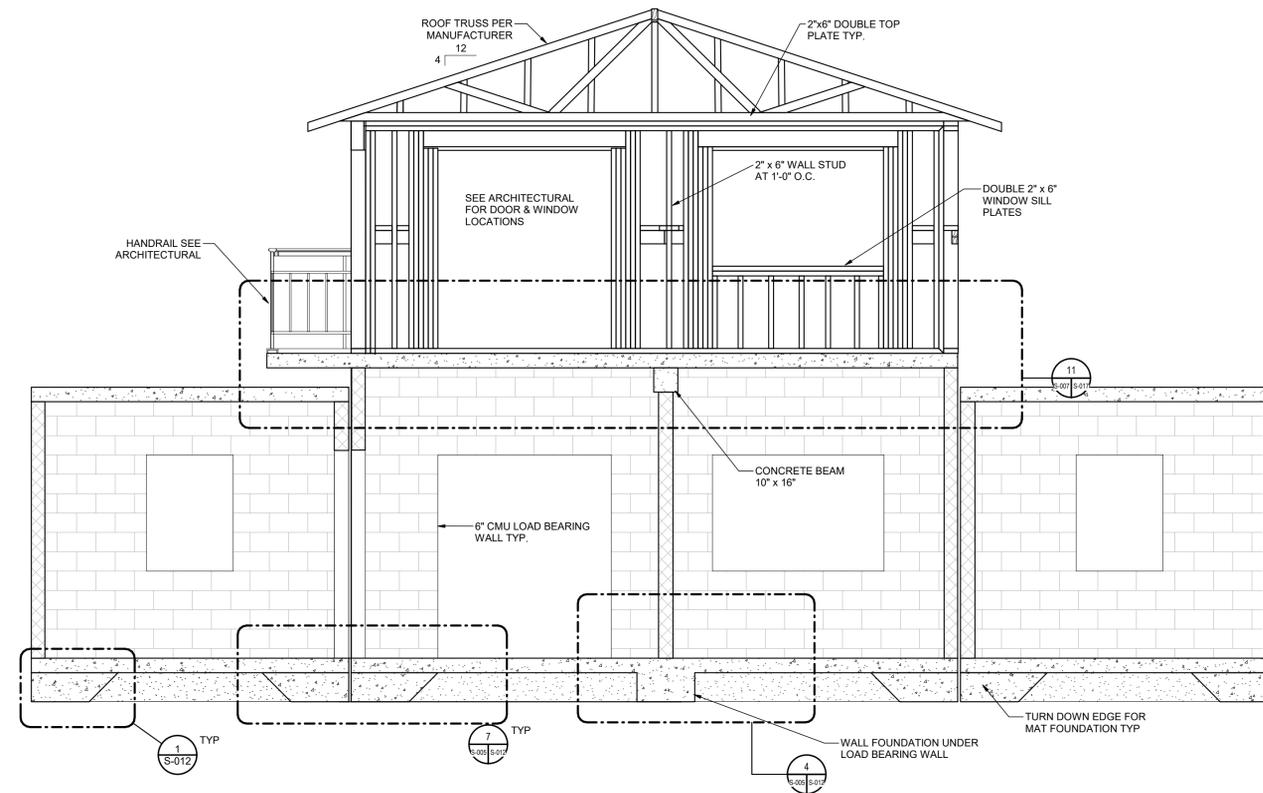
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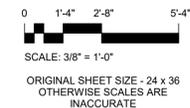
QC Review: _____

Phase: _____

S-010



1
SECTION 1
S-011 3/8" = 1'-0"



NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

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ISSUE LOG

No.	Date	Description

PROFESSIONAL SEALS:

SHEET TITLE:

Sections

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-011
QC Review:	Phase:

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (OGP-DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

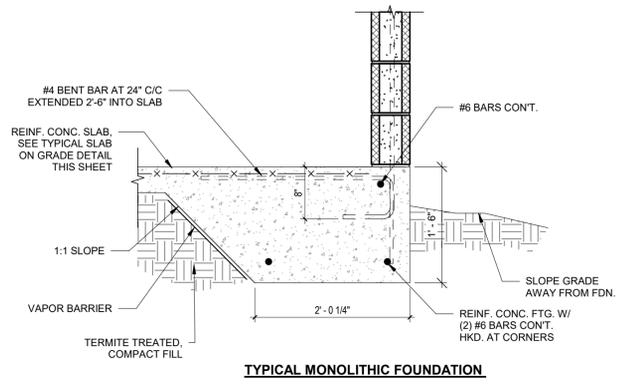
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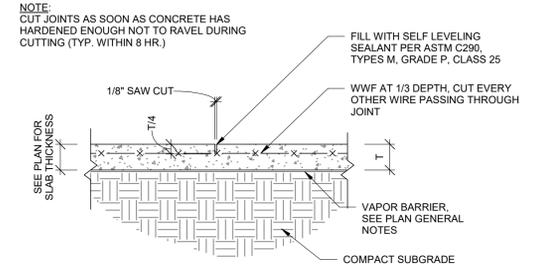
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Foundation Sections and Details

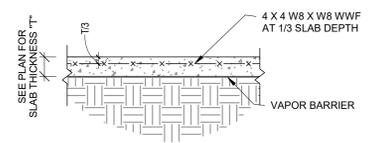
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JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-012
QC Review:	Phase:



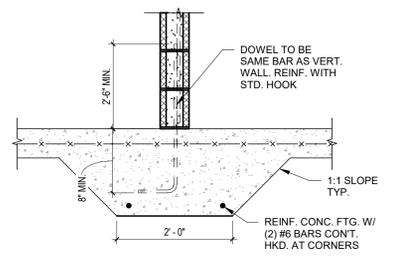
1 FOUNDATION DETAIL
S-012 1" = 1'-0"



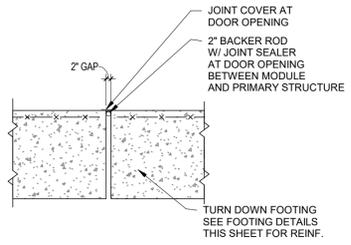
2 CONTROL JOINT DETAIL
S-012 1" = 1'-0"



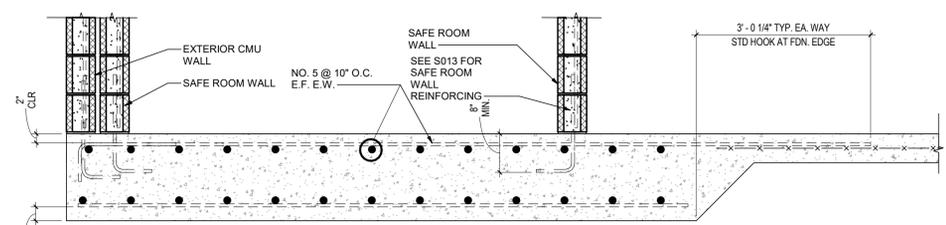
3 TYPICAL SLAB ON GRADE DETAIL
S-012 3/4" = 1'-0"



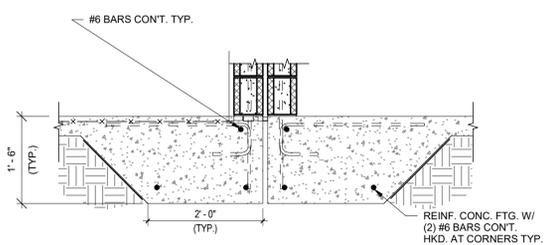
4 TYPICAL INTERIOR FOUNDATION DETAIL
S-012 3/4" = 1'-0"



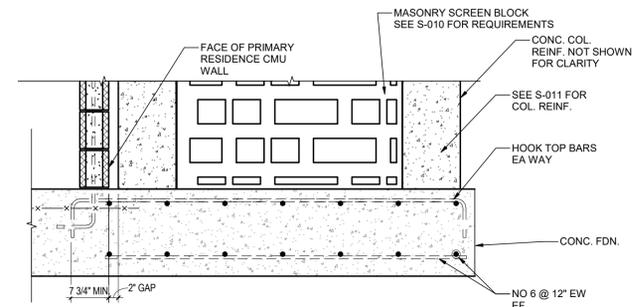
5 TYPICAL FLOOR JOINT DETAIL
S-012 3/4" = 1'-0"



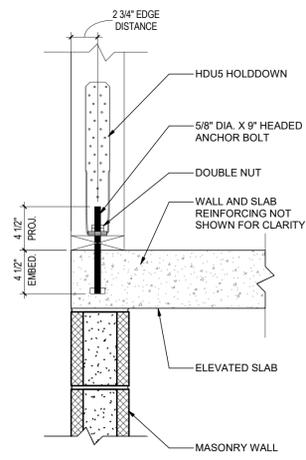
6 TYPICAL SAFE ROOM FOUNDATION SECTION
S-012 3/4" = 1'-0"



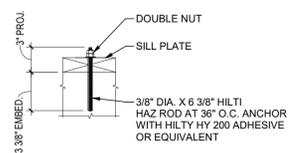
7 TYPICAL FOUNDATION DETAIL AT PRIMARY STRUCTURE AND MODULE INTERFACE
S-012 3/4" = 1'-0"



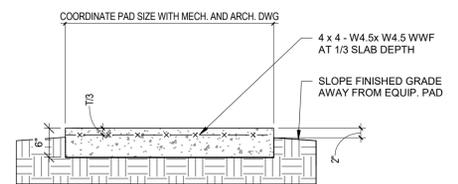
8 OPTIONAL CONCRETE ENTRYWAY FOUNDATION
S-012 3/4" = 1'-0"



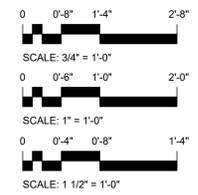
9 HOLDDOWN DETAIL
S-012 1 1/2" = 1'-0"



10 POST INSTALLED SILL ANCHOR DETAIL
S-012 1 1/2" = 1'-0"

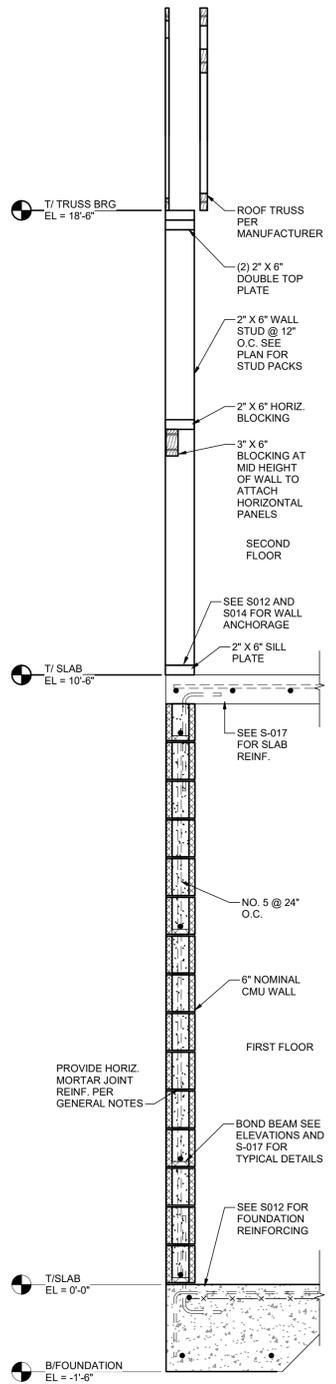


11 TYPICAL EXT. MECH. EQUIP. PAD
S-012 3/4" = 1'-0"

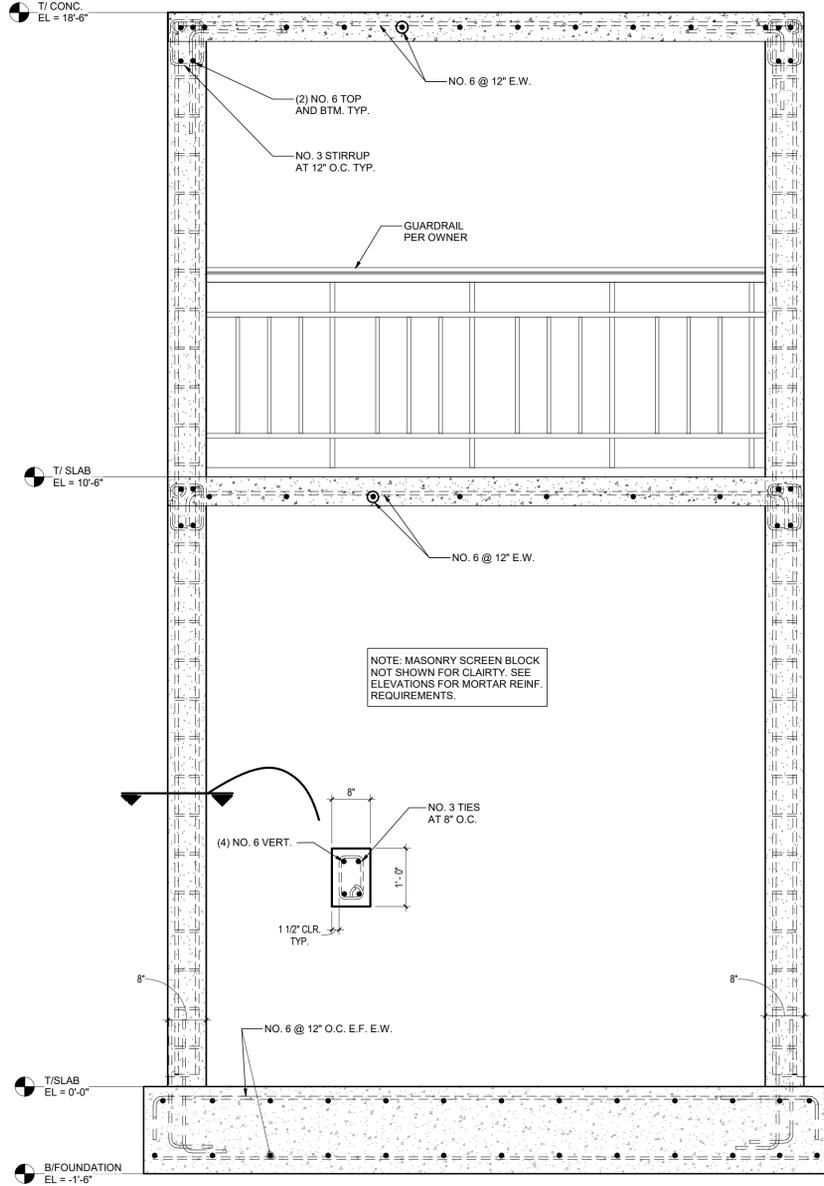


ORIGINAL SHEET SIZE - 24 x 36
OTHERWISE SCALES ARE INACCURATE

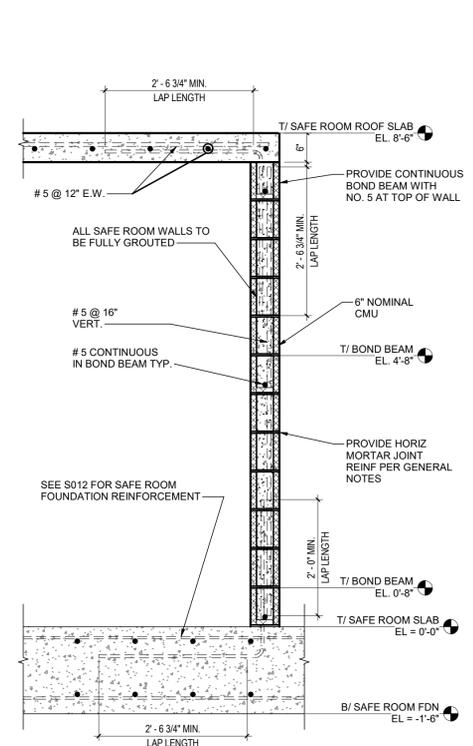
NOT FOR CONSTRUCTION



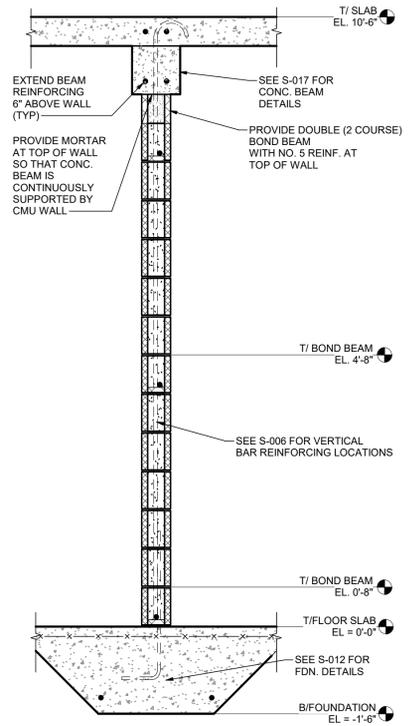
1
S-013
3/4" = 1'-0"



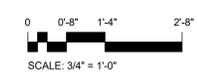
2
S-013
3/4" = 1'-0"



3
S-013
3/4" = 1'-0"



4
S-013
3/4" = 1'-0"



SCALE: 3/4" = 1'-0"
ORIGINAL SHEET SIZE - 24 x 36
OTHERWISE SCALES ARE
INACCURATE

NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

NOTE: PRIOR TO CONSTRUCTION CONTACT PUERTO RICO DEPARTMENT OF ECONOMIC DEVELOPMENT AND COMMERCE (DDEC), PERMITS MANAGEMENT OFFICE (OGPa-DDEC) FOR BUILDING REQUIREMENTS IN PUERTO RICO. THIS INFORMATION HAS BEEN DEVELOPED FOR THE USE OF PUERTO RICO RESIDENTS AND IS BELIEVED TO MEET THE PUERTO RICO BUILDING CODE. ALL DRAWINGS MUST BE SEPARATELY APPROVED BY DDEC, PERMITS MANAGEMENT OFFICE UPON SUBMISSION OF A BUILDING PERMIT APPLICATION.

ISSUE LOG

No.	Date	Description

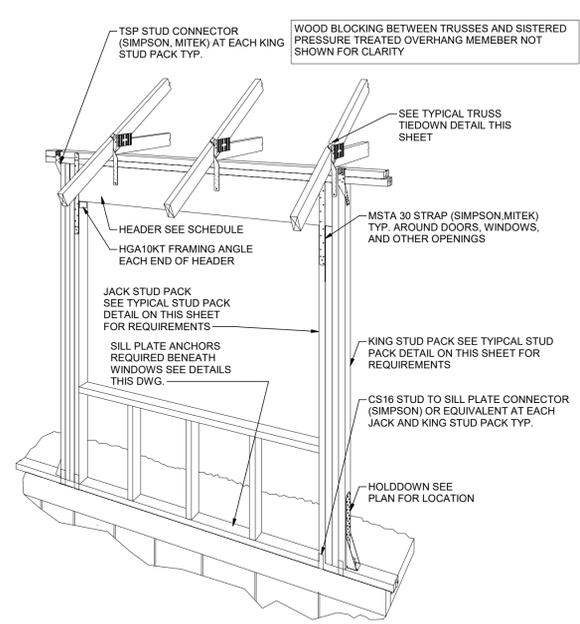
PROFESSIONAL SEALS:

SHEET TITLE:

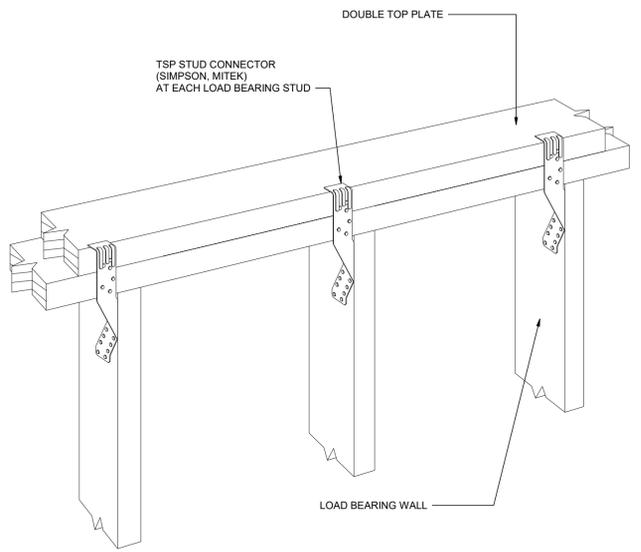
Wall Sections and Details

SHEET INFORMATION:

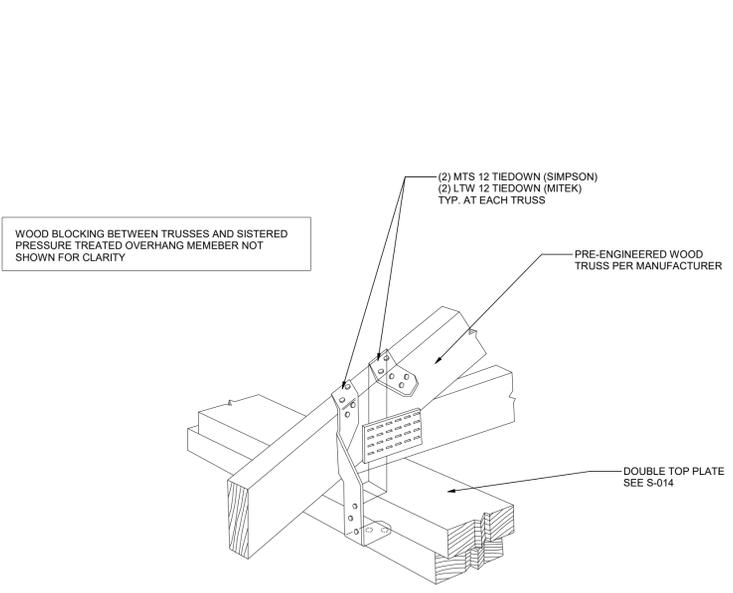
JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-013
QC Review:	Phase:



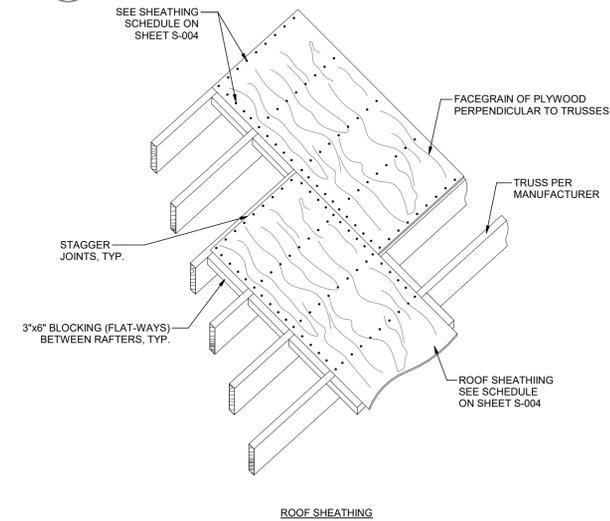
1 TYPICAL OPENING DETAILS
S-014 NOT TO SCALE



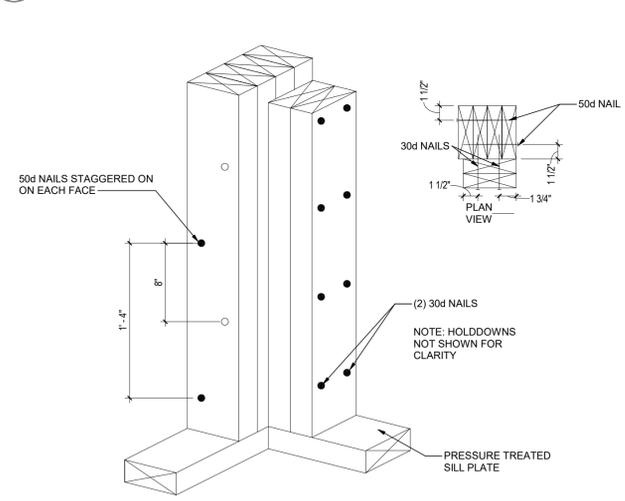
2 TOP PLATE TO STUD TYPICAL CONNECTION
S-014 NOT TO SCALE



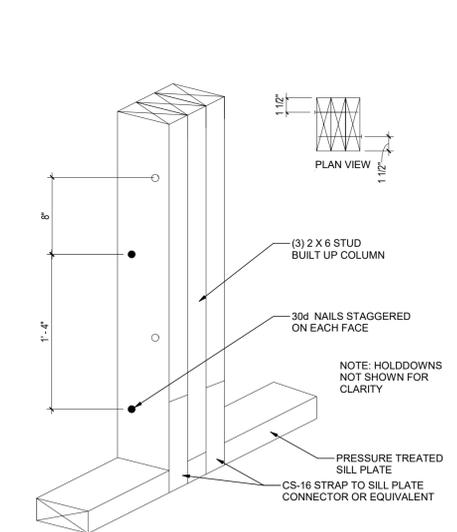
3 TYPICAL TRUSS TIEDOWN DETAIL
S-014 NOT TO SCALE



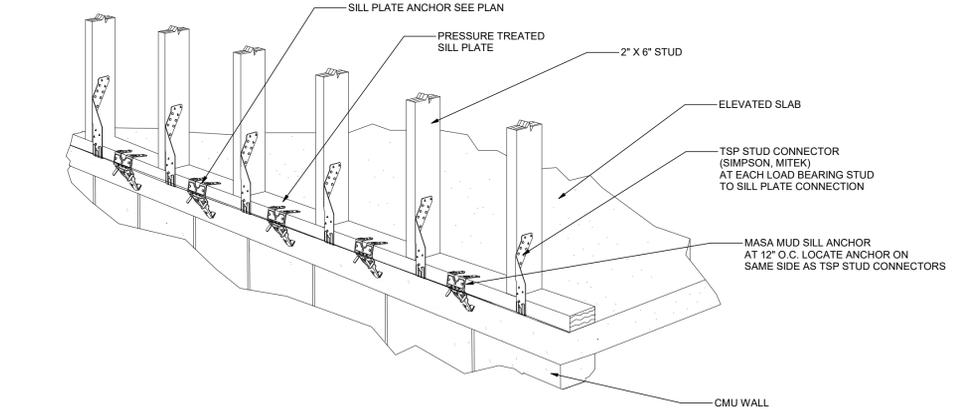
4 ROOF SHEATHING
S-014 NOT TO SCALE



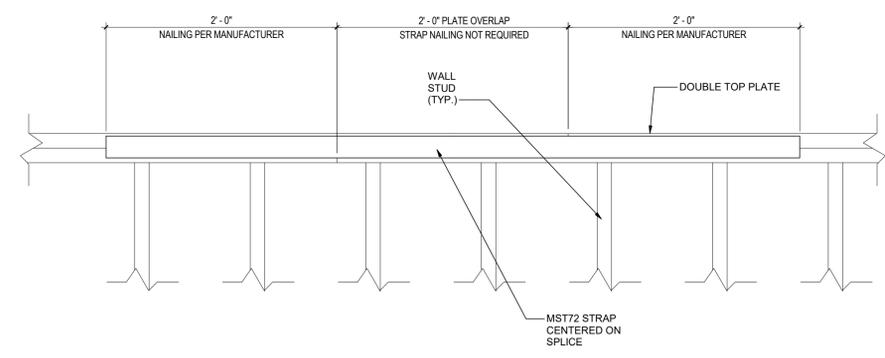
5 CORNER STUD PACK DETAIL
S-014 NOT TO SCALE



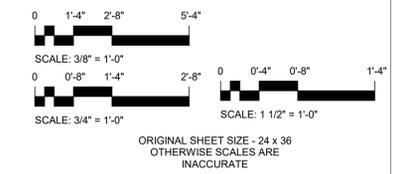
6 TYPICAL STUD PACK DETAIL
S-014 NOT TO SCALE



7 BASE OF WALL CONNECTION
S-014 NOT TO SCALE



8 TOP PLATE SPLICE DETAIL
S-014 1 1/2" = 1'-0"



NOT FOR CONSTRUCTION

CONSULTANT:
CLIENT:
PROJECT NAME:

TWO STORY CMU AND 2ND FL. WOOD HOME

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No.	Date	Description

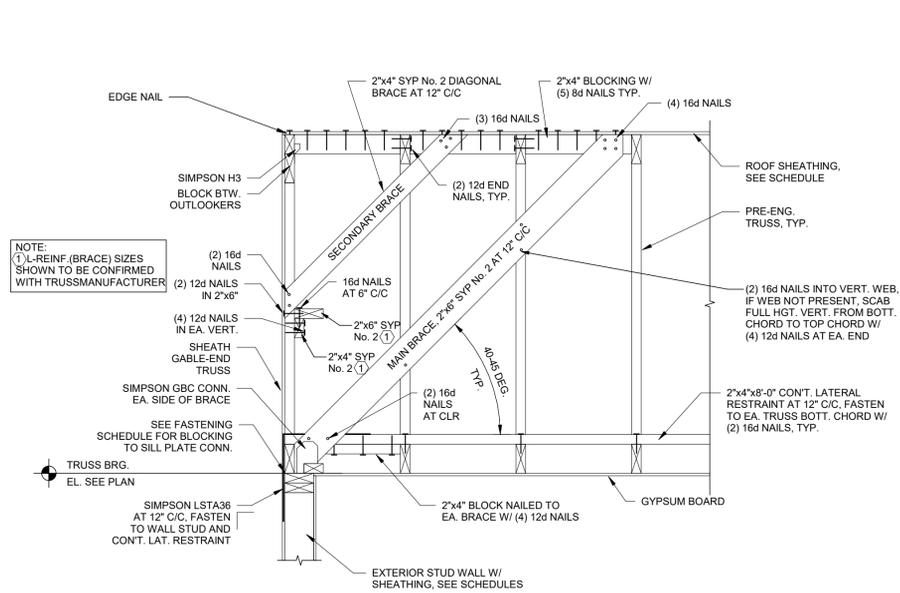
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SHEET TITLE:

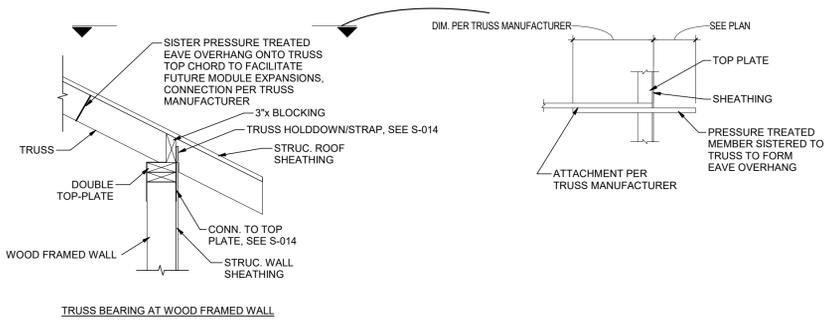
Wood Framing Details

SHEET INFORMATION:

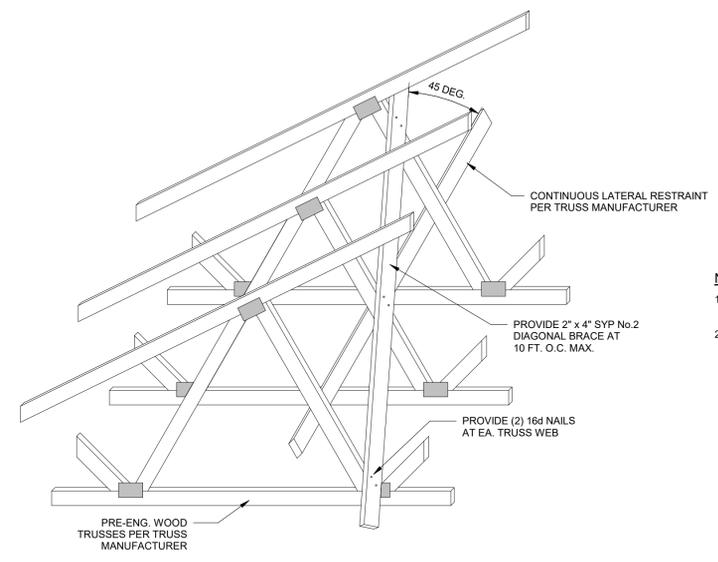
JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-014
QC Review:	Phase:



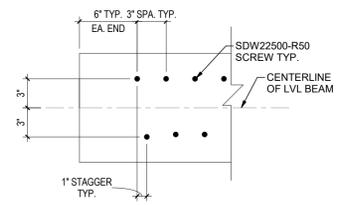
1 TYPICAL GABLE END BRACING DETAILS
 S-015 3/4" = 1'-0"



3 TYPICAL ROOF TRUSS BEARING
 S-015 3/4" = 1'-0"



2 BRACING AT CONTINUOUS LATERAL RESTRAINT (CLR)
 S-015 3/8" = 1'-0"



4 TYPICAL LVL BEAM PLY CONNECTION
 S-015 1 1/2" = 1'-0"

- NOTES:**
- CHECK THE TRUSS DESIGN DRAWINGS (TDD) TO DETERMINE WHICH WEB MEMBERS (IF ANY) REQUIRE RESTRAINT.
 - RESTRAIN AND BRACE WITH:
 - INDIVIDUAL WEB MEMBER REINFORCEMENT (PER THE TRUSS MANUFACTURER) OR CONTINUOUS LATERAL RESTRAINT (PER THE TRUSS MANUFACTURER) & DIAGONAL BRACING.
 - ATTACH EACH ROW OF CLR AT THE LOCATIONS SHOWN ON THE TDD.
 - INSTALL THE DIAGONAL BRACING SHOWN IN THE DETAIL AT AN ANGLE OF LESS THAN OR EQUAL TO 45 DEGREES TO THE CLR AND POSITION SO THAT IT CROSSES THE WEB IN CLOSE PROXIMITY TO THE CLR. ATTACH THE DIAGONAL BRACE AS CLOSE TO THE TOP AND BOTTOM CHORDS AS POSSIBLE AND TO EACH WEB IT CROSSES. REPEAT EVERY 10 FT. OR LESS.

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
 CMU AND 2ND
 FL. WOOD
 HOME**

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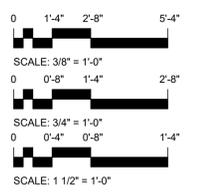
PROFESSIONAL SEALS:

SHEET TITLE:

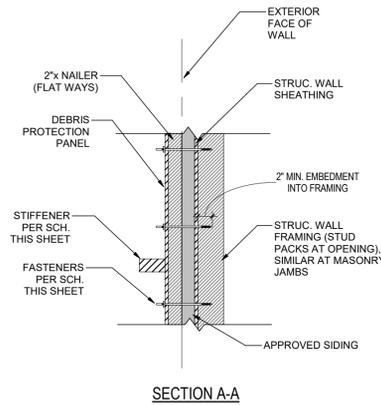
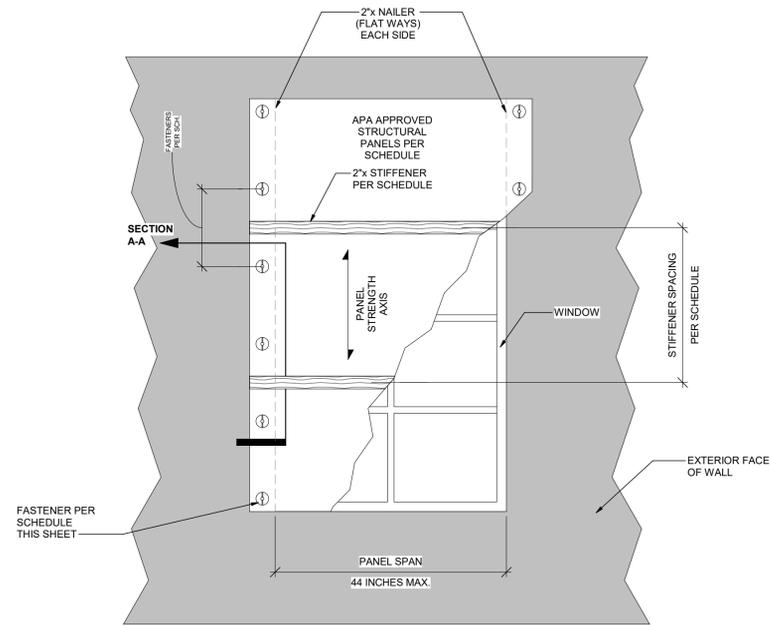
Wood Framing Details

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-015
QC Review:	Phase:



NOT FOR CONSTRUCTION



WIND-BORNE DEBRIS PROTECTION FOR GLAZED AND JALOUSIE WINDOW OPENINGS (NOT SUITABLE FOR SAFE ROOM)

NOTES:

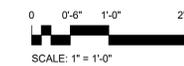
1. THE DETAIL'S INTENDED USE IS TO PROVIDE PROTECTION FROM WIND-BORNE DEBRIS. THE PREFERRED METHOD OF PROTECTION IS APPROVED IMPACT RESISTANT GLAZING OR APPROVED IMPACT RESISTANT COVERINGS (i.e. SHUTTER SYSTEM).
2. THE WOOD PANEL OPTION ONLY APPLIES TO OPENINGS WHICH DO NOT EXCEED 44 INCHES IN WIDTH. OPENINGS GREATER THAN 44 INCHES WIDE SHALL BE PROTECTED BY ONE OF THE PREFERRED METHODS MENTIONED IN THE ABOVE NOTE (NOTE #1).
3. DETAILS ARE ONLY APPLICABLE FOR ONE & TWO STORY BUILDINGS WITH A MEAN ROOF HEIGHT OF 30 FEET OR LESS.
4. ALL FASTENERS AND HARDWARE SHALL BE PERMANENTLY INSTALLED AND SHALL BE STAINLESS STEEL.
5. MIN. 3/4" DIAM. WASHER REQUIRED AT EXTERIOR PANEL ATTACHMENT.
6. MIN. 2" EMBEDMENT OF SCREW THREADS INTO WOOD WALL FRAMING.
7. STRUCTURAL PANELS SHALL BE APA RATED CDX PLYWOOD.
8. PANELS SHALL BE PRE-CUT AND PRE-DRILLED FOR INSTALLATION EFFICIENCY.
9. THE HOMEOWNER SHALL BE RESPONSIBLE FOR ROUTINE INSPECTION AND MAINTENANCE OF THE SYSTEM TO ENSURE FUNCTIONALITY FOR THE INTENDED PURPOSE DURING A STORM EVENT.
10. PANELS ATTACHED TO MASONRY SHALL BE ATTACHED USING VIBRATION-RESISTANT ANCHORS HAVING AN ULTIMATE WITHDRAWAL CAPACITY OF NOT LESS THAN 1,500 POUNDS.
11. MASONRY ANCHORS SHALL BE A MINIMUM OF 2.5 INCHES AWAY FROM WINDOW AND DOOR EDGES.
12. FASTENERS SHALL BE LOCATED NOT LESS THAN 1 INCH FROM THE EDGE OF THE PANEL.

DEBRIS PROTECTION-STRUCTURAL PANEL SCHEDULE REQUIREMENTS		
STRUCTURAL COMPONENT	PANEL SPAN	
	MAX. STRUCTURAL PANEL SPAN = 44 INCHES	
WOOD FRAMED	PANEL	5/8" APA RATED PRESSURE TREATED PLYWOOD
	FASTENER	1/4" DIAMETER LAG SCREWS AT 12" O.C.
	STIFFENER	2"x4" SYP No.2 PRESSURE TREATED AT 16" O.C.
MASONRY	PANEL	5/8" APA RATED PRESSURE TREATED PLYWOOD
	FASTENER	1/4" DIAMETER MASONRY SCREWS AT 12" O.C.
	STIFFENER	2"x4" SYP No.2 PRESSURE TREATED AT 16" O.C.

NOTES:

1. PANEL REQUIREMENTS SHOWN IN TABLE ABOVE ALSO CAN BE APPLIED AT DOOR OPENINGS WHICH DO NOT EXCEED 44 INCHES IN WIDTH.
2. FOR VENTED OPENINGS NOT EXCEEDING 2'-0" x 2'-0", PROVIDE PANEL WITH FASTENERS AS INDICATED IN TABLE ABOVE. STIFFENERS ARE NOT REQUIRED.

1 PLYWOOD WINDOW PROTECTION DETAIL
S-016 NOT TO SCALE



ORIGINAL SHEET SIZE - 24 x 36
OTHERWISE SCALES ARE
INACCURATE

NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND
FL. WOOD
HOME**

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No.	Date	Description

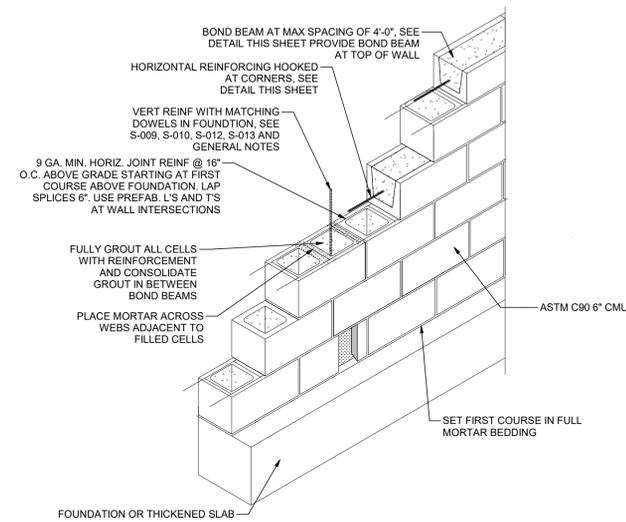
PROFESSIONAL SEALS:

SHEET TITLE:

Window Protection Details

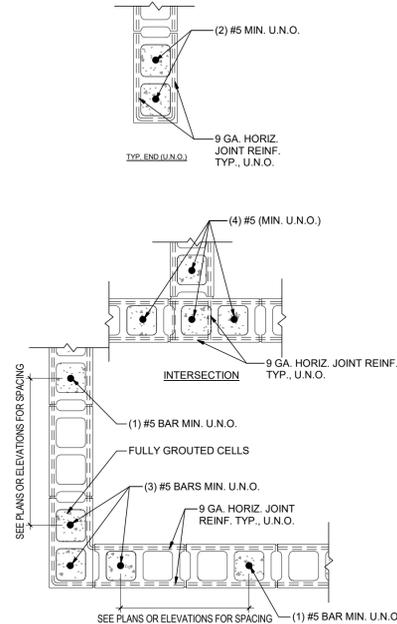
SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-016
QC Review:	Phase:



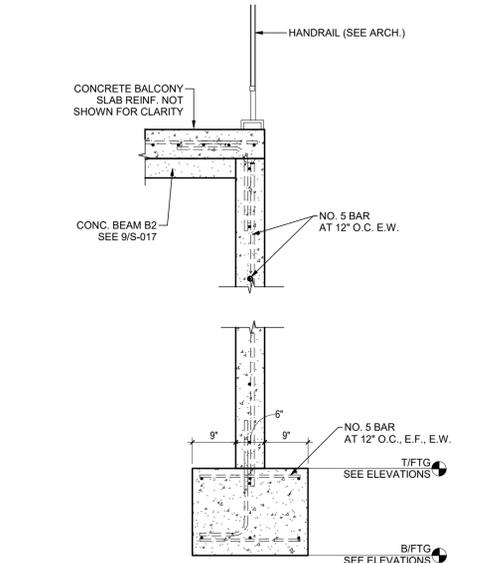
1 TYPICAL MASONRY WALL CONSTRUCTION

S-017 NOT TO SCALE



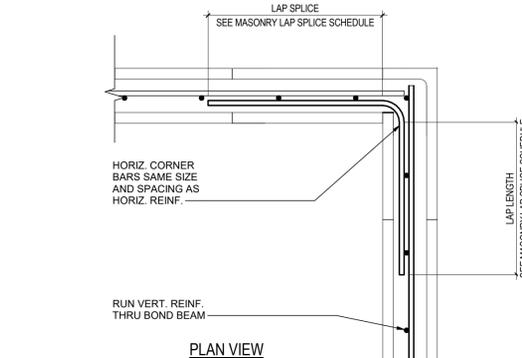
2 TYPICAL CMU CORNER DETAIL

S-017 1" = 1'-0"



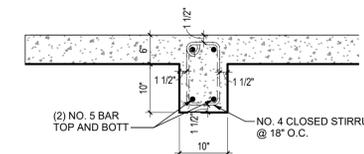
3A WALL SECTION AT WALL SUPPORTING EXTERIOR STAIR

S-017 3/4" = 1'-0"



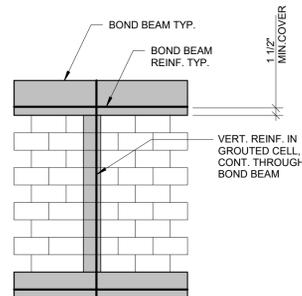
4 TYPICAL CORNER DETAIL AT BOND BEAM

S-017 1 1/2" = 1'-0"



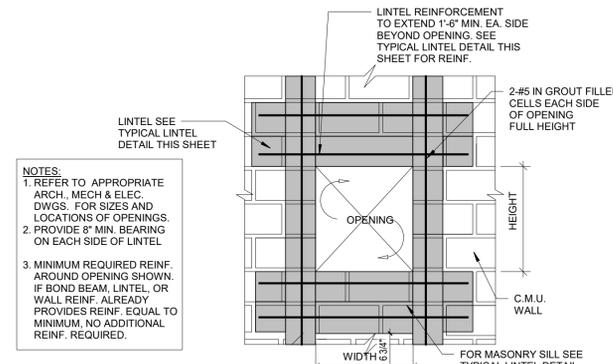
5 CONCRETE BEAM B1 SECTION

S-017 3/4" = 1'-0"



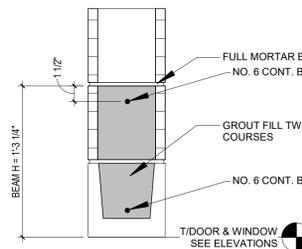
6 TYPICAL VERTICAL REINFORCING AT BOND BEAM

S-017 3/4" = 1'-0"



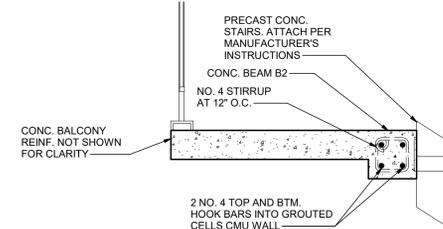
7 TYPICAL REINFORCING AROUND OPENINGS

S-017 NOT TO SCALE



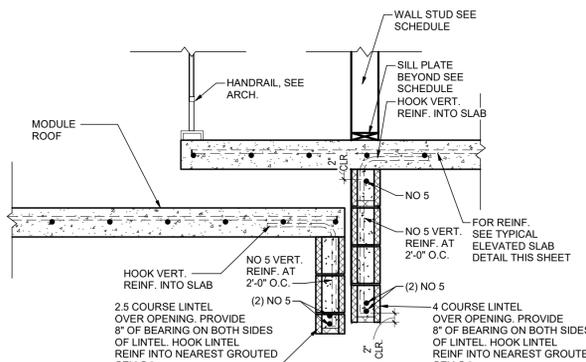
8 TYPICAL LINTEL DETAIL

S-017 NOT TO SCALE



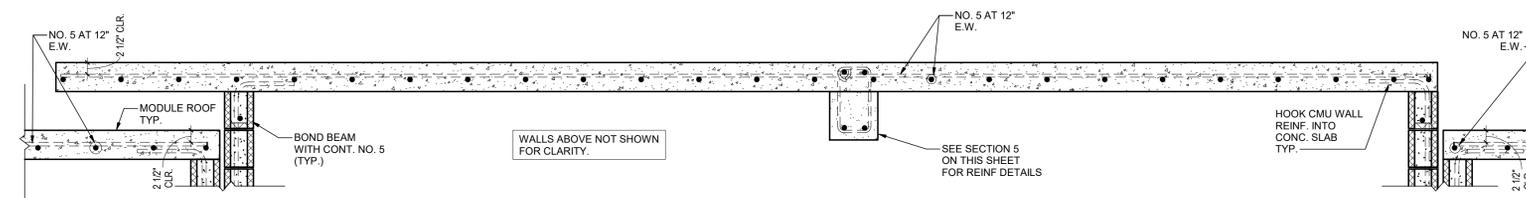
9 CONCRETE BEAM B2 SECTION

S-017 3/4" = 1'-0"



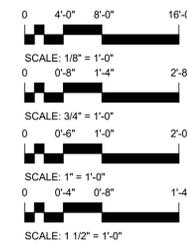
10 WALL SECTION

S-017 3/4" = 1'-0"



11 ELEV. SLAB DETAIL FOR PRIMARY STRUCTURE

S-017 3/4" = 1'-0"



ORIGINAL SHEET SIZE - 24 x 36
OTHERWISE SCALES ARE INACCURATE

NOT FOR CONSTRUCTION

CONSULTANT:

CLIENT:

PROJECT NAME:

**TWO STORY
CMU AND 2ND
FL. WOOD
HOME**

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ISSUE LOG

No.	Date	Description

PROFESSIONAL SEALS:

SHEET TITLE:

**Masonry and Concrete
Details**

SHEET INFORMATION:

JOB No.	Date Issued: 5/15/2020
Drawn By:	Sheet Number:
Checked By:	S-017
QC Review:	Phase:

STARR II

PR Prescriptive Homes Calculations

Two story
Wood/CMU
JOB TITLE House

JOB NO.	_____	SHEET NO.	_____
CALCULATED BY	SW	DATE	2/6/20
CHECKED BY	MH	DATE	2/6/20

CS2018 Ver 2018.03.17

www.struware.com

STRUCTURAL CALCULATIONS

FOR

PR Homes: Two story Wood/CMU House

PUERTO RICO

Code Search

Code: ASCE 7 - 16

Occupancy:

Occupancy Group = R Residential

Risk Category & Importance Factors:

Risk Category = II
Wind factor = 1.00
Snow factor = 1.00
Seismic factor = 1.00

Type of Construction:

Fire Rating:
Roof = 0.0 hr
Floor = 0.0 hr

Building Geometry:

Roof angle (θ) 4.00 / 12 18.4 deg
Building length (L) 24.0 ft
Least width (B) 20.0 ft
Mean Roof Ht (h) 20.5 ft
Parapet ht above grd
Minimum parapet ht

Live Loads:

Roof 0 to 200 sf: 20 psf
200 to 600 sf: 24 - 0.02Area, but not less than 12 psf
over 600 sf: 12 psf

Floor:

Typical Floor 40 psf
Partitions 15 psf
Lobbies & first floor corridors 100 psf
Corridors above first floor 80 psf
Balconies (1.5 times live load) 60 psf

STARR II

PR Prescriptive Homes Calculations

JOB TITLE PR Homes: Two story Wood/CMU House

JOB NO. _____ SHEET NO. _____
 CALCULATED BY SW DATE 2/6/20
 CHECKED BY MH DATE 2/6/20

Wind Loads :

ASCE 7- 16

Ultimate Wind Speed 190 mph
 Nominal Wind Speed 147.2 mph
 Risk Category II
 Exposure Category D
 Enclosure Classif. Partially Open Building
 Internal pressure +/-0.18
 Directionality (Kd) 0.85
 Kh case 1 1.088
 Kh case 2 1.088
 Type of roof Gable

Topographic Factor (Kzt)

Topography
 Hill Height (H)
 Half Hill Length (Lh)
 Actual H/Lh = 0.00
 Use H/Lh = 0.00
 Modified Lh = 0.0 ft
 From top of crest: x =
 Bldg up/down wind?

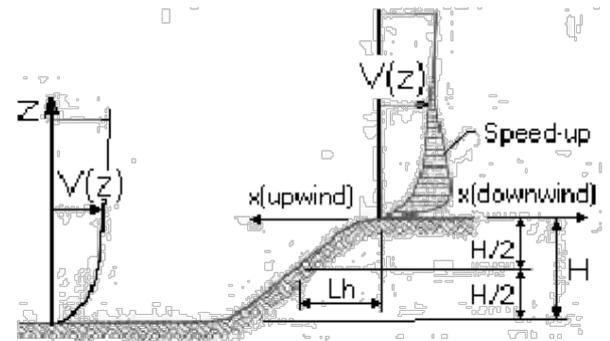
H/Lh = 0.00 $K_1 = 0.000$
 x/Lh = 0.00 $K_2 = 0.000$
 z/Lh = 0.00 $K_3 = 1.000$

At Mean Roof Ht:

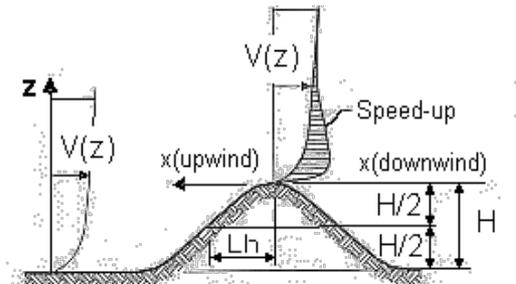
$K_{zt} = (1+K_1K_2K_3)^2 = 1.00$

use 1.00

H < 15ft; exp D
 $\therefore K_{zt} = 1.0$



ESCARPMENT



2D RIDGE or 3D AXISYMMETRICAL HILL

Gust Effect Factor

h = 20.5 ft
 B = 20.0 ft
 lz (0.6h) = 12.3 ft

Flexible structure if natural frequency < 1 Hz (T > 1 second).
 If building h/B > 4 then may be flexible and should be investigated.
 h/B = 1.03

G = 0.85 Using rigid structure default

Rigid Structure

$\bar{e} = 0.13$
 $l = 650$ ft
 $Z_{min} = 7$ ft
 $c = 0.13$
 $g_Q, g_v = 3.4$
 $L_z = 574.7$ ft
 $Q = 0.95$
 $I_z = 0.15$
 $G = 0.90$ use $G = 0.85$

Flexible or Dynamically Sensitive Structure

34 rcy (η_1) = 0.0 Hz
 Damping ratio (β) = 0
 $b = 0.80$
 $\alpha = 0.11$
 $V_z = 199.8$
 $N_1 = 0.00$
 $R_n = 0.000$
 $R_h = 28.282$ $\eta = 0.000$ h = 20.5 ft
 $R_B = 28.282$ $\eta = 0.000$
 $R_L = 28.282$ $\eta = 0.000$
 $g_R = 0.000$
 $R = 0.000$
 $G_f = 0.000$

Enclosure Classification

Test for Enclosed Building: $A_o < 0.01A_g$ or 4 sf, whichever is smaller

Test for Open Building: All walls are at least 80% open.
 $A_o \geq 0.8A_g$

Test for Partially Enclosed Building: Predominately open on one side only

	Input		Test	
Ao	500.0	sf	$A_o \geq 1.1A_{oi}$	NO
Ag	600.0	sf	$A_o > 4'$ or $0.01A_g$	YES
Aoi	1000.0	sf	$A_{oi} / A_{gi} \leq 0.20$	YES
Agi	10000.0	sf		

Building is NOT Partially Enclosed

Conditions to qualify as Partially Enclosed Building. Must satisfy all of the following:

- $A_o \geq 1.1A_{oi}$
- $A_o >$ smaller of 4' or $0.01 A_g$
- $A_{oi} / A_{gi} \leq 0.20$

Where:

- A_o = the total area of openings in a wall that receives positive external pressure.
- A_g = the gross area of that wall in which A_o is identified.
- A_{oi} = the sum of the areas of openings in the building envelope (walls and roof) not including A_o .
- A_{gi} = the sum of the gross surface areas of the building envelope (walls and roof) not including A_g .

Test for Partially Open Building: A building that does not qualify as open, enclosed or partially enclosed.
 (This type building will have same wind pressures as an enclosed building.)

Reduction Factor for large volume partially enclosed buildings (Ri) :

If the partially enclosed building contains a single room that is unpartitioned , the internal pressure coefficient may be multiplied by the reduction factor Ri.

Total area of all wall & roof openings (A_{og}):	0 sf
Unpartitioned internal volume (V_i) :	0 cf
Ri =	1.00

Ground Elevation Factor (Ke)

Grd level above sea level =	0.0 ft	Ke =	1.0000
Constant =	0.00256	Adj Constant =	0.00256

STARR II

PR Prescriptive Homes Calculations

JOB TITLE PR Homes: Two story Wood/CMU House

JOB NO. _____ SHEET NO. _____
 CALCULATED BY SW DATE 2/6/20
 CHECKED BY MH DATE 2/6/20

Wind Loads - MWFRS all h (Except for Open Buildings)

Kh (case 2) = 1.09 h = 20.5 ft GCpi = +/-0.18
 Base pressure (qh) = **85.5 psf** ridge ht = 22.4 ft G = 0.85
 Roof Angle (θ) = 18.4 deg L = 24.0 ft qi = qh
 Roof tributary area - (h/2)*L: 247 sf B = 20.0 ft
 (h/2)*B: 205 sf

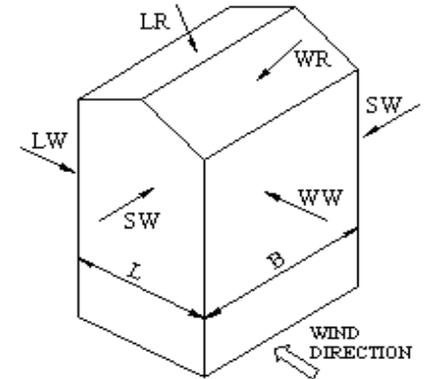
Ultimate Wind Surface Pressures (psf)

Surface	Wind Normal to Ridge				Wind Parallel to Ridge				
	B/L = 0.83		h/L = 1.03		L/B = 1.20		h/L = 0.86		
	Cp	qhGCp	w/+qiGCpi	w/-qhGCpi	Dist.*	Cp	qhGCp	w/+qiGCpi	w/-qhGCpi
Windward Wall (WW)	0.80	58.1	see table below			0.80	58.1	see table below	
Leeward Wall (LW)	-0.50	-36.3	-51.7	-20.9		-0.46	-33.4	-48.8	-18.0
Side Wall (SW)	-0.70	-50.9	-66.2	-35.5		-0.70	-50.9	-66.2	-35.5
Leeward Roof (LR)	-0.60	-43.6	-59.0	-28.2		Included in windward roof			
Neg Windward Roof pressure	-0.79	-57.7	-73.1	-42.3	0 to h/2*	-1.09	-79.3	-94.7	-63.9
Pos/min Windward Roof press.	-0.18	-13.1	-28.5	2.3	h/2 to h*	-0.76	-55.0	-70.4	-39.7
					h to 2h*	-0.64	-46.7	-62.1	-31.3
					Min press.	-0.18	-13.1	-28.5	2.3

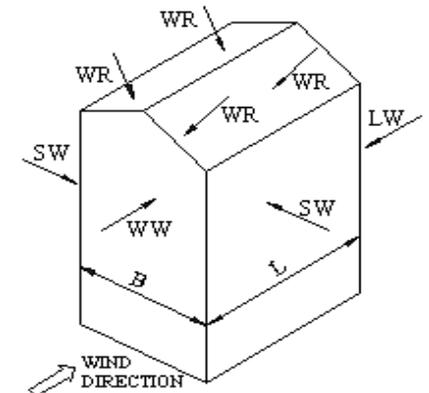
*Horizontal distance from windward edge

Windward Wall Pressures at "z" (psf)

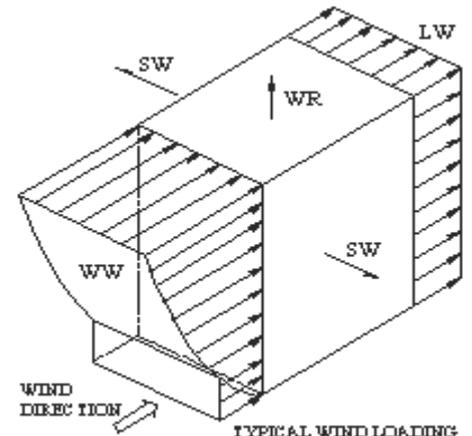
z	Kz	Kzt	Windward Wall			Combined WW + LW	
			qzGCp	w/+qiGCpi	w/-qhGCpi	Normal to Ridge	Parallel to Ridge
0 to 15'	1.03	1.00	55.0	39.6	70.4	91.4	88.5
20.0 ft	1.08	1.00	57.9	42.5	73.2	94.2	91.3
h = 20.5 ft	1.09	1.00	58.1	42.7	73.5	94.5	91.5
ridge = 22.4 ft	1.10	1.00	59.0	43.6	74.4	95.3	92.4



WIND NORMAL TO RIDGE



WIND PARALLEL TO RIDGE



TYPICAL WIND LOADING

NOTE:
 See figure in ASCE7 for the application of full and partial loading of the above wind pressures. There are 4 different loading cases.

Parapet

z	Kz	Kzt	qp (psf)
0.0 ft	1.03	1.00	0.0

Windward parapet: 0.0 psf (GCpn = +1.5)
 Leeward parapet: 0.0 psf (GCpn = -1.0)

Windward roof overhangs (add to windward roof pressure) : 58.1 psf (upward)

ASCE 7-16 Wind Component and Cladding Two story home modules only

(ASCE 7-16 Part 1 Pg 591)

MRH= 8.67
 Kzt = 1
 Kz = 1 ASCE 7-16 Table 26.10
 Kd = 0.85 ASCE 7-16 Table 26.6-1
 V = 250
 qz = 136 psf
 Gcpi = 0.18 ASCE 7-16 Figure 26.10-1

GCp Values ASCE 7-16 Fig 30.4-2B

	10sf	50sf	100sf
ZONE 1	-1.7	-1.4	-1.3
ZONE 1'	-0.9	-0.9	-0.9
ZONE 2	-2.3	-1.9	-1.9
POS ALL	0.3	0.23	0.2
ZONE 3	-3.2	-2.88	-2.46

Note Pressures for one story no modules and one story wood with modules are the same b/c MRH <15'

Roof C&C Pressures

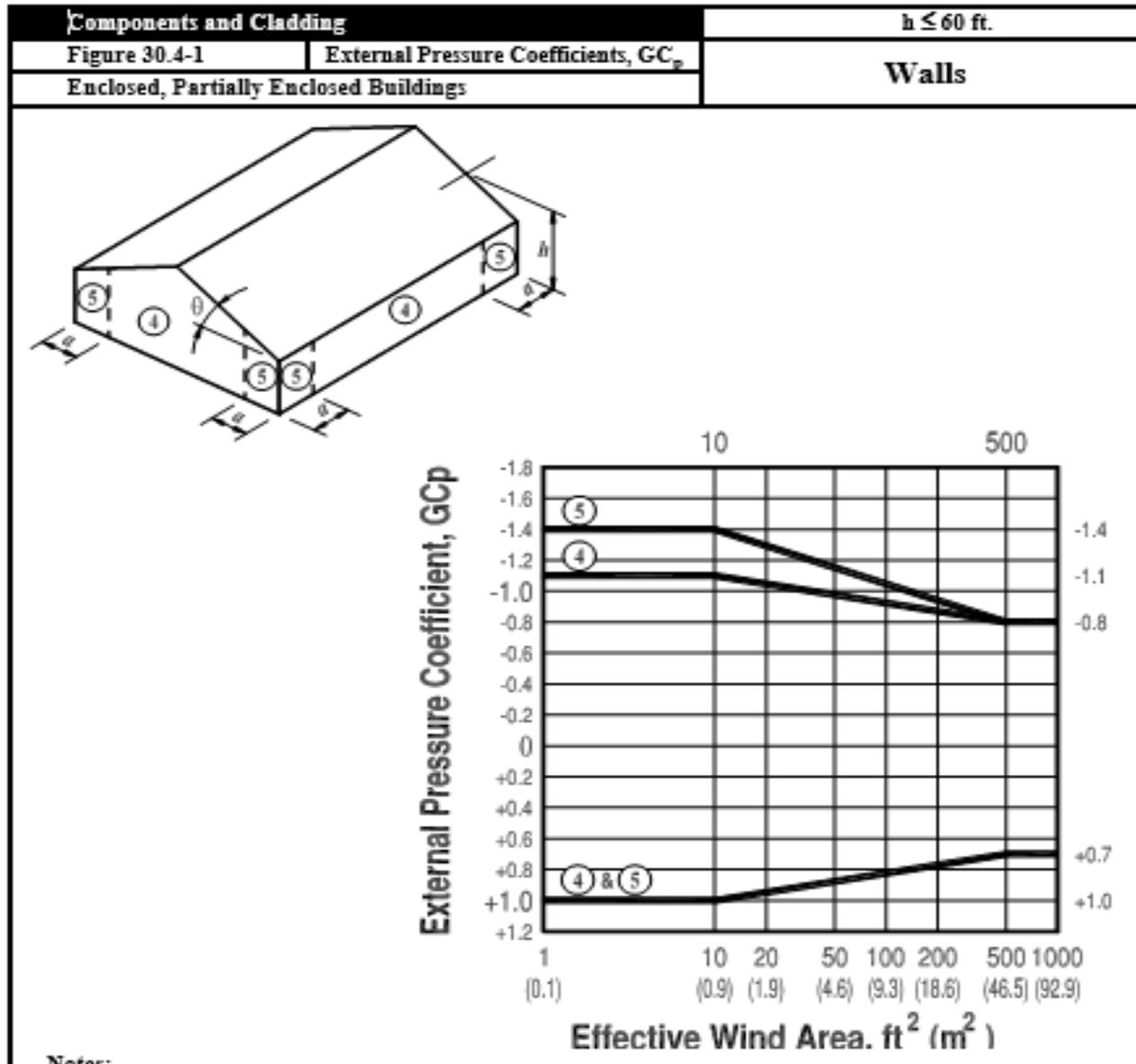
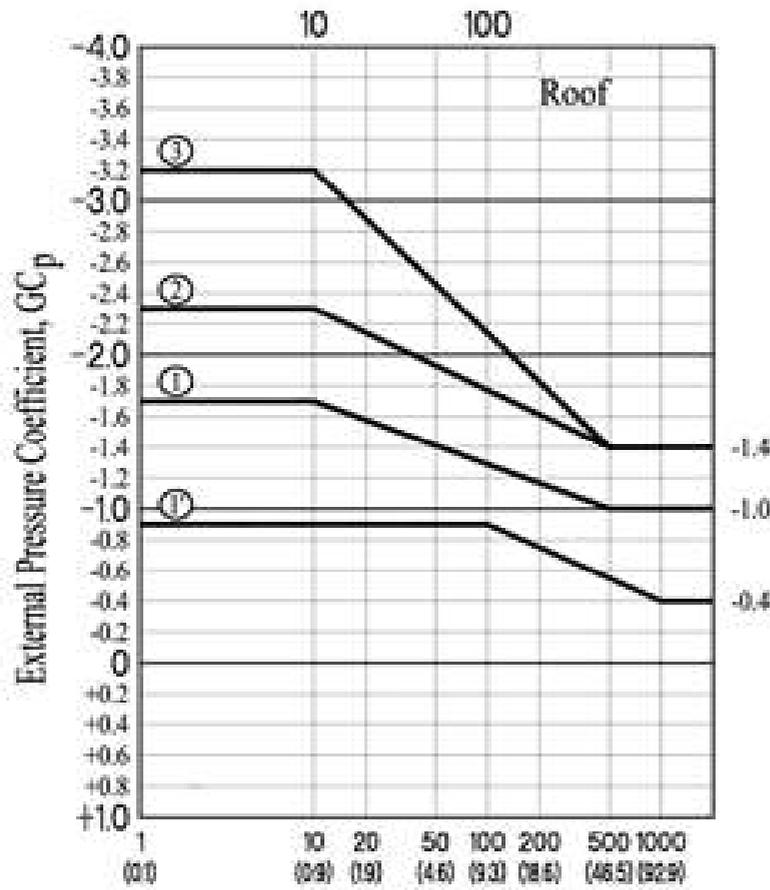
	10sf	50sf	100sf
ZONE 1	-255.7	-214.9	-201.3
ZONE 1'	-146.9	-146.9	-146.9
ZONE 2	-337.3	-282.9	-282.9
POS ALL	65.3	55.8	51.7
ZONE 3	-459.7	-416.2	-359.0

Wall GCp Values ASCE 7-16 Fig 30.4-1

	10sf	50sf	100sf
NEG 4	-1.1	-1	-0.9
NEG 5	-1.4	-1.18	-1.1
POS 4 & 5	1	0.9	0.8

Wall C & C Pressures

	10sf	50sf	100sf
NEG 4	-174.08	-160.48	-146.88
NEG 5	-214.88	-184.96	-174.08
POS 4 & 5	160.48	146.88	133.28



Notes:

ASCE 7-16 Wind Component and Cladding Two story home no modules

(ASCE 7-16 Part 1 Pg 591)

MRH= 20.45
 Kzt = 1
 Kz = 1.09 ASCE 7-16 Table 26.10
 Kd = 0.85 ASCE 7-16 Table 26.6-1
 V = 190
 qz = 85.623424 psf
 Gcpi = 0.18 ASCE 7-16 Figure 26.10-1

GCP Values ASCE 7-16 Fig 30.4-2B

	10sf	50sf	100sf
NEG 1 & 2E	-2	-1.1	-0.5
NEG 2N, 2R, & 3E	-3	-2	-1.6
NEG 3R	-3.6	-2.4	-1.8
POS ALL	0.5	0.39	0.3
OVERHANG 1 & 2E	-2.5	-2.19	-1.9
OVERHANG 2N&2R	-3.5	-2.5	-2
OVERHANG 3E	-4.1	-2.8	-2.3
OVERHANG 3R	-4.7	-3	-2.3

Note Pressures for one story no modules and one story wood with modules are the same b/c MRH <15'

Roof C&C Pressures

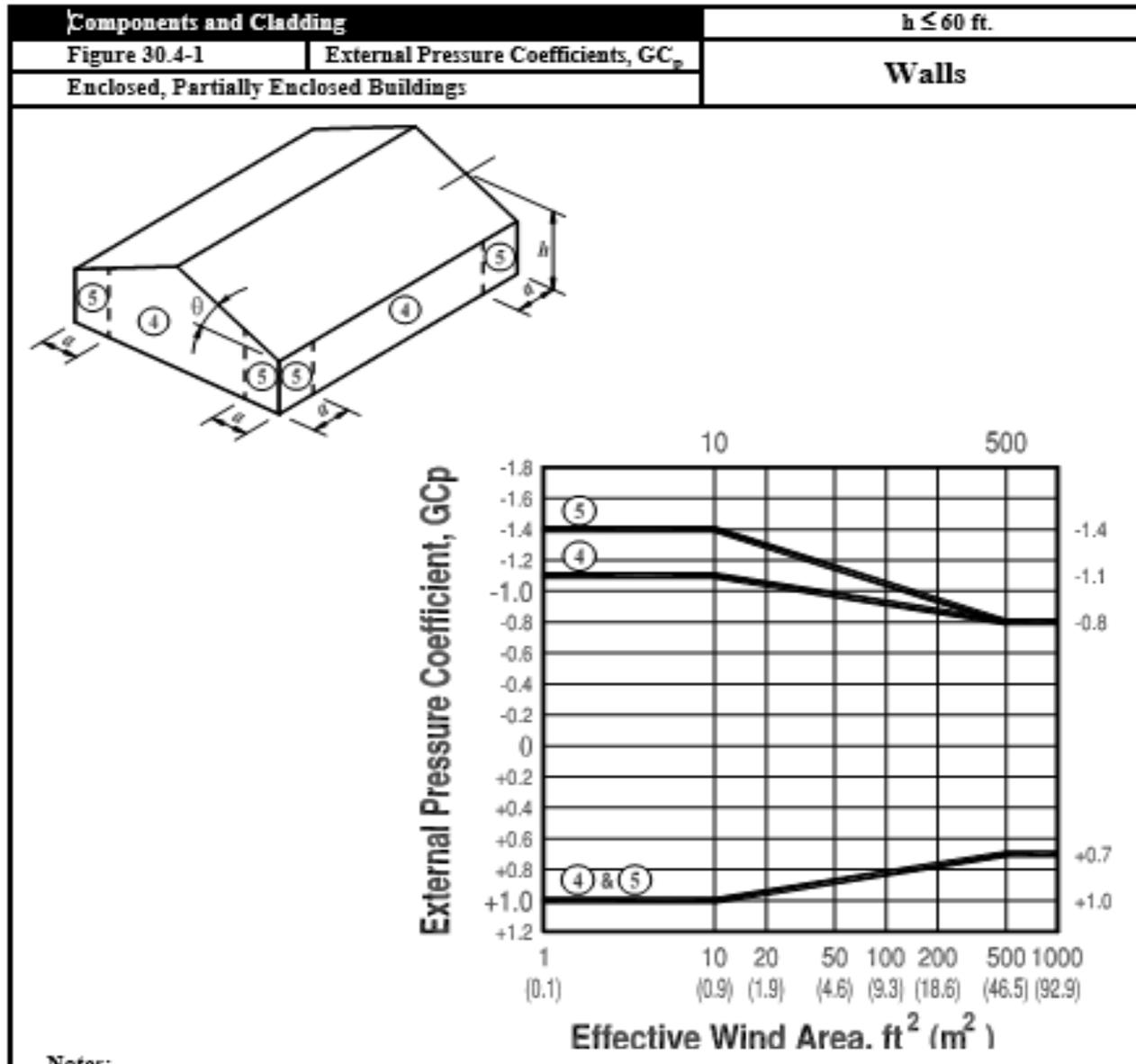
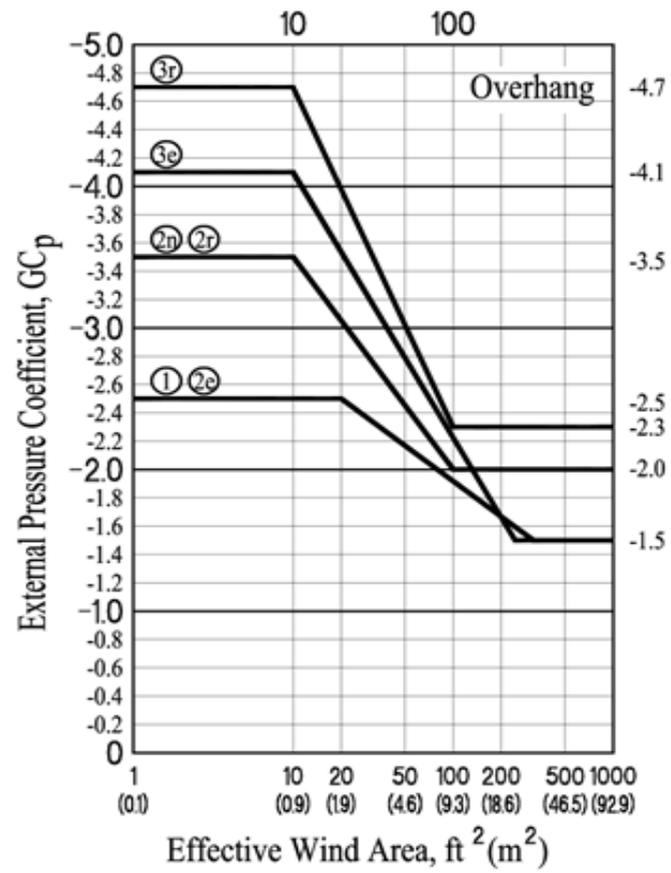
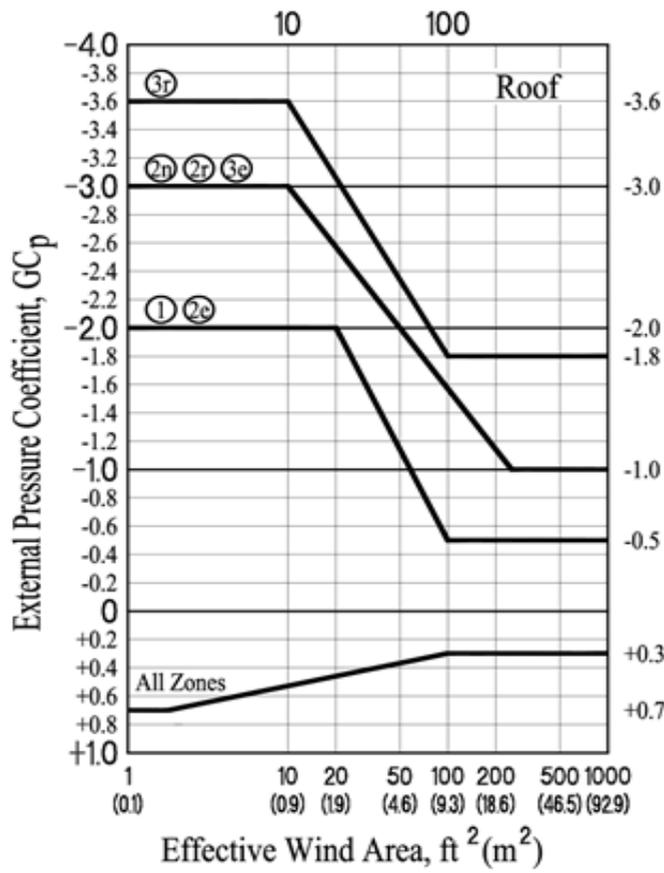
	10sf	50sf	100sf
NEG 1 & 2E	-186.7	-109.6	-58.2
NEG 2N, 2R, & 3E	-272.3	-186.7	-152.4
NEG 3R	-323.7	-220.9	-169.5
POS ALL	58.2	48.8	41.1
OVERHANG 1 & 2E	-229.5	-202.9	-178.1
OVERHANG 2N&2R	-315.1	-229.5	-186.7
OVERHANG 3E	-366.5	-255.2	-212.3
OVERHANG 3R	-417.8	-272.3	-212.3

Wall GCp Values ASCE 7-16 Fig 30.4-1

	10sf	50sf	100sf
NEG 4	-1.1	-1	-0.9
NEG 5	-1.4	-1.18	-1.1
POS 4 & 5	1	0.9	0.8

Wall C & C Pressures

	10sf	50sf	100sf
NEG 4	-109.598	-101.036	-92.4733
NEG 5	-135.285	-116.448	-109.598
POS 4 & 5	101.0356	92.4733	83.91096



ASCE 7-16 Wind Component and Cladding Two story home One Story Option

(ASCE 7-16 Part 1 Pg 591)

MRH= 11.42
 Kzt = 1
 Kz = 1.03 ASCE 7-16 Table 26.10
 Kd = 0.85 ASCE 7-16 Table 26.6-1
 V = 190
 qz = 80.910208 psf
 Gcpi = 0.18 ASCE 7-16 Figure 26.10-1

GCp Values ASCE 7-16 Fig 30.4-2B

	10sf	50sf	100sf
ZONE 1	-1.7	-1.4	-1.3
ZONE 1'	-0.9	-0.9	-0.9
ZONE 2	-2.3	-1.9	-1.9
POS ALL	0.3	0.23	0.2
ZONE 3	-3.2	-2.88	-2.46

Note Pressures for one story no modules and one story wood with modules are the same b/c MRH <15'

Roof C&C Pressures

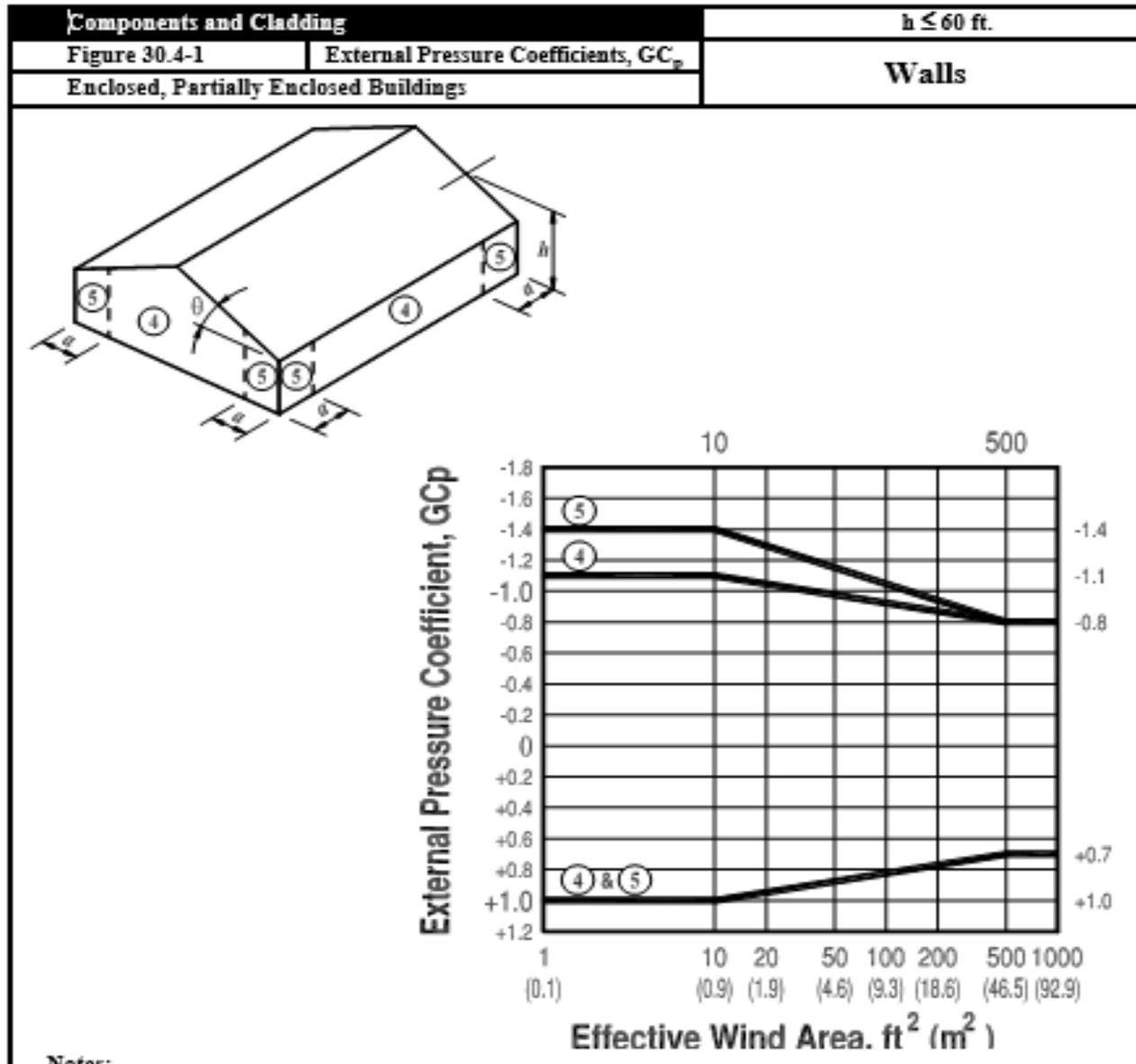
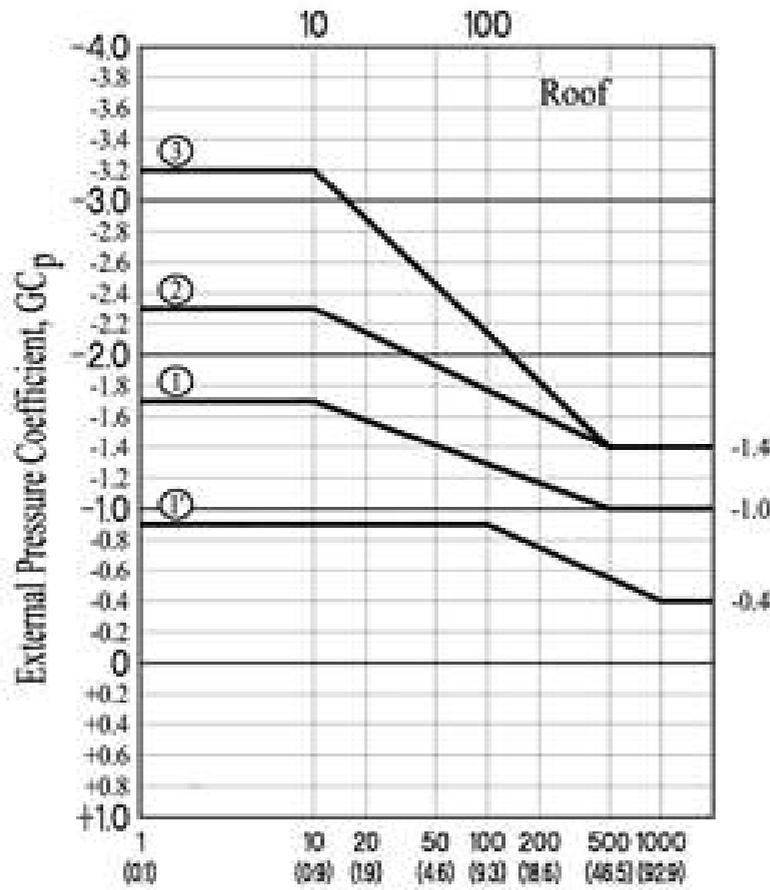
	10sf	50sf	100sf
ZONE 1	-152.1	-127.8	-119.7
ZONE 1'	-87.4	-87.4	-87.4
ZONE 2	-200.7	-168.3	-168.3
POS ALL	38.8	33.2	30.7
ZONE 3	-273.5	-247.6	-213.6

Wall GCp Values ASCE 7-16 Fig 30.4-1

	10sf	50sf	100sf
NEG 4	-1.1	-1	-0.9
NEG 5	-1.4	-1.18	-1.1
POS 4 & 5	1	0.9	0.8

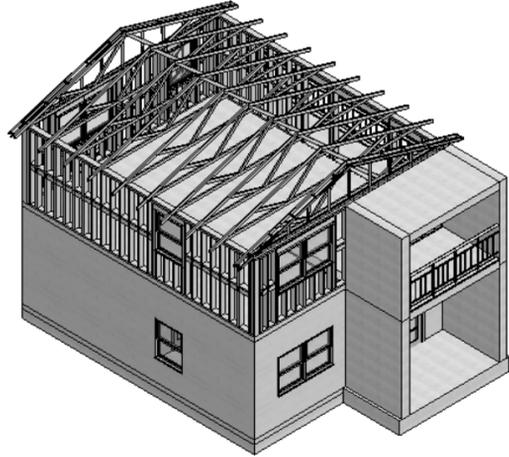
Wall C & C Pressures

	10sf	50sf	100sf
NEG 4	-103.565	-95.474	-87.383
NEG 5	-127.838	-110.038	-103.565
POS 4 & 5	95.47405	87.38302	79.292

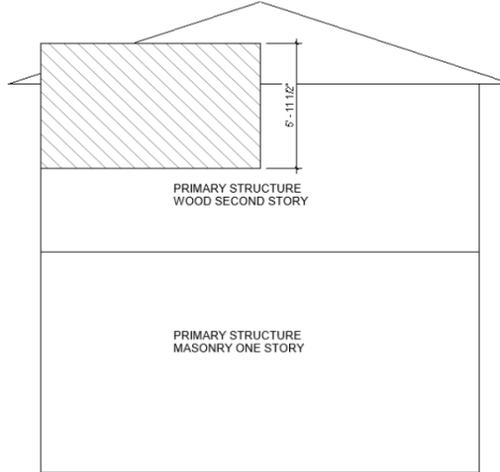


Notes:

ASD WIND PRESSURES								
	Windward Wall Pressures at "z" (psf)						Combined WW + LW	
	z	Kz	Kzt	Windward Wall			Normal	Parallel
qzGCp				w/+qiGCpi	w/-qhGCpi	to Ridge	to Ridge	
	0 to 15'	1.0	1.0	55.0	23.8	42.3	54.8	53.1
h=	20	1.0	1.0	57.9	25.5	43.9	56.5	54.8
ridge =	22.4	1.1	1.0	59.0	26.2	44.6	57.2	55.5



Note: Modules not included because they are acting independent of the primary structure and are not hard attached.

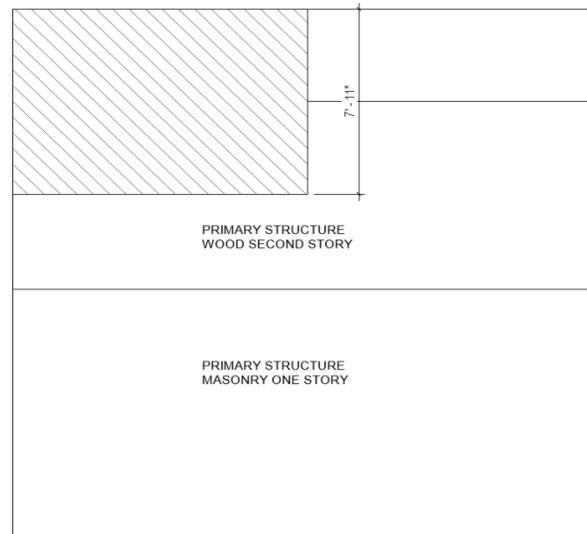


Roof Diaphragm Load Primary Structure Wind Parallel to Ridge:

B =	24	ft	o/o
Wall Ht. Wood =	8.00	ft	
Roof Ht. Above 2nd story =	11.90	ft	
Roof Ht. Avg =	9.95	ft	
Diaphragm Trib Area/ft =	5.95	Ft ² /ft	
Diaphragm Load/ft Main =	330	lb/ft	
Diaphragm Shear/Ft =	137	lb/ft	
Wall Shear 24' Wall Primary	3300	lb	
Diaphragm Moment =	23758	lb*ft	
Diaphragm Chord T/C =	1188	lbs	
Diaphragm Chord T/C per ft =	49	lbs/ft	Doesn't control

TRIBUTARY FOR SHEAR WALL WIND PARALLEL TO RIDGE

Note: Diaphragm transfers load to two adjacent shear walls



TRIBUTARY FOR SHEAR WALL WIND PERPENDICULAR TO RIDGE

Roof Diaphragm Load Primary Structure Wind Perpendicular to Ridge:

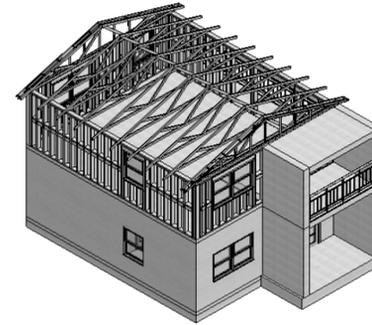
B =	20	ft	o/o
Wall Ht. =	8.00	ft	
Roof Ht. Above 2nd Story =	11.90	ft	
Roof Ht. Avg =	11.90	ft	
Diaphragm Trib Area/ft =	7.90	Ft ² /ft	
Diaphragm Load/ft =	452	lb/ft	
Diaphragm Total Shear/ft =	226	lb/ft	
Wall Shear 20' Wall =	4519	lbs	ASD
Diaphragm Moment =	22594	lb*ft	
Diaphragm Chord T/C =	941	lbs	
Diaphragm Chord T/C per ft =	47	lbs/ft	Doesn't control

Seismic Forces	
Ss =	1.35
S1 =	0.53
Sms =	1.35
Sm1 =	0.795
Sds =	0.9045
Sd1 =	0.3551
CMU R =	5
Wood R =	6.5
Cs second story wood =	0.1392
Cs first story CMU =	0.1809
Wall Weight CMU =	60 psf
Wall Weight CMU total primary =	53 kips
Wall Weight CMU total module =	33 kips
Wall Weight Wood =	20 psf
Wall Weight Wood total =	14.08 kips
Slab Weight primary =	36 kips
Slab Weight module =	18 kips
Roof Weight wood =	13.44 kips
Wal Avg Height =	10 ft
Wall Seismic Pressure Wood =	2.78 psf
Wall Seismic Pressure CMU =	10.854 psf
Fpx Diaphragm Min = 0.2*Sds*Ie*w =	0.18
By Inspection Doesn't Control	
Wall Anchorage Min = 0.4Sds*ka*Ie*Wp =	0.515
Wall Anchorage Design Pressure =	10.3 psf
CMU Base Shear primary =	16.06 kips
Wood Base Shear 2nd story =	3.83 kips
CMU Base Shear Module =	9.16 kips
ASD CMU Base Shear Primary/ Shear Wall =	4.82 kips
ASD Wood Base Shear Primary/Shear Wall =	1.15 kips

Doesn't Control
Doesn't Control

Doesn't Control

Doesn't Control See CMU Wind Base Shears
Doesn't Control See Wind Base Shears Wood



RATED PANELS DESIGN CAPACITIES								
Span Rating	Stress Parallel to Strength Axis				Stress Perpendicular to Strength Axis			
	Plywood		OSB		Plywood		OSB	
	3-ply	4-ply	5-ply		3-ply	4-ply	5-ply	
PANEL BENDING STIFFNESS, EI (lb-in.²/ft of panel width)								
24/0	66,000	66,000	66,000	60,000	3,600	7,900	11,000	11,000
24/16	86,000	86,000	86,000	78,000	5,200	11,500	16,000	16,000
32/16	125,000	125,000	125,000	115,000	8,100	18,000	25,000	25,000
40/20	250,000	250,000	250,000	225,000	18,000	39,500	56,000	56,000
48/24	NA	440,000	440,000	400,000	NA	65,000	91,500	91,500
16 oc	165,000	165,000	165,000	150,000	11,000	24,000	34,000	34,000
20 oc	230,000	230,000	230,000	210,000	13,000	28,500	40,500	40,500
24 oc	NA	330,000	330,000	300,000	NA	57,000	80,500	80,500
32 oc	NA	NA	715,000	650,000	NA	NA	235,000	235,000
48 oc	NA	NA	1,265,000	1,150,000	NA	NA	495,000	495,000
Structural I Multiplier								
	1.0	1.0	1.0	1.0	1.5	1.5	1.6	1.6
PANEL BENDING STRENGTH, F_sS (lb-in./ft of panel width)								
24/0	250	275	300	300	54	65	97	97
24/16	320	350	385	385	64	77	115	115
32/16	370	405	445	445	92	110	165	165
40/20	625	690	750	750	150	180	270	270
48/24	NA	930	1,000	1,000	NA	270	405	405
16 oc	415	455	500	500	100	120	180	180
20 oc	480	530	575	575	140	170	250	250
24 oc	NA	705	770	770	NA	260	385	385
32 oc	NA	NA	1,050	1,050	NA	NA	685	685
48 oc	NA	NA	1,900	1,900	NA	NA	1,200	1,200

APA PANEL BENDING CAPACITY

Table A
Wood Structural Panel Design Capacities Based on Span Ratings^(a)

Span Rating	Strength						Planar Shear F _v (lb/Q)	Stiffness and Rigidity						
	Bending F _s S (lb-in/ft of width)	Axial Tension F _t A (lb/ft of width)	Axial Compression F _c A (lb/ft of width)	Shear through the thickness F _v t _s (lb/in of shear-resisting panel length)	Planar Shear F _v (lb/Q)	Bending EI (lb-in ² /ft of width)		Axial EA (lb/ft of width x 10 ³)	Rigidity through the thickness G, t _s (lb/in of panel depth)					
	Capacities relative to strength axis ^(a)													
	0°	90°	0°	90°	0°	90°	0° / 90°	0°	90°	0°	90°	0°	90°	0° / 90°
Sheathing Span^(b)														
24/0 3-ply	250	54	2,300	600	2,850	2,500	53	156	273	66,000	3,600	3.35	2.90	25,000
32/16 3-ply	370	92	2,800	1,250	3,550	3,100	62	198	347	126,500	8,100	4.15	3.60	27,000
4-ply	407	110	2,800	1,250	5,325	4,650	81	198	479	126,500	17,820	4.15	3.60	35,100
5-ply	444	166	3,640	1,625	5,325	4,650	93	215	165	126,500	25,110	4.15	3.60	40,500
40/20 3-ply	625	150	2,900	1,600	4,200	4,000	68	246	431	247,500	18,000	5.00	4.50	28,500
4-ply	688	180	2,900	1,600	6,300	6,000	88	246	595	247,500	39,600	5.00	4.50	37,050
5-ply	750	270	3,770	2,080	6,300	6,000	102	267	205	247,500	55,800	5.00	4.50	42,750
48/24 4-ply	930	270	4,000	1,950	7,500	7,200	98	300	725	440,000	64,900	5.85	5.00	40,300
5-ply	1,014	405	5,200	2,535	7,500	7,200	113	325	250	440,000	91,450	5.85	5.00	46,500

APA WOOD PANEL SHEAR CAPACITIES

Model No.	Strap Length (in.)	Total Quantity of Fasteners		DF/SP Allowable Uplift Loads (160)		SPF/HF Allowable Uplift Loads (160)		Code Ref.
		0.148" x 3" Nails	0.148" x 1 1/2" Nails	0.148" x 3" Nails	0.148" x 1 1/2" Nails	0.148" x 3" Nails	0.148" x 1 1/2" Nails	
LTS12	12							IBC, FL, LA
LTS16	16	12	12	660	600	570	515	
LTS20	20							
MTS12	12							FL
MTS16	16							
MTS20	20	14	14	990	990	850	850	
MTS30	30							
MTS24C	24							
MTS30C	30							
HTS16	16	16	16	1,310	1,310	1,125	1,125	IBC, FL, LA
HTS20	20							
HTS24	24	20	24	1,310	1,310	1,125	1,125	
HTS30	30							
HTS30C	30							

MTS STRAP CAPACITY

Table 4.2A Nominal Unit Shear Capacities for Wood-Frame Diaphragms

Blocked Wood Structural Panel Diaphragms^{1,2,3,4,5}

Sheathing Grade	Common Nail Size	Minimum Fastener Penetration in Framing Member or Blocking (in.)	Minimum Nominal Panel Thickness (in.)	Minimum Nominal Width of Nailed Face at Adjoining Panel Edges and Boundaries (in.)	A SEISMIC												B WIND							
					Nail Spacing (in.) at diaphragm boundaries (all cases), at continuous panel edges parallel to load (Cases 3 & 4), and at all panel edges (Cases 5 & 6)												Nail Spacing (in.) at diaphragm boundaries (all cases), at continuous panel edges parallel to load (Cases 3 & 4), and at all panel edges (Cases 5 & 6)							
					6			4			2-1/2			2			6	4	2-1/2	2				
					Nail Spacing (in.) at other panel edges (Cases 1, 2, 3, & 4)												Nail Spacing (in.) at other panel edges (Cases 1, 2, 3, & 4)							
6			6			4			3			6	6	4	3									
v _c (plf)		G _a (kips/in.)		v _c (plf)		G _a (kips/in.)		v _c (plf)		G _a (kips/in.)		v _c (plf)		G _a (kips/in.)		v _w (plf)		v _w (plf)						
		OSB	PLY			OSB	PLY			OSB	PLY			OSB	PLY									
Structural I	6d	1-1/4	5/16	2	6			6			4			3			6	6	4	3				
					370		15	12	500		8.5	7.5	750		12	10	840		20	15	520	700	1050	1175
	8d	1-3/8	3/8	2	4			4			2-1/2			2			6	6	4	3				
					420		12	9.5	580		7.0	6.0	840		9.5	8.5	950		17	13	590	785	1175	1330
	10d	1-1/2	15/32	3	2-1/2			2-1/2			15			15			6	6	4	3				
					600		12	10	800		7.5	6.5	1200		10	9.0	1350		18	13	840	1120	1680	1890
Sheathing and Single-Floor	6d	1-1/4	5/16	2	2-1/2			2-1/2			15			15			6	6	4	3				
					340		15	10	450		9.0	7.0	670		13	9.5	780		21	13	475	630	940	1065
					8d	1-3/8	3/8	2	2			2			15			15			6	6	4	3
									380		12	9.0	500		7.0	6.0	760		10	8.0	860		17	12
					10d	1-1/2	15/32	3	2			2			15			15			6	6	4	3
									370		13	9.5	500		7.0	6.0	750		10	8.0	840		18	12
	8d	1-3/8	7/16	3	2			2			15			15			6	6	4	3				
					420		10	8.0	580		5.5	5.0	840		8.5	7.0	950		14	10	590	785	1175	1330
					10d	1-1/2	19/32	2	2			2			15			15			6	6	4	3
									480		15	11	640		9.5	7.5	960		13	9.5	1090		21	13
					10d	1-1/2	15/32	3	2			2			15			15			6	6	4	3
									540		12	9.5	720		7.5	6.0	1080		11	8.5	1220		18	12
					10d	1-1/2	15/32	3	2			2			15			15			6	6	4	3
									510		14	10	680		8.5	7.0	1010		12	9.5	1150		20	13
					10d	1-1/2	15/32	3	2			2			15			15			6	6	4	3
									570		11	9.0	760		7.0	6.0	1140		10	8.0	1290		17	12
					10d	1-1/2	19/32	2	2			2			15			15			6	6	4	3
									540		13	9.5	720		7.5	6.5	1060		11	8.5	1200		19	13
10d	1-1/2	19/32	3	2			2			15			15			6	6	4	3					
				580		25	15	770		15	11	1150		21	14	1310		33	18	810	1080	1610	1835	
10d	1-1/2	19/32	3	2			2			15			15			6	6	4	3					
				650		21	14	860		12	9.5	1300		17	12	1470		28	16	910	1205	1820	2060	
10d	1-1/2	19/32	3	2			2			15			15			6	6	4	3					
				640		21	14	850		13	9.5	1280		18	12	1460		28	17	895	1190	1790	2045	
10d	1-1/2	19/32	3	2			2			15			15			6	6	4	3					
				720		17	12	980		10	8.0	1440		14	11	1640		24	15	1010	1345	2015	2295	

TABLE 4.2A SHEATHING SHEAR CAPACITIES

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Top Plate Chord Design

Max Chord Tension/Compression =	1188	lbs
Ft =	350	psi
Fc =	1000	psi
Cd =	1.6	
As pro (2) 2 x 6 =	16.5	in ²
F't =	560	psi
F't allowable tension =	9240	lbs

Controls because fully braced
By inspection Ok for wall shear force

OK >

1188 lbs

MST72	18	(46) 0.162 x 2½	6,235	5,405
	30	(48) 0.162 x 2½	6,505	5,640
	24	(54) 0.162 x 2½	6,730	6,345
	18	(62) 0.162 x 2½	6,730	6,475

See footnotes below.

4519

MST72 ALLOWABLE TENSION

Top Plate Splice Design

Assuming splice is at a position that has to transfer full tension/compression or full shear		
Max Chord Tension/Compression =	1188	lbs
Wall Shear =	4519	lbs
Try MST72 Strap		
Allowable Tension	6730	lbs

Controls

OK >

Wall Out of Plane Stud Design

ASD Wall Design Pressure =	102.0	psf
2" x 6" Stud Spacing =	1.0	ft
ASD Load/stud =	102.00	lb/ft
Controlling Stud Ht. =	8	ft
ASD Wind Moment =	816.00	ft*lb
2 x 6 Section Modulus =	7.56	in ³
Applied Stress =	1295.24	psi
Cd =	1.6	
Fb southern yellow pine =	1100	psi
F'b =	1760	psi
I stud =	20.8	in ⁴
E stud =	1100000	psi
Deflection =	0.410853147	in
Allowable deflection L/180 =	0.533333333	in

OK > 1295.238

OK

Wall Out of Plane Fastener Withdrawal (side walls negative pressure)

Try 3" spacing s =	3	
Ae =	0.5	sf
C&C Wind Pressure =	-169.2	psf
Applied Withdrawal =	-84.6	lbs
Max ASD Fastener Shear =	137	lbs
Max ASD Fastener Shear Per Fastener =	34.37181273	lbs
Max combined ASD Fastener load =	161.4434694	lbs
Use 2" #12 screw at 3" on center interior and edges capacity =	538.9292165	lbs

OK

Wall In Plane Design Using Segmented Shear Wall Method

Max Wall Shear 20' wall =	4519	lb/ft
Max Wall Shear 24' wall =	3300	lbs

SHEAR WALL 20' WITH DOOR AND 6' WINDOW

See "20' Shear Wall Design" Tab

SHEAR WALL 20' WITH 6' AND 3' WINDOW

See "20' Shear Wall Design" Tab

SHEAR WALL 24' WITH 12' OPENING AND 3' WINDOW

See "24' Shear Wall Design" Tab

**NOTE SEE ROOF DESIGN FOR WALL SHEATHING OUT OF PLANE CAPACITY
B/C ROOF SPAN AND PRESSURES ARE GREATER WALL SHEATHING OUT OF PLANE DOESN'T CONTROL**

Stud Connection to Top Plate/Sill Plate

Uplift =	-56.82061907	psf
Stud Spacing =	1	ft
Uplift per stud =	-375.0160858	
Roof Weight x 0.6 =	153.84	lb/ft
Wall Weight x 0.6 =	49.5	lb/ft
Total Uplift =	-171.6760858	lb

USE TSP ANCHOR BOTTOM OF STUDS TSP ANCHOR TOP OF STUDS ALLOWABLE UPLIFT = 755 LBS

Sill Plate Attachment to Foundation

See Shear Wall Design Tabs

Stud Connection to Top Plate/Sill Plate at Opening and Header Straps

Largest Opening =	6	ft
Uplift at window jack/king studs =	-1125.048258	lb
Six foot opening uplift =	-562.5241288	lb
Dead load =	540	
Required uplift capacity at six foot opening =	-22.52412876	lbs
Required uplift capacity at twelve foot opening =	-45.04825752	lbs
USE MSTA 30 strap around 6 foot openings CAPACITY =	2050	lbs
Use CS16 strap	1325	lbs

OK

OK

Holddown Requirements

See Shear Wall Design Tabs

Model No.	Dimensions (in.)		Stud	Plate Width	Fasteners (in.)		Allowable Uplift Loads				Code Ref.
	W	L			Stud	Plate	DF/SP		SPF/HF		
							Side 8 (160)	Center 9 (160)	Side 8 (160)	Center 9 (160)	
SP1	3 1/2	5 1/2	2x	—	(6) 0.148 x 3	(4) 0.148 x 3	555	555	535	535	IBC, FL, LA
SP2	3 1/2	6 1/2	2x	—	(6) 0.148 x 3	(6) 0.148 x 3	1,010	1,010	605	605	
SP4	3 3/4	7 1/4	2x	4x	(6) 0.148 x 1 1/2	—	415	825	355	710	
SP6	5 1/2	7 3/4	2x	6x	(6) 0.148 x 1 1/2	—	415	825	355	710	
SP8	7 1/2	8 1/2	2x	8x	(6) 0.148 x 1 1/2	—	415	825	355	710	
SPH4	3 3/4	8 3/4	2x	4x	(10) 0.148 x 1 1/2	—	520	1,040	450	895	
					(12) 0.148 x 1 1/2	—	640	1,280	550	1,100	
SPH6	5 1/2	9 1/4	2x	6x	(10) 0.148 x 1 1/2	—	520	1,040	450	895	
					(12) 0.148 x 1 1/2	—	640	1,280	550	1,100	
SPH8	7 1/2	8 3/4	2x	8x	(10) 0.148 x 1 1/2	—	520	1,040	450	895	
					(12) 0.148 x 1 1/2	—	640	1,280	550	1,100	
RSP4 (1)	2 1/2	4 1/2	2x	—	(4) 0.131 x 1 1/2	(4) 0.131 x 1 1/2	245	245	285	285	
RSP4 (2)	2 1/2	4 1/2	2x	—	(4) 0.131 x 1 1/2	(4) 0.131 x 1 1/2	390	390	370	370	
CS20	1 1/4	24	2x	—	(6) 0.148 x 1 1/2	—	—	550	—	475	
					(10) 0.148 x 1 1/2	—	—	915	—	790	
CS16	1 1/4	26	2x	—	(12) 0.148 x 1 1/2	—	—	1,135	—	980	
					(14) 0.148 x 1 1/2	—	—	1,325	—	1,140	

1. See pp. 260-261 for Straps and Ties General Notes.

CS16 STUD PLATE TIES

Headers

Per WFCM three 2" x 8" headers can span	6.82	ft
Dist from top plate to header max =	4.095	ft
Dist from sill plate to bottom of window =	3	ft
x =	4.095	
wall height h =	11.42	ft
x/h =	0.358581436	
Number of full head studs required for 6 foot	3	
Number of full head studs required for 3 foot	2	

Blocking to Stud

Withdrawl C & C pressure =	-169.2	psf
Trib =	4	sf
Withdrawl Pressure =	-676.9933361	
Try 3 connectors each end		
Connector Applied Shear =	-112.8322227	
10d box Z =	93	lbs
Cd =	1.6	
Ctn =	0.83	
Z' =	123.504	lbs

OK

Sill Plate Out of Plane Bending/Shear Design

Sill plate trib =	21	psf
C & C Pressure	75.2	psf
Trib =	3.5	sf
Wapp =	263.13	lb/ft
Mapp (6' window) =	1184.085	lb*ft
S (2) 2 x 6=	15.125	in^3
App Stress =	939.4393388	psi
Cd =	1.6	
Fb =	775	psi
F'b =	1240	psi
Vapp =	789.39	lbs
fv =	47.84181818	psi
F'v =	216	psi
Q =	12.375	in^3
I =	415.9375	in^4
Shear Flow =	281.8318017	lb/ft
Z 10d box =	93	lbs
Z' 10d box =	148.8	lbs
Req Spacing =	6.335693806	in

Say 6"

OK

Ok

Sill Plate Out of Plane Bending/Shear Design

Sill plate trib =	10.5	psf
C & C Pressure	101.5	psf
Trib =	3.5	sf
Wapp =	355.32	lb/ft
Mapp (6' window) =	399.735	lb*ft
S 2 x 6=	7.5625	in^3
App Stress =	634.2902	psi
Cd =	1.6	
Fb =	775	psi
F'b =	1240	psi
Vapp =	532.98	lbs
fv =	32.30182	psi
F'v =	216	psi

OK

Stud Plate Ties (cont.)

These products are available with additional corrosion protection. For more information, see p. 15.

Model No.	Dimensions (in.)		Fasteners (in.)			Allowable Uplift Loads (160)			Code Ref.	
	W	L	Studs	Double Top Plate	Single Sill Plate	DF/SP/SPF		SPF/HF		
						DF/SP	SPF			
SSP	1 1/2	6 1/2	(4) 0.148 x 1 1/2	(3) 0.148 x 1 1/2	—	—	330	—	—	IBC, FL, LA
			(4) 0.148 x 3	(3) 0.148 x 3	(1) 0.148 x 1 1/2	—	395	310	—	
			(4) 0.148 x 3	(3) 0.148 x 3	(1) 0.148 x 3	—	410	—	—	
DSP	2 1/2	6 1/2	(6) 0.148 x 1 1/2	(6) 0.148 x 1 1/2	—	—	730	—	—	
			(6) 0.148 x 3	(2) 0.148 x 1 1/2	—	—	620	515	—	
			(6) 0.148 x 3	(2) 0.148 x 3	—	—	780	—	—	
TSP	1 1/2	7 1/2	(6) 0.148 x 1 1/2	(3) 0.148 x 1 1/2	—	—	755 ⁴	—	400	FL
			(6) 0.148 x 3	(6) 0.148 x 3	—	—	1,015 ⁴	—	—	

1. See pp. 260-261 for Straps and Ties General Notes.
 2. When cross-grain bending or cross-grain torsion cannot be avoided in the members, mechanical reinforcement to resist such forces shall be considered by the Designer.
 3. Allowable loads for DSP installed to a rim board are 620 lb. (DF/SP) and 515 lb. (SPF/HF).
 4. Noted values apply only to DF/SP members. For SPF values, multiply by 0.88.

TSP STUD PLATE TIES

SS	MSTA24	1 1/4	24	(18) 0.148 x 2 1/2	1,640	1,460	
	MSTA30	1 1/4	30	(22) 0.148 x 2 1/2	2,050	1,825	
	MSTA36	1 1/4	36	(26) 0.148 x 2 1/2	2,050	2,050	
SS	MSTA49	1 1/4	49	(26) 0.148 x 2 1/2	2,020	2,020	FL, LA
	ST9	1 1/4	9	(8) 0.162 x 2 1/2	885	765	
	ST12	1 1/4	11 3/4	(10) 0.162 x 2 1/2	1,105	955	
	ST18	1 1/4	17 3/4	(14) 0.162 x 2 1/2	1,420	1,335	IBC, FL, LA
	ST22	1 1/4	21 3/4	(18) 0.162 x 2 1/2	1,420	1,420	

MSTA 30 STRAP CAPACITY

Table 3.22A1 Laterally Unsupported (Dropped) Header Spans for Exterior Loadbearing Walls

(Supporting a Roof and Ceiling)

Dead Load Assumptions: Roof/Ceiling Assembly = 20 psf, $L/\Delta_{LL}=240$

Dropped Exterior

		Roof Live Load			Ground Snow Load								
		20 psf			30 psf			50 psf			70 psf		
		Building Width (ft)											
		12	24	36	12	24	36	12	24	36	12	24	36
Headers Supporting	Size	Maximum Header/Girder Spans (ft-in.) for Common Lumber Species ^{1,3,4}											
 <p>Roof and Ceiling</p>	1-2x6	4-4	3-4	2-9	3-11	3-0	2-7	3-4	2-7	2-2	3-0	2-4	2-0
	1-2x8	5-3	4-1	3-6	4-10	3-9	3-3	4-2	3-3	2-9	3-9	2-11	2-6
	1-2x10	6-0	4-9	4-0	5-7	4-5	3-9	4-10	3-10	3-3	4-4	3-5	2-11
	1-2x12	6-6	5-3	4-7	6-2	5-0	4-4	5-5	4-5	3-9	4-11	4-0	3-4
	2-2x4	4-4	3-3	2-9	3-11	3-0	2-7	3-4	2-7	2-2	3-0	2-4	1-11
	2-2x6	6-2	4-10	4-1	5-8	4-5	3-9	4-11	3-10	3-3	4-5	3-5	2-11
	2-2x8	7-2	5-9	4-11	6-9	5-5	4-8	5-11	4-8	4-0	5-4	4-3	3-7
	2-2x10	7-10	6-4	5-6	7-6	6-1	5-3	6-7	5-4	4-8	6-0	4-10	4-2
	2-2x12	8-5	6-10	6-0	8-1	6-7	5-10	7-2	5-11	5-2	6-6	5-5	4-9
	3-2x8	8-5	6-10	5-11	8-0	6-6	5-7	7-1	5-8	4-11	6-5	5-2	4-5
	3-2x10	9-2	7-5	6-6	8-9	7-2	6-3	7-9	6-4	5-6	7-1	5-9	5-0
	3-2x12	9-9	8-0	7-0	9-4	7-8	6-9	8-4	6-10	6-1	7-8	6-3	5-7
	4-2x8	9-4	7-7	6-8	8-11	7-3	6-4	7-11	6-5	5-7	7-2	5-10	5-0
	4-2x10	10-2	8-3	7-3	9-8	8-0	7-0	8-8	7-1	6-3	7-11	6-6	5-8
4-2x12	10-10	8-10	7-9	10-4	8-7	7-6	9-3	7-8	6-9	8-6	7-0	6-2	

MAXIMUM HEADER SPANS



DESIGN WITH ONE OPENING EXCLUDE PANEL ADJACENT TO DOOR

Shear Wall Design 20' Wall with door

Shear Wall Shear =	3300 lb	
Using preforated method		
L1 =	2.58	
L2 =	3.50	
L3 =	2.75	
worst case h/L ratio =	3.10 < 3.5	OK
Ltot =	21.00	
% Full Ht. =	0.29	
Co =	0.41	
V/Co =	8048.034	
panel shear =	911.0982	
nominal panel shear =	1822.196	
10d nails at 3" with 3" blocking 15/32" struct 1 OSB =	1860 plf	OK*
T/Co =	3065.918	
T/Co LRFD =	5109.863	
USE HDU5 holddown capacity =	5646 lb	
5/8" DIA. CAP. LRFD 4.5" embed =	5110 lb	OK
NEED 2 STUDS AT EACH HOLDDOWN (NEED DETAIL)		
Required Shear Wall Sill Plate Anchorage Force =	911.0982 lb/ft	
MASA Anchor at 1'-0" on center =	1475 lb	OK

Table 4.3.3.5 Shear Capacity Adjustment Factor, C.

Wall Height, h	Maximum Opening Height ¹				
	h/3	h/2	2h/3	5h/6	h
8' Wall	2'-8"	4'-0"	5'-4"	6'-8"	8'-0"
10' Wall	3'-4"	5'-0"	6'-8"	8'-4"	10'-0"
Percent Full-Height Sheathing ²		Effective Shear Capacity Ratio			
10%	1.00	0.69	0.53	0.43	0.36
20%	1.00	0.71	0.56	0.45	0.38
30%	1.00	0.74	0.59	0.49	0.42
40%	1.00	0.77	0.63	0.53	0.45
50%	1.00	0.80	0.67	0.57	0.50
60%	1.00	0.83	0.71	0.63	0.56
70%	1.00	0.87	0.77	0.69	0.63
80%	1.00	0.91	0.83	0.77	0.71
90%	1.00	0.95	0.91	0.87	0.83
100%	1.00	1.00	1.00	1.00	1.00

SHEAR CAPACITY ADJUSTMENT FACTOR

* Provided sheathing thickness is greater than maximum thickness provided by NDS table therefore actual capacity will be greater than what is shown



20' ShearWallWithTwoWindows

Shear Wall Design 20' Wall with door

Shear Wall Shear =	3300 lb	
Using preforated method		
L1 =	2.75	
L2 =	5.82	
L3 =	3.33	
worst case h/L ratio =	2.91	<3.5 OK
Ltot =	21.00	
% Full Ht. =	0.41	
Co =	0.77	
V/Co =	4285.317	
panel shear =	360.1107	
nominal panel shear =	720.2213	
10d nails at 3" with 3" blocking 15/32" struct 1 OSB =	1860 plf	OK*
Applied Tension T/Co =	1632.502 lb	
Applied Tension T/Co LRFD =	2720.836 lb	
USE HDU5 holddown capacity =	5646 lb	OK
5/8" DIA. CAP. LRFD 4.5" embed=	5110 lb	OK
NEED 2 STUDS AT EACH HOLDDOWN		
Required Shear Wall Sill Plate Anchorage Force =	360.1107 lb/ft	
MASA Anchor at 1'-0" on center =	1475 lb	OK

* Provided sheathing thickness is greater than maximum thickness provided by NDS table therefore actual capacity will be greater than what is shown

Table 4.3.3.5 Shear Capacity Adjustment Factor, C_s

Wall Height, h	Maximum Opening Height ¹				
	h/3	h/2	2h/3	5h/6	h
8' Wall	2'-8"	4'-0"	5'-4"	6'-8"	8'-0"
10' Wall	3'-4"	5'-0"	6'-8"	8'-4"	10'-0"
Percent Full-Height Sheathing ²	Effective Shear Capacity Ratio				
10%	1.00	0.69	0.53	0.43	0.36
20%	1.00	0.71	0.56	0.45	0.38
30%	1.00	0.74	0.59	0.49	0.42
40%	1.00	0.77	0.63	0.53	0.45
50%	1.00	0.80	0.67	0.57	0.50
60%	1.00	0.83	0.71	0.63	0.56
70%	1.00	0.87	0.77	0.69	0.53
80%	1.00	0.91	0.83	0.77	0.71
90%	1.00	0.95	0.91	0.87	0.83
100%	1.00	1.00	1.00	1.00	1.00

SHEAR CAPACITY ADJUSTMENT FACTOR

Table 4.3A Nominal Unit Shear Capacities for Wood-Frame Shear Walls^{1,3,6,7}

Wood-based Panels⁴

Sheathing Material	Minimum Nominal Panel Thickness (in.)	Minimum Fastener Penetration in Framing Member or Blocking (in.)	Fastener Type & Size	A SEISMIC								B WIND							
				Panel Edge Fastener Spacing (in.)								Panel Edge Fastener Spacing (in.)							
				6		4		3		2		6	4	3	2				
				V _s (plf)	G _a (kips/in.)	V _s (plf)	G _a (kips/in.)	V _s (plf)	G _a (kips/in.)	V _s (plf)	G _a (kips/in.)	V _w (plf)	V _w (plf)	V _w (plf)	V _w (plf)				
Wood Structural Panels - Structural I ^{4,5}	5/16	1-1/4	Nail (common or galvanized box) 6d	OSB		PLY		OSB		PLY		OSB		PLY		560	840	1090	1430
	3/8 ²	1-3/8		400	13	10	600	18	13	780	23	16	1020	35	22	645	1010	1290	1710
	7/16 ²	1-3/8	8d	460	19	14	720	24	17	920	30	20	1220	43	24	645	1010	1290	1710
	15/32	1-1/2		510	16	13	790	21	16	1010	27	19	1340	40	24	715	1105	1415	1875
	5/16	1-1/2	10d	560	14	11	860	18	14	1100	24	17	1460	37	23	785	1205	1540	2045
5/16	1-1/2	10d	680	22	16	1020	29	20	1330	36	22	1740	51	28	950	1430	1860	2435	

NOMINAL SHEAR WALL CAPACITIES

Model No.	Ga.	Dimensions (in.)					Fasteners (in.)		Minimum Wood Member Size (in.)	Allowable Tension Loads (160)		
		W	H	B	CL	SO	Anchor Bolt Dia. (in.)	Wood Fasteners		DF/SP	SPF/HF	Deflection at Allowable Load (in.)
DTT1Z	14	1 1/2	7 1/8	1 7/16	3/4	3/16	3/8	(6) SD #9 x 1 1/2	1 1/2 x 5 1/2	840	840	0.17
								(6) 0.148 x 1 1/2		910	640	0.167
								(8) 0.148 x 1 1/2		910	850	0.167
DTT2Z	14	3 1/4	6 15/16	1 5/8	1 1/16	3/16	1/2	(8) 1/4 x 1 1/2 SDS	1 1/2 x 3 1/2	1,825	1,800	0.105
								(8) 1/4 x 1 1/2 SDS		2,145	1,835	0.128
DTT2Z-SDS2.5	14	3 1/4	6 15/16	1 5/8	1 1/16	3/16	1/2	(8) 1/4 x 2 1/2 SDS	3 x 3 1/2	2,145	2,105	0.128
HDU2-SDS2.5	14	3	8 15/16	3 1/4	1 5/16	1 3/16	5/8	(6) 1/4 x 2 1/2 SDS	3 x 3 1/2	3,075	2,215	0.088
HDU4-SDS2.5	14	3	10 15/16	3 1/4	1 5/16	1 3/16	5/8	(10) 1/4 x 2 1/2 SDS	3 x 3 1/2	4,565	3,285	0.114
HDU5-SDS2.5	14	3	13 3/16	3 1/4	1 5/16	1 3/16	5/8	(14) 1/4 x 2 1/2 SDS	3 x 3 1/2	5,645	4,340	0.115

HDU5 HOLDDOWN ALLOWABLE CAPACITIES

Simpson Strong-Tie® Wood Construction Connectors

MASA/MASAP

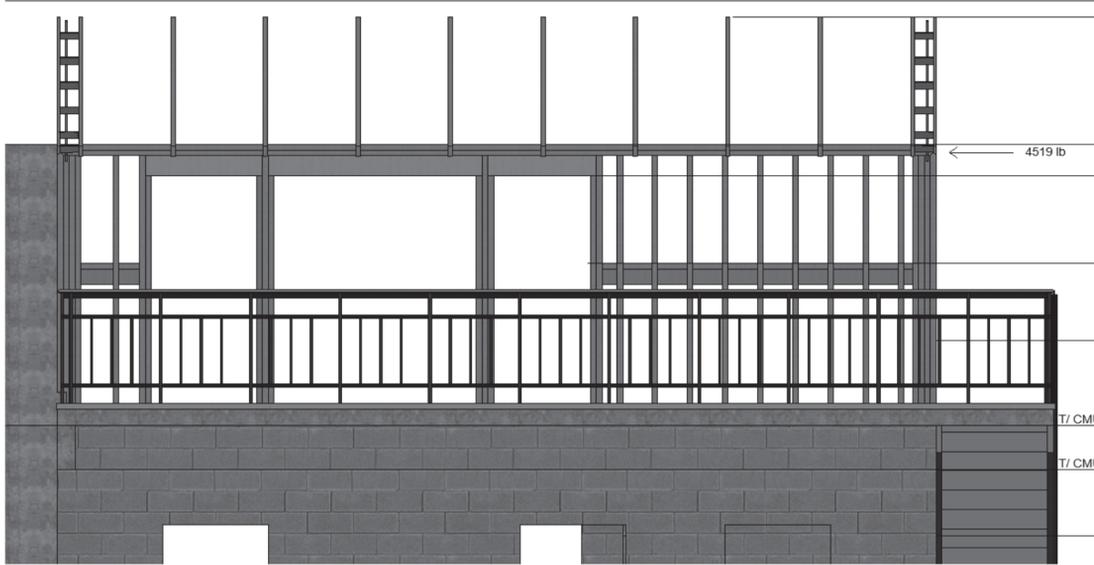


Mudsill Anchors (cont.)

These products are available with additional corrosion protection. For more information, see p. 15.

Model No.	Sill Size	Fasteners (in.)		Allowable Loads												Code Ref.
		Sides	Top	Uncracked						Cracked						
				Wind and SDC A&B ^{5,6}			SDC C-F ⁶			Wind and SDC A&B ^{5,6}			SDC C-F ⁶			
Uplift	F ₁	F ₂	Uplift	F ₁	F ₂	Uplift	F ₁	F ₂	Uplift	F ₁	F ₂	Uplift	F ₁	F ₂		
Standard Installation – Attached to DF/SP Sill Plate																
MASA or MASAP	2x4, x6, x8, x10	(3) 0.148 x 1 1/2	(6) 0.148 x 1 1/2	920	1,475	1,095	745	1,235	1,045	750	1,475	875	660	1,235	765	
	3x4, 3x6	(5) 0.148 x 1 1/2	(4) 0.148 x 1 1/2	630	1,165	725	550	1,020	725	475	1,165	725	415	1,020	640	
One-Leg-Up Installation – Attached to DF/SP Sill Plate																

MASA MUDSILL ANCHOR CAPACITIES



DESIGN WITH ONE OPENING EXCLUDE PANEL ADJACENT TO DOOR
THIS DESIGN WILL WORK FOR MODULE WALL WITH 12' OPNG WITH SHORTER PANELS AND LESS LOAD

Shear Wall Design 24' Wall with large opening and window

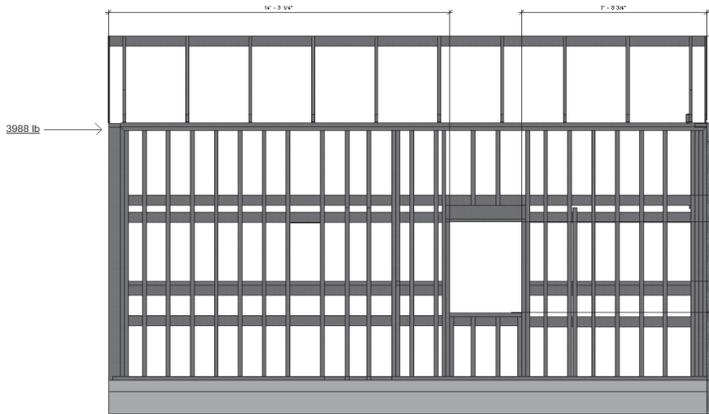
Shear Wall total shear =	4519 lb	
Using preforated method		
L1 =	3.82	
L2 =	3.00	
L3 =	2.75	
worst case h/L ratio =	2.91 < 3.5	OK
Ltot =	24.00	
% Full Ht. =	0.28	
Co =	0.73	
V/Co =	6190.225	
panel shear =	646.8365	
nominal panel shear =	1293.673	
10d nails at 3" with 3" blocking 15/32" struct 1 OSB =	1860 plf	OK*
T/Co =	2063.408	
T/Co LRFD =	3439.014	
USE HDU5 holddown capacity =	5646 lb	
5/8" DIA. CAP. LRFD 4.5" embed =	5110 lb	
NEED 2 STUDS AT EACH HOLDDOWN		
Required Shear Wall Sill Plate Anchorage Force =	646.8365 lb/ft	
MASA Anchor at 1'-0" on center =	1475 lb	OK

Table 4.3.3.5 Shear Capacity Adjustment Factor, C_s

Wall Height, h	Maximum Opening Height ¹				
	h/3	h/2	2h/3	5h/6	h
8' Wall	2'-8"	4'-0"	5'-4"	6'-8"	8'-0"
10' Wall	3'-4"	5'-0"	6'-8"	8'-4"	10'-0"
Percent Full-Height Sheathing ²	Effective Shear Capacity Ratio				
	10%	1.00	0.69	0.53	0.43
20%	1.00	0.71	0.56	0.45	0.38
30%	1.00	0.74	0.59	0.49	0.42
40%	1.00	0.77	0.63	0.53	0.45
50%	1.00	0.80	0.67	0.57	0.50
60%	1.00	0.83	0.71	0.63	0.56
70%	1.00	0.87	0.77	0.69	0.63
80%	1.00	0.91	0.83	0.77	0.71
90%	1.00	0.95	0.91	0.87	0.83
100%	1.00	1.00	1.00	1.00	1.00

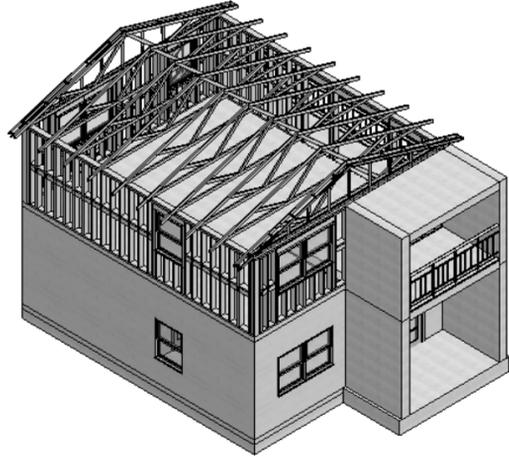
* Provided sheathing thickness is greater than maximum thickness provided by NDS table therefore actual capacity will be greater than what is shown

need blocking behind collector

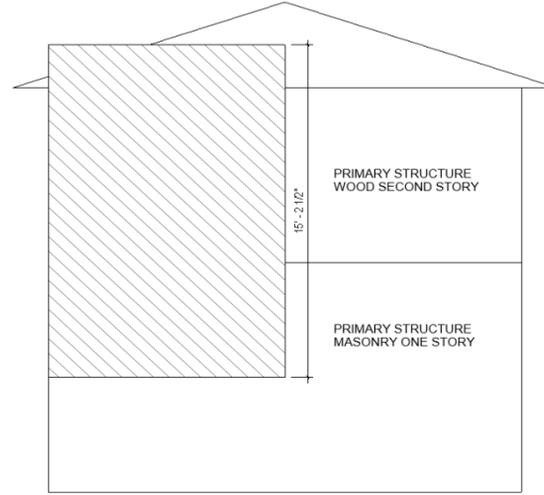


BY INSPECTION ABOVE DESIGN WILL WORK FOR THIS WALL

ASD WIND PRESSURES								
	Windward Wall Pressures at "z" (psf)						Combined WW + LW	
	z	Kz	Kzt	Windward Wall			Normal	Parallel
				to Ridge	to Ridge	to Ridge	to Ridge	
	0 to 15'	1.0	1.0	qzGCp	w/+qiGCpi	w/-qhGCpi	54.8	53.1
h=	20	1.0	1.0	55.0	23.8	42.3	56.5	54.8
ridge =	22.4	1.1	1.0	57.9	25.5	43.9	57.2	55.5



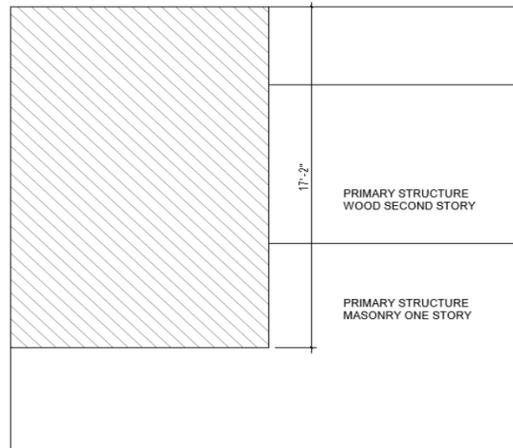
Note: Modules not included because they are acting independent of the primary structure and are not hard attached.



Roof Diaphragm Load Primary Structure Wind Parallel to Ridge:

B =	24	ft	o/o
Wall Ht. CMU =	18.50	ft	
Roof Ht. Above 1st story=	11.90	ft	
Roof Ht. Avg =	15.20	ft	
Diaphragm Trib Area/ft =	15.20	Ft ² /ft	
Diaphragm Load/ft Main =	843	lb/ft	
Diaphragm Shear/Ft =	351	lb/ft	Note: Diaphragm transfers load to two adjacent shear walls
Wall Shear 24' Wall Primary	8429	lb	
Diaphragm Moment =	60692	lb*ft	
Diaphragm Chord T/C =	3035	lbs	
Diaphragm Chord T/C per ft =	126	lbs/ft	Doesn't control

TRIBUTARY FOR SHEAR WALL WIND PARALLEL TO RIDGE



Roof Diaphragm Load Primary Structure Wind Perpendicular to Ridge:

B =	20	ft	o/o
Wall Ht. CMU =	10.50	ft	
Roof Ht. Above 1nd Story =	11.90	ft	
Roof Ht. Avg =	11.90	ft	
Diaphragm Trib Area/ft =	17.15	Ft ² /ft	
Diaphragm Load/ft =	981	lb/ft	
Diaphragm Total Shear/ft =	490	lb/ft	
Wall Shear 20' Wall =	9810	lbs	ASD
Diaphragm Moment =	49050	lb*ft	
Diaphragm Chord T/C =	2044	lbs	
Diaphragm Chord T/C per ft =	102	lbs/ft	Doesn't control

TRIBUTARY FOR SHEAR WALL WIND PERPENDICULAR TO RIDGE

Roof Diaphragm Load Primary Module for 10' Shear Wall:

B =	20	ft	o/o
Wall Ht. CMU =	10.50	ft	
Roof Ht. Above 1nd Story =	10.50	ft	
Roof Ht. Avg =	10.50	ft	
Diaphragm Trib Area/ft =	5.25	Ft ² /ft	
Diaphragm Load/ft =	300	lb/ft	
Diaphragm Total Shear/ft =	300	lb/ft	
Wall Shear 10' Wall =	3003	lbs	ASD
Diaphragm Moment =	15015	lb*ft	
Diaphragm Chord T/C =	1502	lbs	
Diaphragm Chord T/C per ft =	150	lbs/ft	Doesn't control

Roof Diaphragm Load Primary Module for 20' Shear Wall:

B =	10	ft	o/o
Wall Ht. CMU =	10.50	ft	
Roof Ht. Above 1nd Story =	10.50	ft	
Roof Ht. Avg =	10.50	ft	
Diaphragm Trib Area/ft =	5.25	Ft ² /ft	
Diaphragm Load/ft =	300	lb/ft	
Diaphragm Total Shear/ft =	75	lb/ft	
Wall Shear 20' Wall =	1502	lbs	ASD
Diaphragm Moment =	3754	lb*ft	
Diaphragm Chord T/C =	375	lbs	
Diaphragm Chord T/C per ft =	38	lbs/ft	Doesn't control

Wall Design C and C Zone 4

Assume No. 5 at 24" O.C.		
Effective Wind Area =	36.75	
Wind Load =	60.6 lb/ft	ASD
Vert Load =	1150 lb	D+L
Self Wt Mid wall =	195 lb	Self
As pro =	0.15 sq in	
d =	2.8125 in	
Rho =	0.004444	
n =	21.5	
Rho x n =	0.095556	
k =	0.351928	
j =	0.882691 in	
M =	909 lb*ft	
fs =	29292.26 psi	< 32,000 psi OK
fb =	739.8538 psi	< 1900*0.45 = 855 psi OK
Equivalent Wall Thickness =		4 in
fa =	28.02083	28.02083 psi
fa+fb =	767.8747 psi	< 855 psi OK

Development Length

Wall is considered pinned/pinned
but is also a special shear wall

As min special shear wall = $0.2 \text{ in}^2 / 24" = 0.1 \text{ in}^2$ per foot
As provided = 0.225 in^2 per foot OK

W1.7 bed joint reinforcement not spaced at more than 16" on center (horiz)

ACI 530 7.4.3.1

ASCE 7

Anchor bolts embedded in grout have to resist 2 x seismic load (might not control)

Wall Design C and C Zone 5

Assume No. 5 at 16" O.C. at 3' out from edge		
Wind Load =	75.6 lb/ft	
Vert Load =	1150 lb	
Self Wt Mid wall =	195 lb	
As pro =	0.225 sq in	
d =	2.8125 in	
Rho =	0.006667	
n =	21.5	
Rho x n =	0.143333	
k =	0.410933	
j =	0.863022 in	
M =	1134 lb*ft	
fs =	24917.08 psi	
fb =	808.472 psi	
Equivalent Wall Thickness =		
fa =	28.02083	
fa+fb =	836.4928 psi	
NOTE: Many walls will have equivalent of Required steel due to shear wall panel req.		

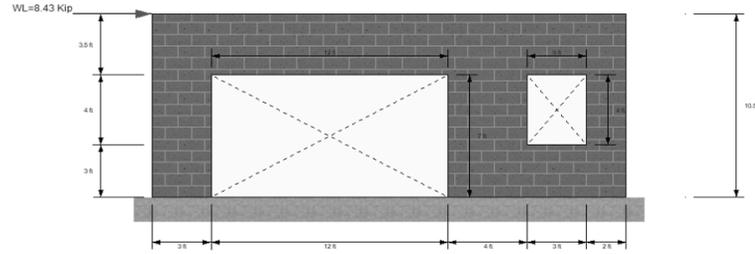
WALL LOADS

D =	750	lb/ft
L =	400	lb/ft
Self =	64	psf
Wind =	45	psf
	-31.02886	psf
Wind in plane =	8429	lbs
Wind out of plane =	45	psf

Fully Grouted
At 32" O.C.
windward
leeward

Relative Rigidities of Piers

Pier No.	Height	Length	h/l	Relative Rigidity Table ASD-89	Percentage of Lateral Force	V
1	10.5	3	3.5	0.187	0.295886076	2494.163
2	10.5	4	2.625	0.383	0.606012658	5108.366
3	10.5	2	5.25	0.062	0.098101266	826.9417
				0.632		



Wall Segment 1

l =	3	ft
P =	2.586	kips
Wind Segment =	2.494163	kips
M =	314.2645	kip*in
l =	36	in
t =	5.625	in
fa =	0.01277	ksi
r =	1.62	in
h/r =	77.77778	
Fa =	0.259259	psi
Try no 7 at end of wall		
d =	28	in
b =	5.625	in
As =	0.6	in^2
p =	0.00381	
n =	21.5	
pn =	0.081905	
k =	0.331033	
j =	0.889656	
fb =	483.9417	psi
Fb =	855	psi
fs =	21026.36	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	16.41905	psi
Fv =	21.79	psi
Fv =	77.46	psi

Fully Grouted

2 no 5

> 483.9417 psi OK
> 21026.36 psi OK
> 16.41905 psi OK
Doesn't Control

TABLE 11.2 Relative Rigidities of Piers – West Wall

Pier No.	Height h (ft)	Length l (ft)	h/l Ratio (all piers fixed)	Relative Rigidity Table ASD-89 Fixed Piers ²	Percentage Lateral Force to Each Pier	Force V to each Pier (pounds)	Unit Shear f_v in each pier = $\frac{V}{tl}$ (psi)
1	10	3	3.33	0.213	1.5	353	1.1
2	5	2	2.50	0.75	5.0	1,172	5.5
3	5	18	0.28	11.602	81.2	19,050	9.9
4	4	3	1.33	1.577	11.0	2,580	8.0
5	7	2	3.50	0.187	1.3	306	1.4
				$\Sigma = 14.329$	100%	$\Sigma = 23,460$ pounds ¹	

1. It would be conservative and quite usual to use the base shear, $V = 26,700$ lbs as the force on the wall and distribute this amount to all piers. The approach here is a little more detailed.

Wall Segment 2

l =	4	ft
P =	3.336	kips
Wind Segment =	5.108366	kips
M =	643.6541	kip*in
l =	48	in
t =	5.625	in
fa =	0.012356	ksi
r =	1.62	in
h/r =	77.77778	
Fa =	0.259259	psi
Try no 7 at end of wall		
d =	40	in
b =	5.625	in
As =	0.6	in^2
p =	0.002667	
n =	21.5	
pn =	0.057333	
k =	0.286111	
j =	0.90463	
fb =	552.6308	psi
Fb =	855	psi
fs =	29646.29	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	14.82667	psi
Fv =	21.79	psi
Fv =	77.46	psi

Fully Grouted

2 no 5

> 552.6308 psi OK
> 29646.29 psi OK
> 14.82667 psi OK
Doesn't Control

Wall Segment 3

l =	2	ft	
P =	1.836	kips	
Wind Segment =	0.826942	kips	
M =	104.1947	kip*in	
l =	24	in	
t =	5.625	in	
fa =	0.0136	ksi	
r =	1.62	in	Fully Grouted
h/r =	77.77778		
Fa =	0.259259	psi	
Try no 7 at end of wall			
d =	16	in	
b =	5.625	in	
As =	0.6	in ²	2 no 5
p =	0.006667		
n =	21.5		
pn =	0.143333		
k =	0.410933		
j =	0.863022		
fb =	408.0562	psi	
Fb =	855	psi	> 408.0562 psi OK
fs =	12576.28	psi	
Fs =	32000	psi	> 12576.28 psi OK
M/Vd =	3.50		
fv =	20.4	psi	
Fv =	21.79	psi	> 20.4 psi OK
Fv =	77.46	psi	Doesn't Control

Maximum bar size for 6" block

1/8" member thickness = 0.703125 in

one quarter of cell = 1 in

No. 9 bar

PROVIDE 2 NO 5 AT ENDS OF EACH SEGMENT

WALL LOADS

D =	750	lb/ft
L =	400	lb/ft
Self =	64	psf
	39	psf
Wind =	45	psf
	-31.02886	psf
Wind in plane =	8429	lbs
Wind out of plane =	45	psf

Relative Rigidities of Piers

Pier No.	Height	Length	h/l	Relative Rigidity Table ASD-89	Percentage of Lateral Force	V
1	10.5	7	1.5	1.27	0.4127397	3479.177
2	10.5	8	1.3125	1.62	0.5264868	4438.005
3	10.5	3	3.5	0.187	0.0607735	512.2883
				3.077		

Wall Segment 1

l =	7	ft
P =	2.45475	kips
Wind Segment =	3.479177	kips
M =	438.3763	kip*in
l =	84	in
t =	5.625	in
fa =	0.005195	ksi
r =	1.91	in
h/r =	65.96859	
Fa =	0.291737	psi
Try no 5 at end of wall		
d =	80	in
b =	5.625	in
As =	0.3	in^2
p =	0.000667	
n =	21.5	
pn =	0.014333	
k =	0.155585	
j =	0.948138	
fb =	165.0958	psi
Fb =	855	psi
fs =	19264.78	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	5.455	psi
Fv =	21.79	psi
Fv =	77.46	psi

Fully Grouted
At 32" O.C.
windward
leeward

Partially Grouted

OK > fa

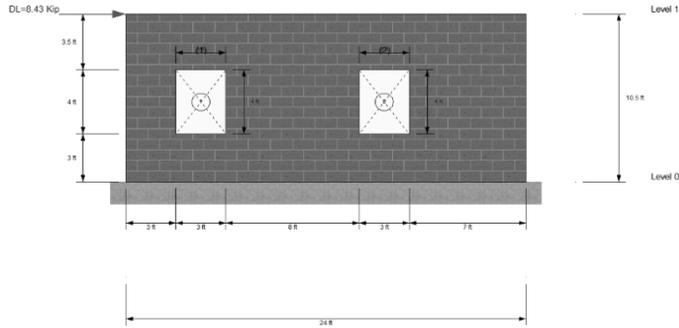
1 NO 5

> 165.0958 psi OK

> 19264.78 psi OK

> 5.455 psi OK

Doesn't Control



Wall Segment 2

l =	8	ft
P =	6.336	kips
Wind Segment =	4.438005	kips
M =	559.1887	kip*in
l =	96	in
t =	5.625	in
fa =	0.011733	ksi
r =	1.91	in
h/r =	65.96859	
Fa =	0.291737	psi
Try no 5 at end of wall		
d =	92	in
b =	5.625	in
As =	0.3	in^2
p =	0.00058	
n =	21.5	
pn =	0.012464	
k =	0.145912	
j =	0.951363	
fb =	169.2205	psi
Fb =	855	psi
fs =	21296.25	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	12.24348	psi
Fv =	21.79	psi
Fv =	77.46	psi

Partially Grouted

OK > fa

> 169.2205 psi OK

> 21296.25 psi OK

> 12.24348 psi OK

Doesn't Control

Wall Segment 2

l =	3	ft		
P =	2.586	kips		
Wind Segment =	0.512288	kips		
M =	64.54832	kip*in		
l =	36	in		
t =	5.625	in		
f _a =	0.01277	ksi		
r =	1.91	in	Partially Grouted	
h/r =	65.96859			
F _a =	0.291737	psi	OK > f _a	
Try no 5 at end of wall				
d =	32	in		
b =	5.625	in		
A _s =	0.3	in ²		
p =	0.001667			
n =	21.5			
p _n =	0.035833			
k =	0.234261			
j =	0.921913			
f _b =	103.7775	psi		
F _b =	855	psi	>	103.7775 psi OK
f _s =	7293.294	psi		
F _s =	32000	psi	>	7293.294 psi OK
M/Vd =	3.50			
f _v =	14.36667	psi		
F _v =	21.79	psi	>	14.36667 psi OK
F _v =	77.46	psi		Doesn't Control

Maximum bar size for 6" block

1/8" member thickness =	0.703125	in	No. 6 bar
one quarter of cell =	1	in	

WALL LOADS

D =	750	lb/ft
L =	400	lb/ft
Self =	64	psf
	39	psf
Wind =	45	psf
	-31.02886	psf
Wind in plane =	9810	lbs
Wind out of plane =	45	psf

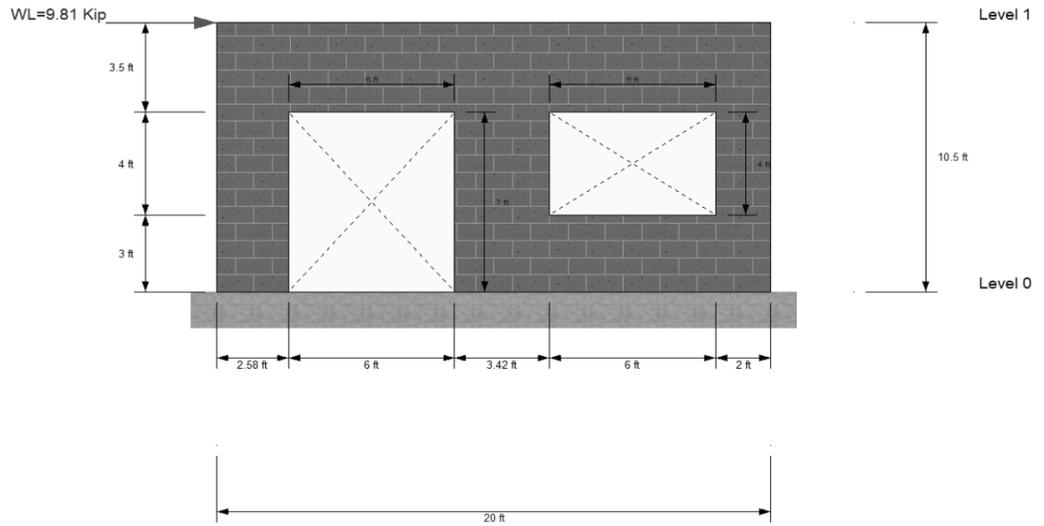
Relative Rigidity of Piers

Pier No.	Height	Length	h/l	Relative Rigidity		Percentage of Lateral Force	V
				Table ASD-89	Percentage of Lateral Force		
1	10.5	2.58	4.069767	0.125	0.323834	3176.794	
2	10.5	3.42	3.070175	0.199	0.515544	5057.456	
3	10.5	2	5.25	0.062	0.160622	1575.69	
				0.386			

Wall Segment 1

l =	2.58	ft
P =	2.271	kips
Wind Segment =	3.176794	kips
M =	400.276	kip*in
l =	30.96	in
t =	5.625	in
fa =	0.01304	ksi
r =	1.62	in
h/r =	77.77778	
Fa =	0.259259	psi
Try 2 no 6 at end of wall		
d =	23	in
b =	5.625	in
As =	0.88	in^2
p =	0.006802	
n =	21.5	
pn =	0.146242	
k =	0.413999	
j =	0.862	
fb =	753.8839	psi
Fb =	855	psi
fs =	22942.55	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	17.55362	psi
Fv =	21.79	psi
Fv =	77.46	psi

Fully Grouted



> 753.8839 psi OK
> 22942.55 psi OK
> 17.55362 psi OK
Doesn't Control

Wall Segment 2

l =	3.42	ft
P =	2.901	kips
Wind Segment =	5.057456	kips
M =	637.2394	kip*in
l =	48	in
t =	5.625	in
fa =	0.010744	ksi
r =	1.62	in
h/r =	77.77778	
Fa =	0.259259	psi
Try 2 no 6 at end of wall		
d =	33.04	in
b =	5.625	in
As =	0.88	in^2
p =	0.004735	
n =	21.5	
pn =	0.101803	
k =	0.360765	
j =	0.879745	
fb =	653.9563	psi
Fb =	855	psi
fs =	24912.83	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	15.60936	psi
Fv =	21.79	psi
Fv =	77.46	psi

Fully Grouted

> 653.9563 psi OK
> 24912.83 psi OK
> 15.60936 psi OK
Doesn't Control

Wall Segment 3

l =	2	ft		
P =	1.836	kips		
Wind Segment =	1.57569	kips		
M =	198.5369	kip*in		
l =	24	in		
t =	5.625	in		
fa =	0.0136	ksi		
r =	1.62	in	Fully Grouted	
h/r =	77.77778			
Fa =	0.259259	psi		
Try no 2 NO 5 at end of wall				
d =	16	in		
b =	5.625	in		
As =	0.6	in^2		
p =	0.006667			
n =	21.5			
pn =	0.143333			
k =	0.410933			
j =	0.863022			
fb =	777.5275	psi		
Fb =	855	psi	>	777.5275
fs =	23963.37	psi		
Fs =	32000	psi	>	23963.37 psi OK
M/Vd =	3.50			
fv =	20.4	psi		
Fv =	21.79	psi	>	20.4 psi OK
Fv =	77.46	psi		Doesn't Control

Maximum bar size for 6" block

1/8" member thickness = 0.703125 in No. 6 bar = 0.75 in

one quarter of cell = 1 in

No. 9 bar

PROVIDE 2 NO. 5/6 AT ENDS OF WALL SEGMENTS

WALL LOADS

D =	750	lb/ft
L =	400	lb/ft
Self =	64	psf
	39	psf
Wind =	45	psf
	-31.02886	psf
Wind in plane =	9810	lbs
Wind out of plane =	45	psf

Relative Rigidities of Piers

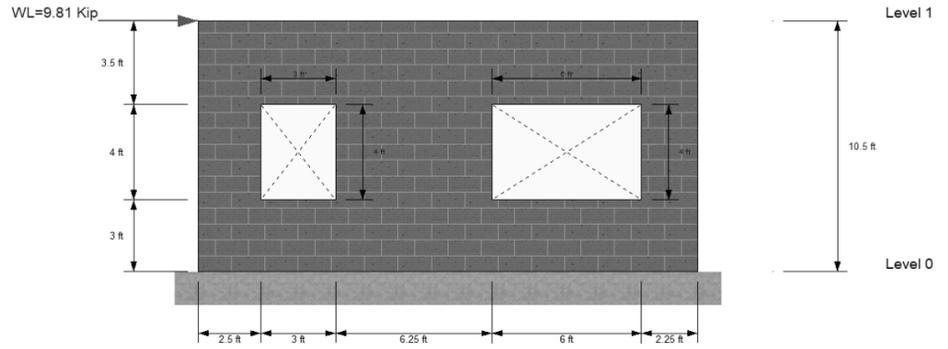
Pier No.	Height	Length	h/l	Relative Rigidity Table ASD-89	Percentage of Lateral Force	V
1	10.5	2.5	4.2	0.115	0.094031	922.4391
2	10.5	6.25	1.68	1.022	0.83565	8197.676
3	10.5	2.25	4.666667	0.086	0.070319	689.824
				1.223		

Wall Segment 1

l =	2.5	ft
P =	2.07975	kips
Wind Segment =	0.922439	kips
M =	116.2273	kip*in
l =	30.96	in
t =	5.625	in
fa =	0.011942	ksi
r =	1.62	in
h/r =	77.77778	
Fa =	0.259259	psi
Try no 5 at end of wall		
d =	26	in
b =	5.625	in
As =	0.3	in^2
p =	0.002051	
n =	21.5	
pn =	0.044103	
k =	0.256148	
j =	0.914617	
fb =	260.9391	psi
Fb =	855	psi
fs =	16291.99	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	14.22051	psi
Fv =	21.79	psi
Fv =	77.46	psi

Fully Grouted

> 260.9391 psi OK
> 16291.99 psi OK
> 14.22051 psi OK
Doesn't Control



Wall Segment 2

l =	6.25	ft
P =	5.0235	kips
Wind Segment =	8.197676	kips
M =	1032.907	kip*in
l =	75	in
t =	5.625	in
fa =	0.011908	ksi
r =	1.62	in
h/r =	77.77778	
Fa =	0.259259	psi
Try no 7 at end of wall		
d =	71	in
b =	5.625	in
As =	0.6	in^2
p =	0.001502	
n =	21.5	
pn =	0.0323	
k =	0.223911	
j =	0.925363	
fb =	351.6128	psi
Fb =	855	psi
fs =	26202.31	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	12.5784	psi
Fv =	21.79	psi
Fv =	77.46	psi

Fully Grouted

> 351.6128 psi OK
> 26202.31 psi OK
> 12.5784 psi OK
Doesn't Control

Wall Segment 3

l =	2.25	ft		
P =	2.0235	kips		
Wind Segment =	0.689824	kips		
M =	86.91783	kip*in		
l =	27	in		
t =	5.625	in		
fa =	0.013323	ksi		
r =	1.62	in	Fully Grouted	
h/r =	77.77778			
Fa =	0.259259	psi		
Try no 7 at end of wall				
d =	23	in		
b =	5.625	in		
As =	0.6	in^2		
p =	0.004638			
n =	21.5			
pn =	0.09971			
k =	0.357851			
j =	0.880716			
fb =	185.3626	psi		
Fb =	855	psi	>	185.3626
fs =	7151.444	psi		
Fs =	32000	psi	>	7151.444 psi OK
M/Vd =	3.50			
fv =	15.64058	psi		
Fv =	21.79	psi	>	15.64058 psi OK
Fv =	77.46	psi		Doesn't Control

Maximum bar size for 6" block

1/8" member thickness = 0.703125 in

one quarter of cell = 1 in

No. 9 bar

WALL LOADS

D =	750	lb/ft
L =	400	lb/ft
Self =	64	psf
	39	psf
Wind =	45	psf
	-31.02886	psf
Wind in plane =	3003	lbs
Wind out of plane =	45	psf

Relative Rigidities of Piers

Pier No.	Height	Length	h/l	Relative Rigidity Table ASD-89	Percentage of Lateral Force	V
1	10.5	3.5	3	0.278	0.5	1501.521
2	10.5	3.5	3	0.278	0.5	1501.521
				0.556		

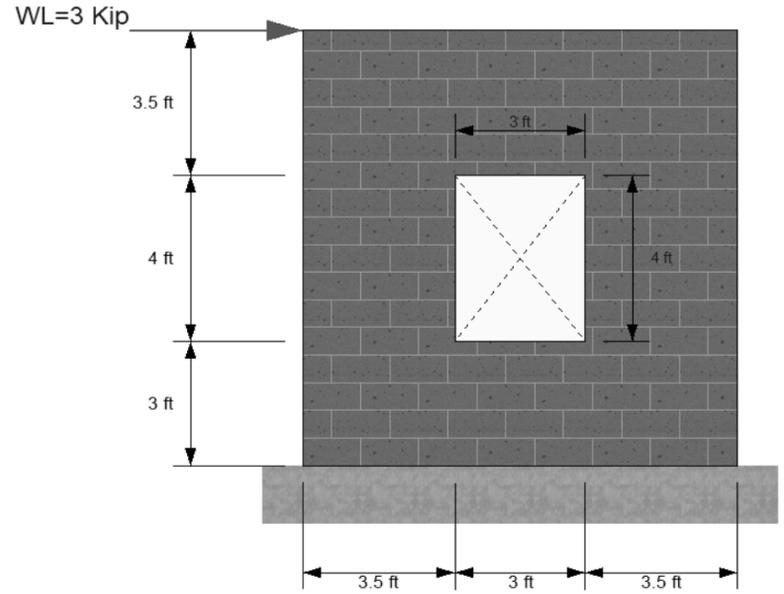
Fully Grouted
At 32" O.C.
windward
leeward

Wall Segment 1/2

l =	3.5	ft
P =	2.82975	kips
Wind Segment =	1.501521	kips
M =	189.1917	kip*in
l =	42	in
t =	5.625	in
fa =	0.011978	ksi
r =	1.9	in
h/r =	66.31579	
Fa =	0.290859	psi
Try no 5 at end of wall		
d =	38	in
b =	5.625	in
As =	0.3	in ²
p =	0.001404	
n =	21.5	
pn =	0.030175	
k =	0.217335	
j =	0.927555	
fb =	231.0856	psi
Fb =	855	psi
fs =	17891.94	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	13.2386	psi
Fv =	21.79	psi
Fv =	77.46	psi

Partially Grouted

> 231.0856 psi OK
> 17891.94 psi OK
> 13.2386 psi OK
Doesn't Control



WALL LOADS

D =	750	lb/ft
L =	400	lb/ft
Self =	64	psf
	39	psf
Wind =	45	psf
	-31.02886	psf
Wind in plane =	3003	lbs
Wind out of plane =	45	psf

Relative Rigidities of Piers

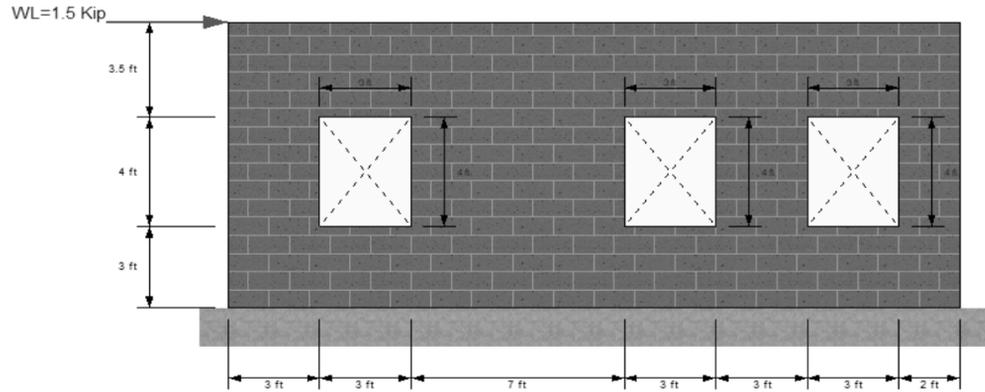
Pier No.	Height	Length	h/l	Relative Rigidity Table ASD-89	Percentage of Lateral Force	V
1	10.5	3	3.5	0.187	0.109613	329.1729
2	10.5	7	1.5	1.27	0.744431	2235.559
3	10.5	3	3.5	0.187	0.109613	329.1729
4	10.5	2	5.25	0.062	0.036342	109.1375
				1.706		

Wall Segment 1/3

l =	3	ft
P =	2.45475	kips
Wind Segment =	0.329173	kips
M =	41.47579	kip*in
l =	36	in
t =	5.625	in
fa =	0.012122	ksi
r =	1.9	in
h/r =	66.31579	
Fa =	0.290859	psi
Try no 5 at end of wall		
d =	32	in
b =	5.625	in
As =	0.3	in^2
p =	0.001667	
n =	21.5	
pn =	0.035833	
k =	0.234261	
j =	0.921913	
fb =	66.68267	psi
Fb =	855	psi
fs =	4686.336	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	13.6375	psi
Fv =	21.79	psi
Fv =	77.46	psi

Partial Gouted

> 66.68267 psi OK
> 4686.336 psi OK
> 13.6375 psi OK
Doesn't Control



Wall Segment 2

l =	7	ft
P =	5.45475	kips
Wind Segment =	2.235559	kips
M =	281.6805	kip*in
l =	84	in
t =	5.625	in
fa =	0.011544	ksi
r =	1.9	in
h/r =	66.31579	
Fa =	0.290859	psi
Try no 5 at end of wall		
d =	80	in
b =	5.625	in
As =	0.3	in^2
p =	0.000667	
n =	21.5	
pn =	0.014333	
k =	0.155585	
j =	0.948138	
fb =	106.083	psi
Fb =	855	psi
fs =	12378.66	psi
Fs =	32000	psi
M/Vd =	3.50	
fv =	12.12167	psi
Fv =	21.79	psi
Fv =	77.46	psi

Partial Gouted

> 106.083 psi OK
> 12378.66 psi OK
> 12.12167 psi OK
Doesn't Control

Wall Segment 4

l =	2	ft		
P =	1.70475	kips		
Wind Segment =	0.109138	kips		
M =	13.75133	kip*in		
l =	24	in		
t =	5.625	in		
f _a =	0.012628	ksi		
r =	1.9	in	Partiall Grouted	
h/r =	66.31579			
F _a =	0.290859	psi		
Try no 5 at end of wall				
d =	20	in		
b =	5.625	in		
A _s =	0.3	in ²		
p =	0.002667			
n =	21.5			
pn =	0.057333			
k =	0.286111			
j =	0.90463			
f _b =	47.22666	psi		
F _b =	855	psi	>	47.22666 psi OK
f _s =	2533.51	psi		
F _s =	32000	psi	>	2533.51 psi OK
M/Vd =	3.50			
f _v =	15.15333	psi		
F _v =	21.79	psi	>	15.15333 psi OK
F _v =	77.46	psi		Doesn't Control

BY INSPECTION: Module 20' wall with one window will work with similar reinforcing

Twelve Foot Opening Design

DL roof =	20	psf	
Lr =	40	psf	
Half of Roof Width =	12.65	ft	
Height Above Opening =	1	ft	
Header DL =	252.98	lb/ft	
Header LL =	505.96	lb/ft	
Effective wind area =	21.33	sf	
D+L =	758.95	lb/ft	
0.6W =	-221.56	lb/ft	
Try 5.25 x 12			
b =	5.25		
d =	12.00		
Sx =	126.00	in ³	
Ix =	756.00	in ⁴	
Sy =	55.13	in ³	
Iy =	144.70	in ⁴	
Mapp D+L =	13661.04	lb ft	
Applied Stress D + L =	1301.05	psi	
Allowable Stress 2.6F-1.9E =	2600.00	psi	OK
Use L/360 defl criteria for brittle windows =	0.4	in	
Applied Live Load Deflection =	0.164343332	in	OK
Moment 0.6W =	-3988.106198	lb ft	
Applied Stress 0.6W =	-868.1591724	psi	
Fby =	1600	psi	OK
V app =	-1329.368733	lbs	OK
fv applied =	216.8418967	psi	
Fv =	300	psi	OK
V out of plane =	-997.0265495		
Use HGA10 KT =	1165	lbs	OK

Three Foot Opening Out of Plane Check

V (D+L) =	1138.42		
V(0.6W) =	-332.342		
HGA10kt out of plane =	1165	lbs	> -332.342 lbs OK

Six Foot Opening Out of Plane Check

V (D+L) =	2276.84		
V(0.6W) =	-664.684		
HGA10kt out of plane =	1165	lbs	> -664.684 lbs OK

Use HGA10 KT for 3' and 6' openings
for gravity conn. check see "Wall Design Calcs per WFCM"
for uplift see "Wall Design Calcs"

LVL PLY Connector Design

Max Shear Wind Loads =	-1329.368733	lbs	
Ply width =	1.75	in	
Ply height =	9.25	in	
Total width =	5.25	in	
Q =	14.1640625	in ³	
I =	111.5419922	in ⁴	
VQ/I =	-2025.704736	lbs/ft	
TRY 2 SDW22500-R50 screws			
Z' =	275	lbs/ft	
Spacing Required =	3.258125374	in	OK
USE 2 SDW22500-R50 screws staggered at 3" on center			

12' Lintel

Span/2 = 6' therefore not a deep beam.

Dead = 481.25 lb/ft
 Live = 550 lb/ft
 Self = 192 lb/ft
 1223.25 lb/ft

V = 4281.375 lb
 b = 5.625
 d = 30
 applied
 shear stress = 25.37111 psi
 $F'v = 2 * \sqrt{1900} = 87.17798$ psi
 M = 22018.5 lb-ft
 dv = 30 in
 $M/(Vdv) = 1$
 Fvm = 49.03761

OK
 No stirrups req.

M app = 264222 lb in
 As pro = 0.6 sq in
 b = 5.625
 d = 30
 Rho = 0.003556
 n = 21.5
 nRho = 0.076444
 k = 0.321968
 j = 0.892677
 fsteel = 16443.79 lb in
 fbmasonry = 363.1838 lb in

2 NO 5 Check spacing
 1.375 > 1" OK
 OK < 32000
 OK < 0.45 * 1900 = 855

Masonry Lintel Deflection

b = 5.625 in
 h = 22.875 in
 Ig = 5610.797 in^4
 fr = 1047.318 psi
 yt = 11.4375 in
 Mcr = 513773.9 lb in
 M = 264222 lb in
 Mcr/Ma = 7.352063
 Em = 1350 ksi
 n = 21.48148
 d = 32 in
 As = 0.31 in^2
 p = 0.001722
 np = 0.036996
 c = 7.600727 in
 Icr = 4787.737 in^4
 Ie = 331872 in^4
 w = 0.05125 k/in
 L = 144 in
 Defl = 0.00064 in
 L/600 = 0.24 in

OK

Out of plane loading

Wind Load = -92.31727 psf
 Span = 12 ft
 M = -1661.711 lb ft
 Fb all = 65 psi
 Fv = 38.72983 psi
 S = 168.75 in³
 M/S = -118.1661 psi NG

Count on Bars at Bottom and top

As 0.6 two number fives
 d = 2.8125
 b = 32
 p = 0.006667
 n = 21.5
 pn = 0.143333
 k = 0.410933 OK
 j = 0.863022
 Fs = -13692.13 psi < 32000 psi OK
 Fbm = -444.2615 psi Fb all = 855

3 fully grouted cells next to masonry wall

As = 0.9
 Point load = -553.9036 lb
 b = 15.625
 d = 2.8125
 M = 1.55 kip ft
 M = 1550 lb ft
 As 0.9 three number fives
 d = 2.8125
 b = 15.625
 p = 0.02048
 n = 21.5
 pn = 0.44032
 k = 0.596271
 j = 0.801243
 Fs = 9170.937 psi OK
 Fbm = 629.9843 psi OK

6' Lintel

Dead = 411 lb/ft not a load bearing wall
 Live = 80 lb/ft
 Self = 42 lb/ft
 533 lb/ft

V = 1599 lb
 b = 5.625
 d = 11.125 two grouted cores
 applied
 shear stress = 25.55206 psi
 F'v = 2 * sqrt(1500) = 77.45967 psi
 M = 2398.5 lb-ft
 dv = 11.125 in
 M/(Vdv) = 1
 Fvm = 43.57106 OK no stirrups Fvm > applied

M app =	28782 lb in		
As pro =	0.3 sq in		
b =	5.625		
d =	11.125		
Rho =	0.004794		
n =	21.5		
nRho =	0.103071		
k =	0.36251		
j =	0.879163		
fsteel =	9809.122 lb in	< 32000 psi OK	
fbmasonry	259.441 lb in	Fb all =	675

Masonry Lintel Deflection

b =	5.625 in		
h =	15.25 in		
Ig =	1662.458 in ⁴		
fr =	290.4738 psi		
yt =	7.625 in		
Mcr =	63331.22 lb in		
M =	28782 lb in		
Mcr/Ma =	10.65346		
Em =	1350 ksi		
n =	21.48148		
d =	12.5 in		
As =	0.62 in ²		
p =	0.008818		
np =	0.189419		
c =	5.682083 in		
Icr =	963.0706 in ⁴		
Ie =	846612 in ⁴		
w =	0.05125 k/in		
L =	144 in		
Defl =	0.000251 in	OK	
L/600 =	0.24 in		

12' Lintel

Span/2 = 6' therefore not a deep beam.

Dead = 475 lb/ft
 Live = 200 lb/ft
 Self = 85.33333 lb/ft
 760.3333 lb/ft

V = 2661.167 lb
 b = 5.625
 d = 17.375
 applied
 shear stress = 27.22856 psi
 $F'v = 2 * \text{sqrt}(1900) = 87.17798$ psi
 M = 13686 lb-ft
 dv = 17.375 in
 $M/(Vdv) = 1$
 Fvm = 49.03761

No Stirrups Pro

M app = 164232 lb in
 As pro = 0.6 sq in
 b = 5.625
 d = 17.375
 Rho = 0.006139
 n = 21.5
 nRho = 0.13199
 k = 0.398483
 j = 0.867172
 fsteel = 18166.71 lb in
 fbmasonry = 559.7579 lb in

2 no 5

Check spacing
 1.375 > 1" OK

OK < 32000
 OK < 0.45 * 1900 = 855

Masonry Lintel Deflection

b = 5.625 in
 h = 14 in
 Ig = 1286.25 in⁴
 fr = 1047.318 psi
 yt = 7 in
 Mcr = 192444.7 lb in
 M = 164232 lb in
 Mcr/Ma = 1.608957
 Em = 1350 ksi
 n = 21.48148
 d = 32 in
 As = 0.31 in²
 p = 0.001722
 np = 0.036996
 c = 7.600727 in
 Icr = 4787.737 in⁴
 Ie = -9796.567 in⁴
 w = 0.05125 k/in
 L = 144 in
 Defl = -0.021696 in
 L/600 = 0.24 in

OK

Foundation and Porch Conc. Design

DL =	20	psf
LL =	40	psf
Lr =	20	psf
Wall Weight Wood =	20	psf
Wall Weight Masonry =	39	psf
Wall Height CMU =	10.5	ft
Wall Height Wood =	8	ft
Bearing Width Footing =	2	ft
Slab Wt.	75	psf
Trib 24' wall	10	ft
D+ (24' wall)	1050.75	lb/ft
L (24' wall)	225	lb/ft
Trib 20' wall	3	ft
D (20' wall)	854.5	lb/ft
Increase for Gaps in Wall Carried by beam =	2.823529412	
D INTERIOR WALL =	2647.058824	lb/ft
L INTERIOR WALL =	1411.764706	lb/ft
Footing Weight =	300	lb/ft
Bearing Pressure/ft =	787.875	psf/ft
Allowed Bearing Pressure =	1500.00	psf
Uplift Check:		
Dead Load into Ram 24' wall =	1516.00	lb/ft
Dead Load into Ram 20' wall =	854.50	lb/ft
Live Load into Ram 24' wall =	225.00	lb/ft
Wind Uplift =	-94.70103178	psf
Wind Uplift into Ram 24' wall =	-947.0103178	lb/ft
Wind Wall Pressure =	94.45	psf
Wind Overturning Moment =	16163.48	lb/ft/ft
Wind Overturning into Ram 24' wall =	808.1741511	lb/ft
Total Uplift Wind Only =	1755.184469	lb/ft
Uplift on Compression Wall =	-138.8361667	lb/ft

2' wide footing
OK

Uplift transferred through trusses
Combined

Compression or Uplift

Safe Room Loads:

DL Roof =	75	psf
LL =	150	psf
Wall Wt. =	512	lb/ft
Wind Speed =	250	mph
Kd =	0.85	
Kzt =	1	
G =	0.85	
Kh =	1.03	
qz =	140.08	psf
G =	0.85	
Cp windward =	0.8	
Cp leeward =	-0.5	
Cp Side =	-0.7	
Cp roof =	-0.9	
Gcpi =	0.55	
Windward load =	18.2104	psf
Leeward load =	-136.578	psf
Upward Load =	-184.2052	psf
Sidewall Load =	-160.3916	psf

Porch Wind lods

DL Roof =	self	
LL =	40	psf
Wind Speed =	190	mph
Kd =	0.85	
Kzt =	1	
G =	0.85	
Kh =	1.1	
qz =	86.40896	psf
G =	0.85	
Cn =	1.2	
Cf =	2	
Wall Wind Load =	146.8952	psf
Roof Uplift =	88.13714	psf
Wall Span =	11.5	ft
Mu (wind) =	2.428362	k ft
As req prelim =	0.151773	sq in
As min =	0.144	sq in
Vu =	2.111619	kip
Phi Vc =	3.943602	kip
a =	0.575163	in
d =	3.625	in
Phi Mn =	6.608088	kip ft

No.6 at 12"

8" Wall d =4"

OK

make roof steel similar to wall steel (roof has less loads and smaller span)

RAM Results:

Max Uplift =	0.05	in
Max Slab Stress =	0.36	ksi
Modulus of Rupture/Safety Factor =	0.205395959	ksi
Max Bearing Pressure =	755	psf

Minimal

Need Tensile Reinforcement

OK < 1500 psf

Applied Moment (ASD)

M =	810	ft lb
MOR =	410.7919181	psi
b =	12	in
h =	4	in
Mcr =	1095.445115	ft lb
M*FS =	1620	ft lb
As =	0.017910448	
As subdrag =	0.02	
As provided =	0.28	
d =	2	
a =	0.039215686	
c =	0.046136101	
Es =	0.12705	> 0.005 Tension Controlled
Ma =	2772.54902	ft lb > M _{applied} x FS OK

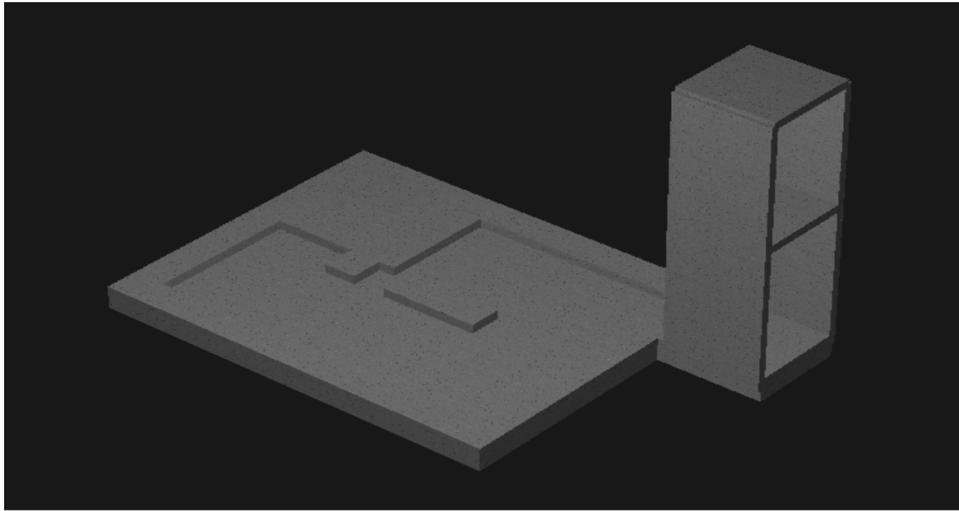
per foot of slab

> M_{cr} Need to count on reinf

W8 x W8 4" spacing

Assumed Center specify

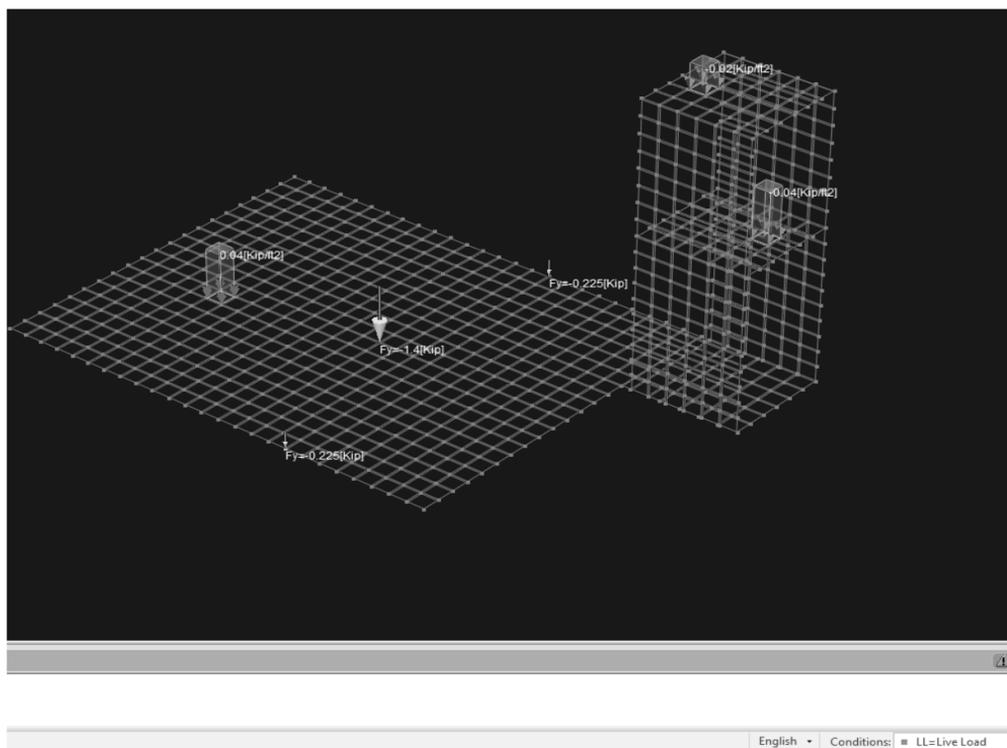
upper 1/3



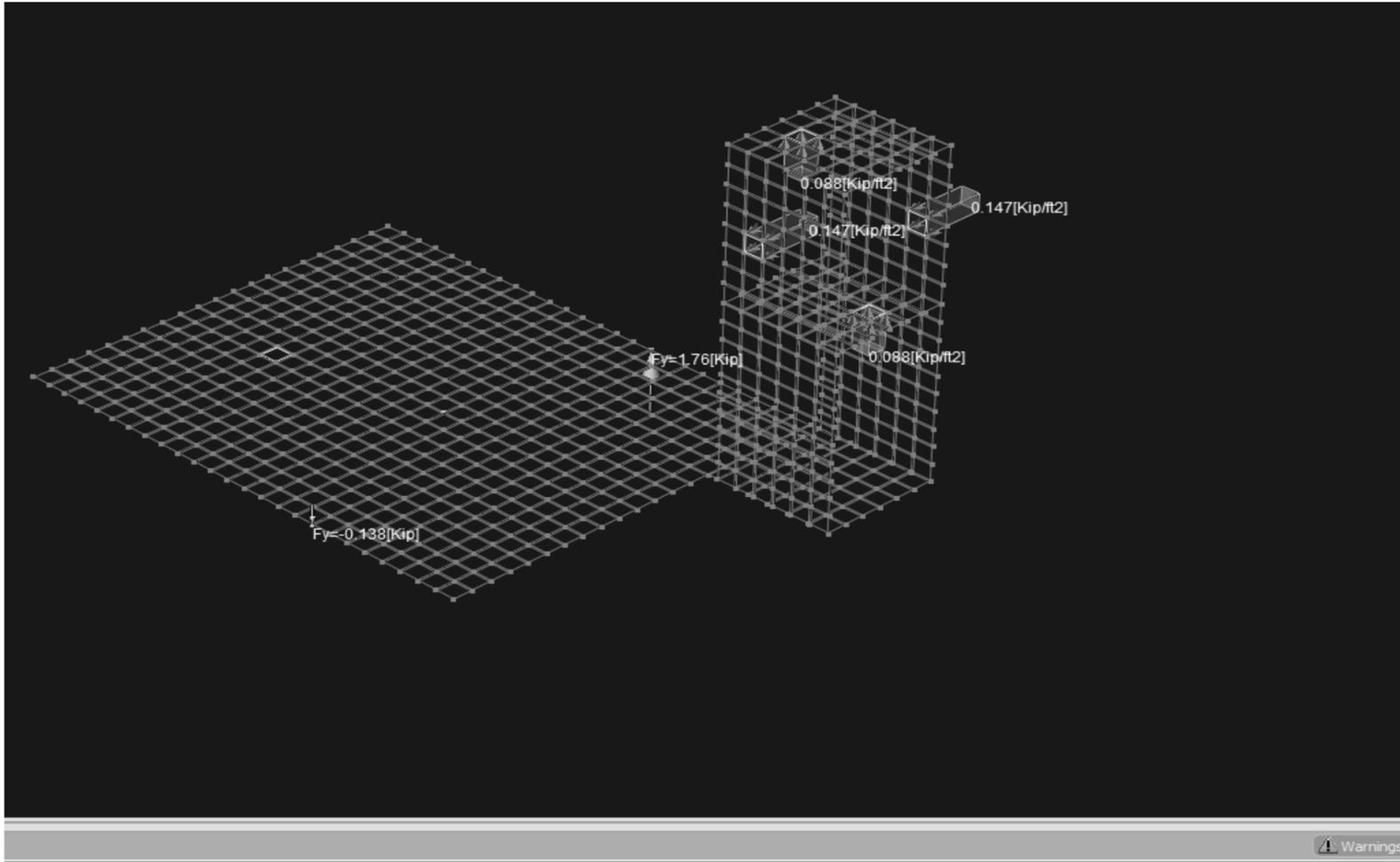
RAM MODEL RENDERING



RAM MODEL APPLIED DEAD LOADS

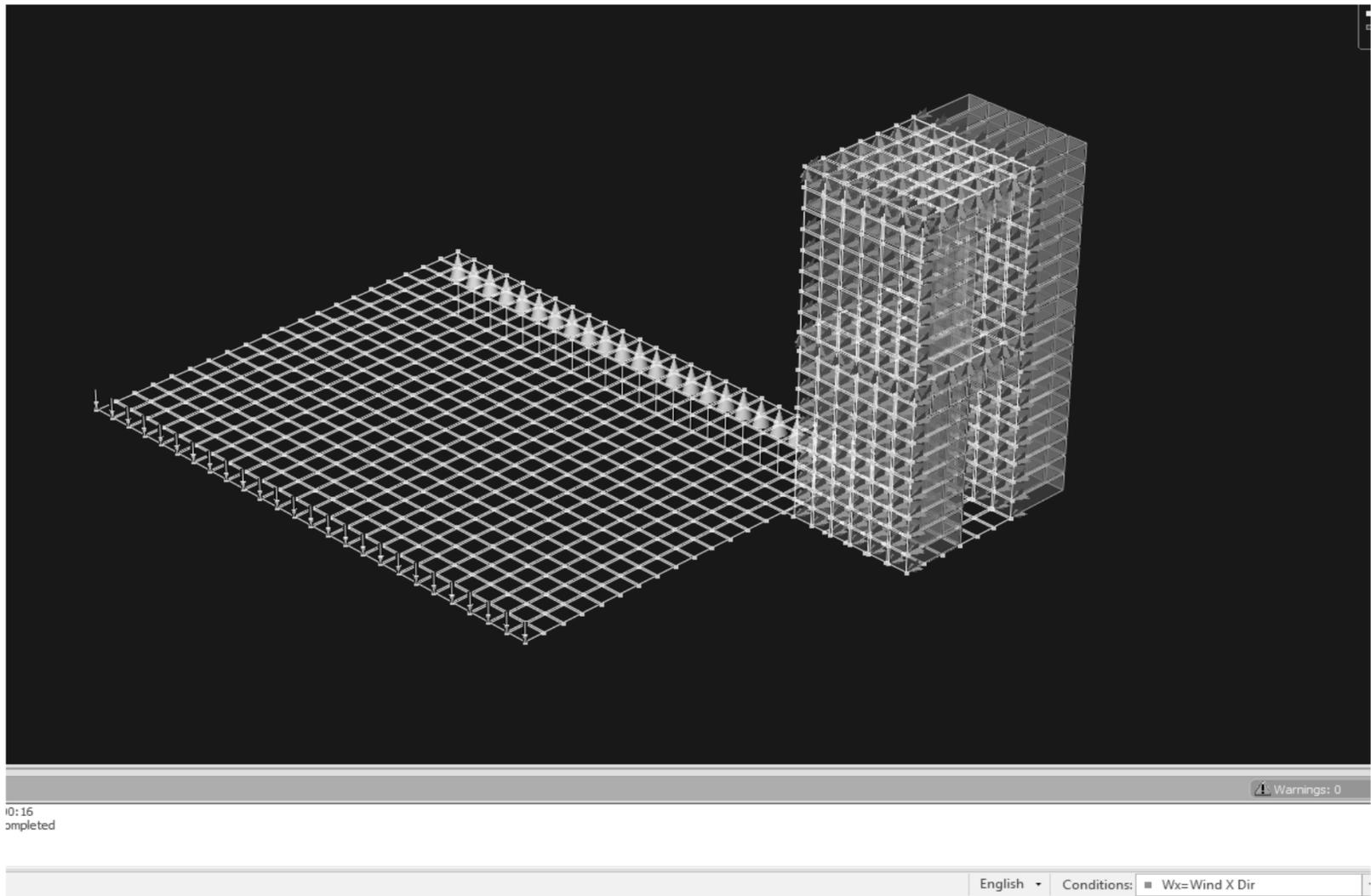


RAM MODEL APPLIED LIVE LOADS (note area Live load not applied to slab to produce maximum tension in slab)

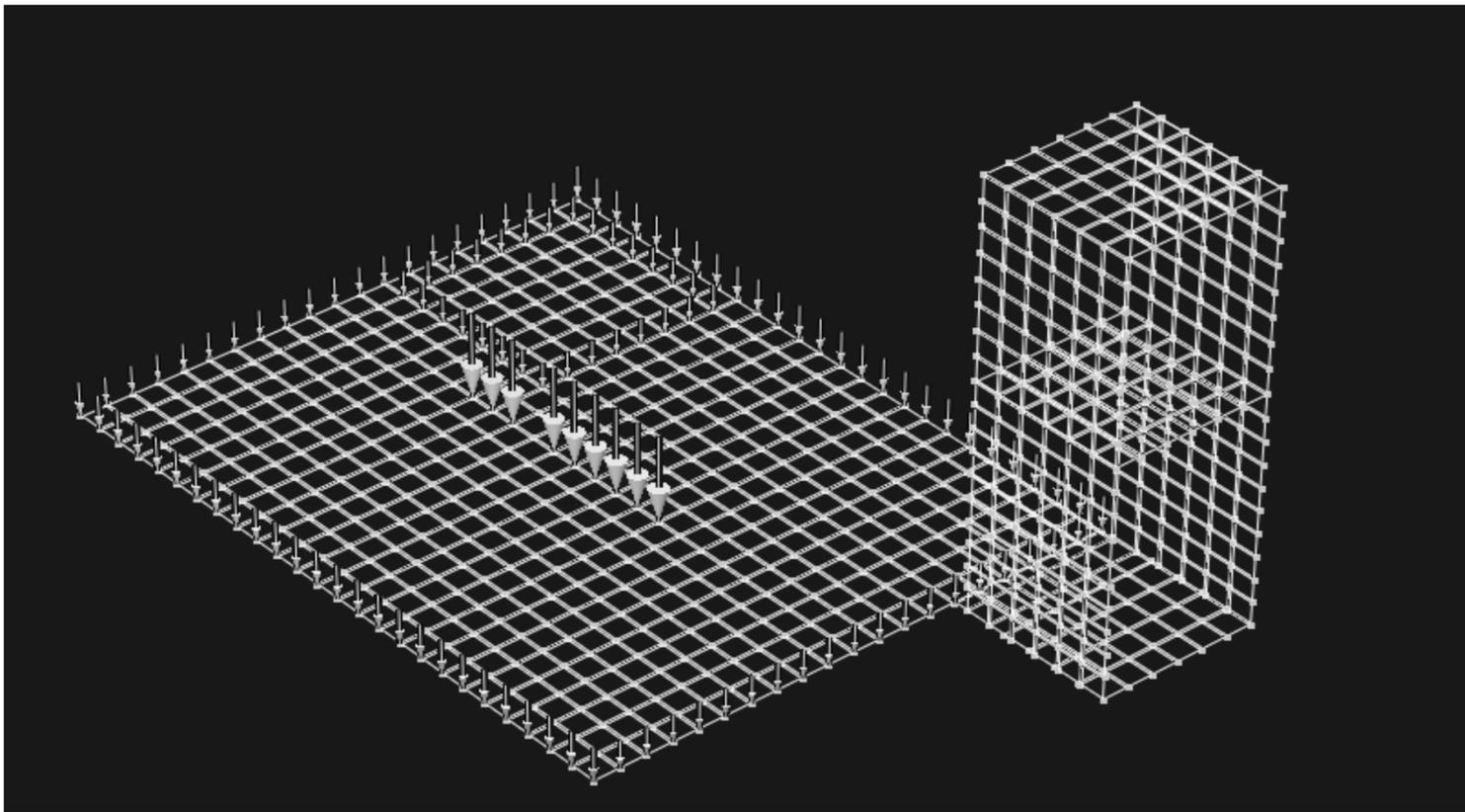


English ▾ Conditions: ■ Wx=Wind X Dir

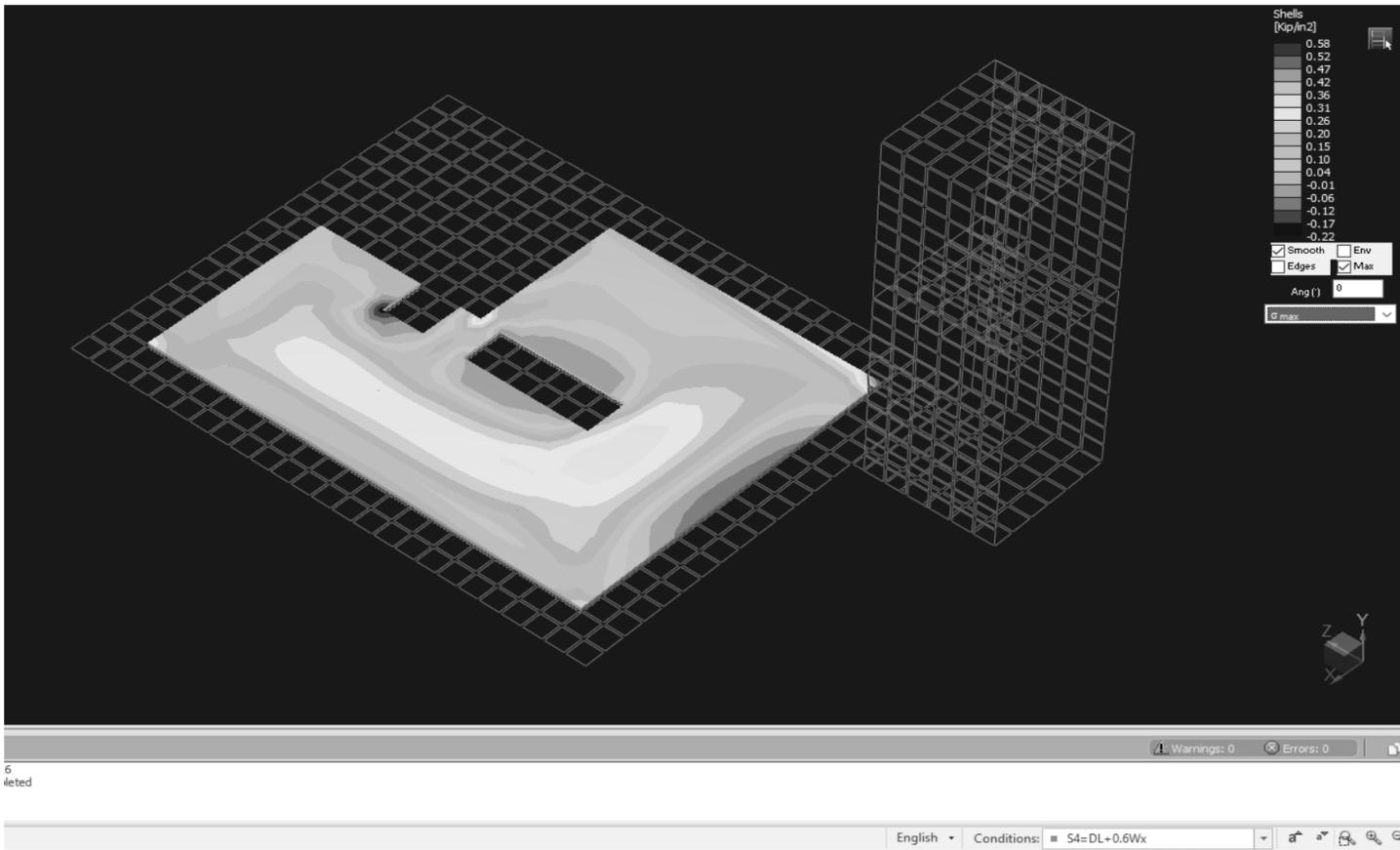
RAM MODEL APPLIED WIND LOADS



RAM MODEL APPLIED WIND LOADS



RAM MODEL APPLIED DEAD LOADS



RAM MODEL APPLIED STRESS

Interior Beam Design

DL =	0.9375	k/ft
LL =	0.5	k/ft
Wu =	1.925	k/ft
Span =	11.33	ft
Vu =	10.905125	kip
Min depth =	8.4975	in
Ceiling Height is 9'-4" minus 6" = 8'-10"		
Even block course at 8'-0" try 10" deep beam		
8" width		
Phi Vc =	8.544471897	kip
Try No. 4 at 18"		
Phi Vs =	8	kip
Phi VC + Phi VS =	16.5444719	kip
Av/s pro =	0.022222222	OK
Av/s Min =	0.006846532	
Av/s Min =	0.005	
d =	13	in
Mu =	30.88876656	k ft
As flexure required =	0.594014742	sq in
As min =	0.213611797	sq in
As min =	0.26	sq in

ACI does have an exception for 10" deep beams however if the slab is included in the beam depth then the beam is really 16" deep

OK
OK

2 no 5

2 no 5 with no. 4 stirrups at 18" on center

Elev Slab Design

Span =	11.33	ft
DI =	0.075	k/ft
LL =	0.04	k/ft
Wu =	0.154	k/ft
Mu =	2.471101325	k*ft
Vu =	0.77	kip
As req =	0.247110133	sq in
As min =	0.144	sq in
Phi Vc =	2.464751509	kip

No. 5 at 12
OK
OK

Exterior Stair Beam Design

DL slab and stairs =	75	psf	
LL slab and stairs =	40	psf	
Trib =	12.58	ft	half of stairs and all of landing
Wu =	1.93732	k/ft	
Span =	3.5	ft	
Vu =	3.39031	kip	
Try 10" deep x 8" wide beam			
d =	7.5	in	
Phi Vc =	6.161878772	kip	Since h<= 10" per ACI Table 9.6.3.1 Min. Stirrups not required.
Mu =	2.96652125	k ft	
As flexure required =	0.098884042	sq in	2 no 5
As min =	0.205395959	sq in	
As min =	0.25	sq in	CONT 2 no 5 As pro = 0.6 sq in.
Tu =	2.23685	kip ft	
Acp	100	sq in	
Pcp =	40	in	
Torsion Threshold =	0.855816496	kip ft	< 2.23 kip ft Therefore Stirrups Req.
At/s =	1.21833E-06		
No. 4 at 12" At/s =	0.016666667	OK	
As min =	0.1	< 0.4 sq in ok	Use No. 4 at 12" Stirrups

Wall Design

Wu =	146.895232	psf	
Span =	10.5	ft	
Mu =	2.024399916	k*ft	
Vu =	0.771199968	kip	
As req =	0.202439992	sq in	No. 5 at 12
As min =	0.144	sq in	OK
Phi Vc =	2.464751509	kip	OK

Wall FTG Design

BRG =	760.625	lb/ft	2'-0" width OK < 1500
Span =	0.75	ft	
As min =	0.288	sq in	OK No. 5 at 12"